

# Bound Reports

## 1720

LEGENDS @ KINGS RIDGE  
STORMWATER CALCULATIONS  
FBA NO. 961504.001

4-069-0357A-ERP

19451-1  
**RECEIVED**  
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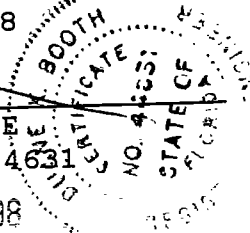
FARNER, BARLEY & ASSOCIATES, INC.  
350 NORTH SINCLAIR AVENUE  
TAVARES, FLORIDA 32778

BY: \_\_\_\_\_

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DATE: \_\_\_\_\_

SEP 28 1998



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Lake Louisa Club (A/K/A Legends) November 22, 1996
  - B. Geotechnical Engineering Study  
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  - C. Geotechnical Investigation of Legends Subdivision July 22, 1998
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**LEGENDS  
(F/K/A LAKE LOUISA CLUB)**

**STORMWATER DESIGN SUMMARY**

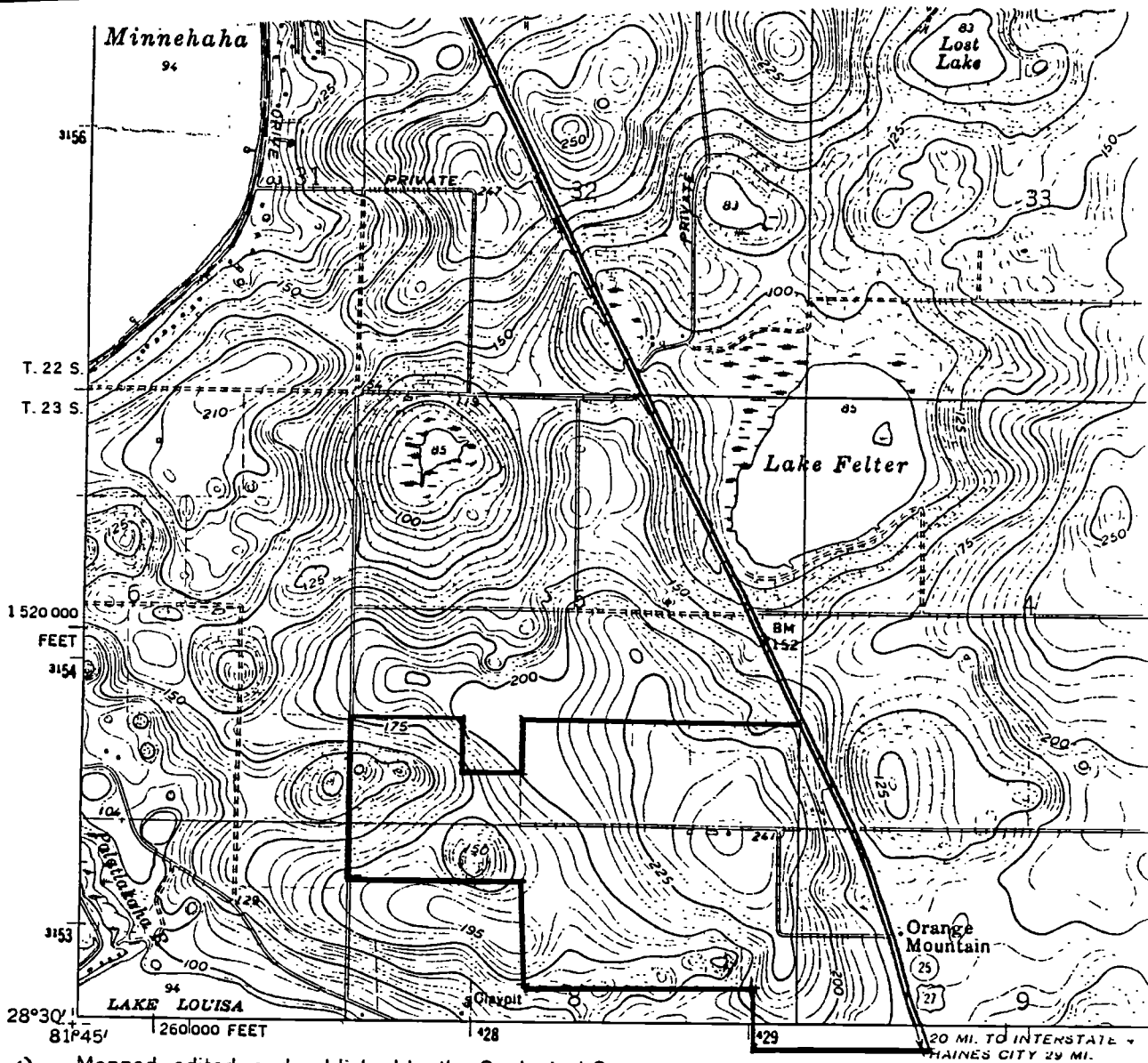
Legends is located in Sections 4, 5, 8, and 9 of Township 23S, Range 26E on U.S. Highway 27 South of Clermont consisting of approximately 403 acres. The property as existing today is mostly burned out orange grove and an abandoned farm house and sheds with a paved drive from U.S. Highway 27 to the farm house. The grove has been replanted with small pine trees.

Since the subject property does not have a positive outfall, the stormwater management system is designed to retain the total runoff from the 25 year-96 hour storm event. Therefore, the pre-develop site conditions were not modeled for pre vs. post comparison.

All ponds have been modeled through "ICPR" with infiltration calculated through "ponds". Pond 9 has been omitted in "ponds" because it is a lined pond and used for irrigation as discussed in the pre-application meeting. Ponds 18, 20, 22, and 24 shall be over excavated and filled with clean sand to provide adequate depth between pond bottom and confining layer as suggested in soil report. The plans and calculations depict the appropriate elevation of excavation. Basins 5, 13, and 17 do not exist and are not referred to in this submittal. These basins were used in preliminary design and were eventually omitted from final design.

See ICPR Max Node conditions for comparison of peak stage versus pond max elevation and ponds Recovery analysis for stormwater treatment volume calculation and recovery analysis.

MAPS



(LAKE NELLIE)  
1650 IV NE

Mapped, edited, and published by the Geological Survey

Control by USGS and USC&GS

Planimetry by photogrammetric methods from aerial photographs taken 1952. Topography by planetable surveys 1962

Polyconic projection

10,000-foot grid based on Florida coordinate system, east zone

1000-meter Universal Transverse Mercator grid ticks,

zone 17, shown in blue. 1927 North American Datum

To place on the predicted North American Datum 1983

move the projection lines 27 meters south and

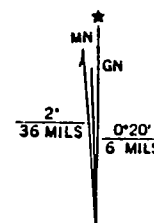
18 meters west as shown by dashed corner ticks

Fine red dashed lines indicate selected fence and field lines where generally visible on aerial photographs. This information is unchecked

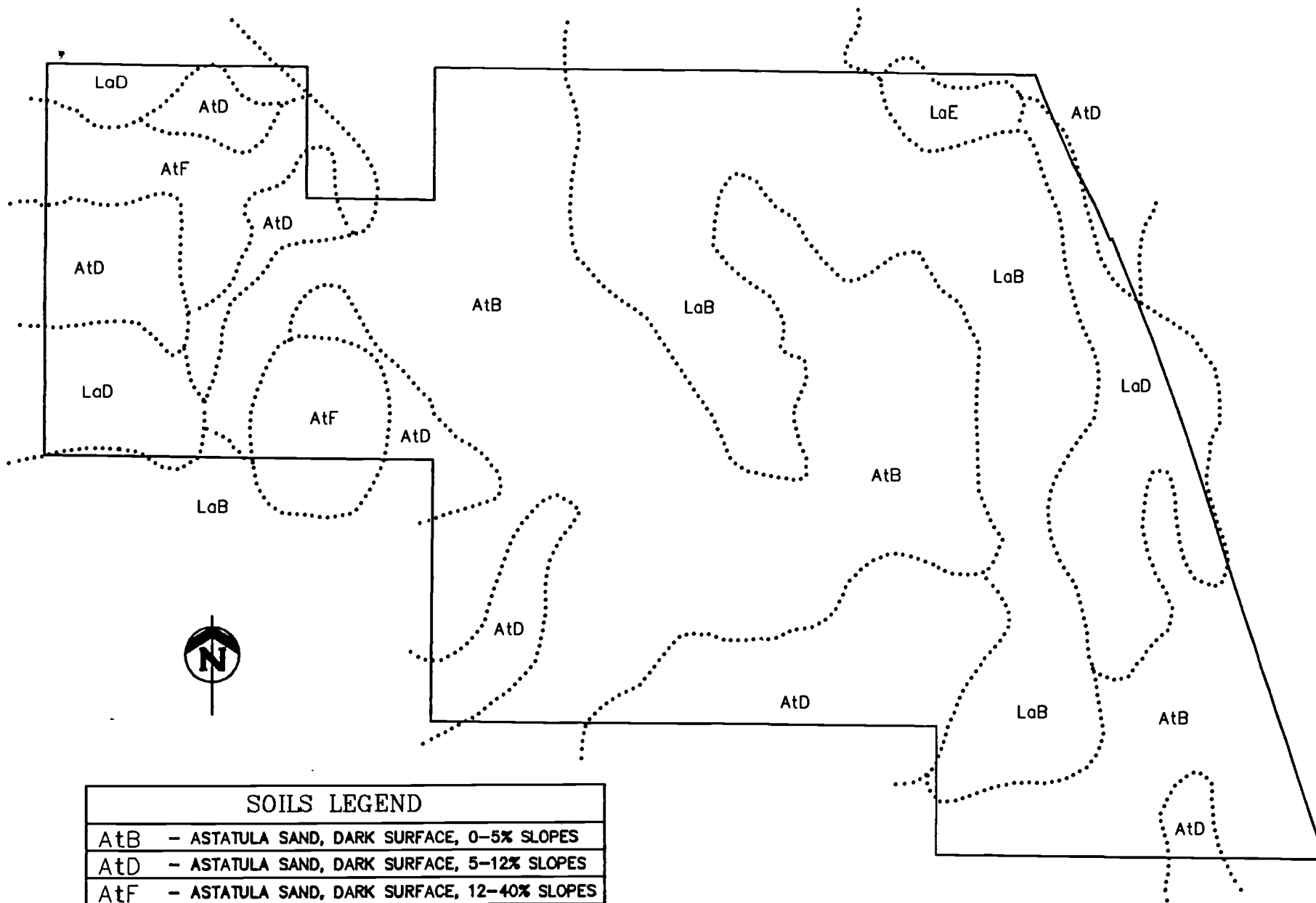
Revisions shown in purple compiled from aerial photographs

taken 1977 and other source data. This information not

field checked. Map edited 1980



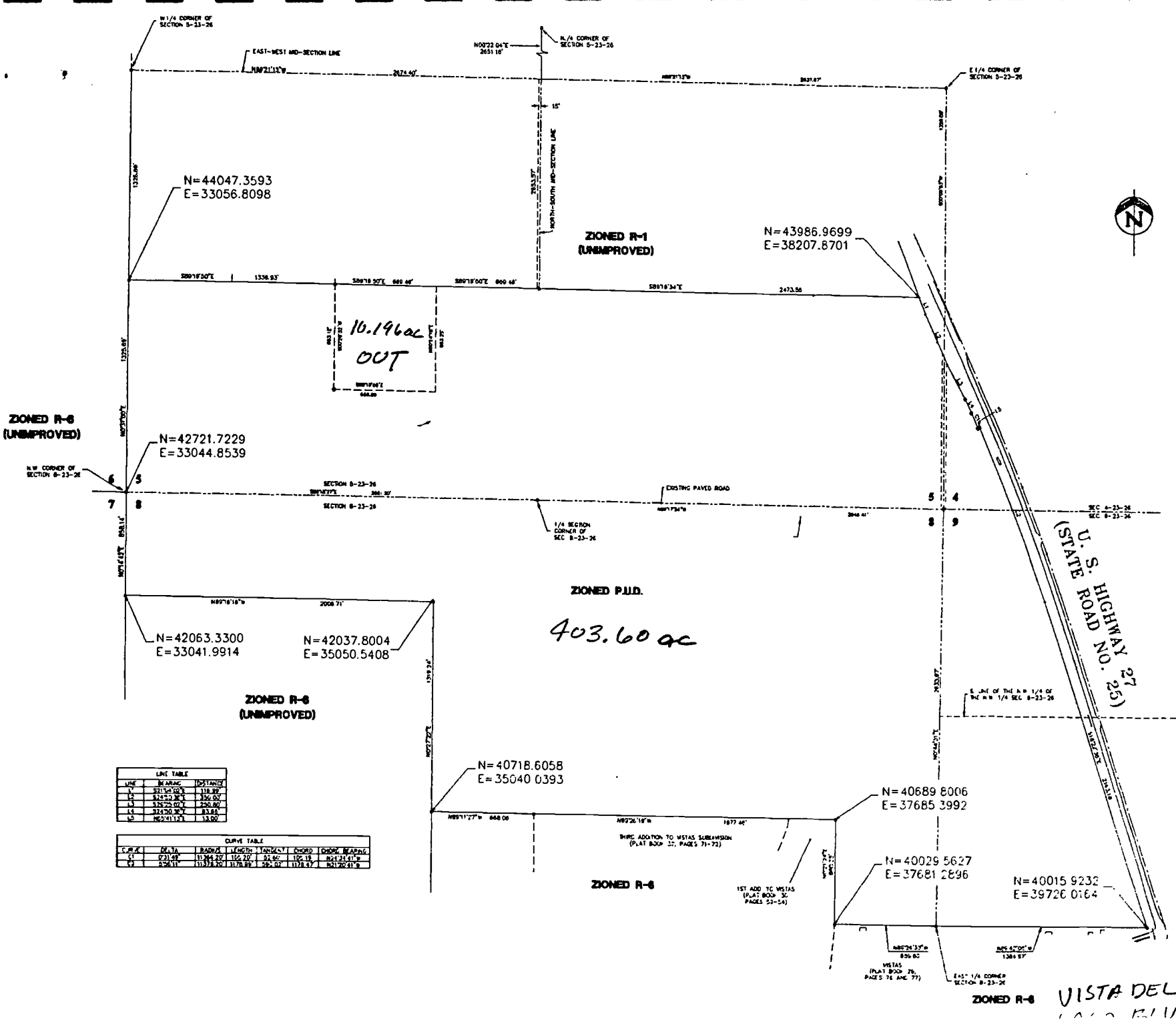
UTM GRID AND 1980 MAGNETIC NORTH DECLINATION AT CENTER OF SHEET



### SOILS LEGEND

AtB	- ASTATULA SAND, DARK SURFACE, 0-5% SLOPES
AtD	- ASTATULA SAND, DARK SURFACE, 5-12% SLOPES
AtF	- ASTATULA SAND, DARK SURFACE, 12-40% SLOPES
LaB	- LAKE SAND, 0-5% SLOPES
LaD	- LAKE SAND, 5-12% SLOPES
LaE	- LAKE SAND, 12-22% SLOPES

NOTE: SOIL INFORMATION OBTAINED FROM U.S.D.A.  
SOIL CONSERVATION SERVICE.



N=44047.3593  
E=33056.8098

N=43986.9699  
E=38207.8701

N=42721.7229  
E=33044.8539

N=42063.3300  
E=33041.9914

N=42037.8004  
E=35050.5408

N=40718.6058  
E=35040.0393

N=40689.6006  
E=37685.3992

N=40029.5627  
E=37681.2896

N=40015.9232  
E=39726.0164

10.196 ac  
OUT

403.60 ac

LINE	BEARING	DISTANCE
1	S73°34'00"W	118.89'
2	S74°57'30"E	136.02'
3	S75°25'00"E	220.80'
4	S74°50'30"E	83.83'
5	N62°41'17"E	13.02'

C.P.#	DEG. A	RADIUS	LENGTH	CHORD	CHORD BEARING
1	0°31'49"	11,984.20'	162.20'	55.86'	N64°21'41"W
2	2°56'11"	11,978.20'	117.88'	58.20'	N17°40'41"E

VISTA DEL  
LAO BLVD.



**DEVELOPED BASIN SUMMARY  
AND CURVE NUMBER CALCULATION**

LOT SIZE	SITE IMPERVIOUS AREA
65' X 115'	3750 SF
80' X 115'	4725 SF

BASIN NUMBER	AREA (ON SITE) (acres)	AREA (OFF SITE) (acres)	TOTAL AREA (acres)	IMPERVIOUS AREA (acres)	PERVIOUS AREA (acres)	CN
B1	7.84	—	7.84			50
B2a	8.64	—	8.64			55
B2b	18.74	—	18.74			54
B2c	14.84	—	14.84			49
B3	23.59	—	23.59			62
B4	18.39	—	18.39			48
B6	10.47	—	10.47			39
B7	32.65	—	32.65			51
B8	6.92	—	6.92			45
B9	7.81	—	7.81			60
B10	13.60	—	13.60			53
B11	11.52	—	11.52			52


BASIN NUMBER	AREA (ON SITE) (acres)	AREA (OFF SITE) (acres)	TOTAL AREA (acres)	IMPERVIOUS AREA (acres)	PERVIOUS AREA (acres)	CN
B12	14.39	—	14.39			53
B14	4.79	—	4.79			54
B15	16.02	—	16.02			51
B16	17.16	—	17.16			54
B18	23.37	0.66	24.03			54
B19	11.26	—	11.26			51
B20	8.70	—	8.70			51
B21	23.79	—	23.79			57
B22	11.22	3.13	14.35			48



# STORM RUNOFF WORKSHEET

PROJECT #: 961504.001 PROJECT: LEGENDS DATE: 6/2/98  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 1 TOTAL AREA 7.84 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	6.40		39	82	3198	
RES		14 X 3750 = 1.21						
PUMT		24 X 414 = 0.23						
		<u>1.44</u>		1.44	98	18	1764	
TOTALS								4962

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 50

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. (2) TOTAL AREA \_\_\_\_\_ STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	38.10		39	85		
RES		44 X 3750 = 165,000						
PUMT		24 X 1655 = 39,720						
		BLVD <u>82,860</u>						
		<u>287,580</u>		6.60	98	15		
TOTALS								

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = \_\_\_\_\_

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: LEGENDS DATE: 6/15/98  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. B29 TOTAL AREA 8.64 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GLASS - GOOD	6.31		39	73	2347
RES		21 X 3750 =	78,750				
PVMT		24 X 947 =	22,728				
		<u>101,478</u>		2.33	98	27	2644
TOTALS							5493

PRODUCT COVERAGE =  $\overline{CN} = 55$

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. B26 TOTAL AREA 18.74 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GLASS - GOOD	13.82		39	74	2886
RES		21 X 3750 =	78750				
CLUB SITE		85% IMP =	50816				
PVMT		=	74800				
		<u>204,366</u>		4.92	98	24	2548
TOTALS							5434

PRODUCT COVERAGE =  $\overline{CN} = 54$

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: LEGENDS DATE: 6/24/98  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. B2c TOTAL AREA 14.84 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A		12.35		39	83	3237
RES		3 X 4725 = 14,175					
		2 X 3750 = 7,500					
PVMT		23 X 964 = 22,192					
		48,667		1.12	98	8	784
POWDER (NET)		EL. 163.00	59,326		98	9	882
TOTALS							4903

PRODUCT COVERAGE =  $\bar{CN}$  = 49

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. \_\_\_\_\_ TOTAL AREA \_\_\_\_\_ STORM: \_\_\_\_\_ YEAR \_\_\_\_\_ HOUR \_\_\_\_\_

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
TOTALS							

PRODUCT COVERAGE =  $\bar{CN}$  = \_\_\_\_\_

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = 11.6 in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_

PRE-DEVELOPMENT  
 POST-DEVELOPMENT

BASIN NO. 3 TOTAL AREA 23.59 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	14.40		39	61	23.79	
	Res	30 X 4725 = 3.25						
	PUMPT	24 X 1871 = 1.03						
	85% MAINT/SHOP	5.78 ac. 0.25 = 4.91						
		9.19		9.19	98	31	3822	
TOTALS								6201

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 6.2

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 4 TOTAL AREA 18.39 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	15.41		39	84	3274	
	RES	20 X 4725 = 2.17						
	PUMPT	0.81						
		2.98		2.98	98	16	1563	
TOTALS								4844

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 48

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.



# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. <b>5</b>		TOTAL AREA <b>2.77</b>			STORM: <b>25</b> YEAR <b>96</b> HOUR		
SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<b>A</b>	<b>GREEN GRASS - GOOD</b>	<b>2.77</b>	<b>0</b>	<b>39</b>	<b>100</b>	<b>3400</b>
					<b>98</b>	<b>0</b>	<b>0</b>
TOTALS							<b>3400</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\overline{CN} = 39$

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. <b>6</b>		TOTAL AREA <b>10.47</b>			STORM: <b>25</b> YEAR <b>96</b> HOUR		
SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<b>A</b>	<b>GREEN GRASS - GOOD</b>	<b>10.47</b>	<b>0</b>	<b>39</b>	<b>100</b>	<b>3400</b>
					<b>98</b>	<b>0</b>	<b>0</b>
TOTALS							<b>3400</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\overline{CN} = 39$

$$S = \frac{1000}{CN} - 10$$

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

Q = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 7 TOTAL AREA 32.65 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	25.89		39	79	3081
	RES	11 X 4725 = 1.19					
	PUM'T	24 X 957 = 0.53					
	85% Rec SITE	1.15 ac x 0.85 = 5.23					
		<u>6.95</u>		6.76	98	21	2058
TOTALS						100	5139

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 51

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 8 TOTAL AREA 6.92 STORM: 25 YEAR 76 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	6.25		39	90	3510
	RES	6 X 3750 = 0.52					
	PUM'T	<u>0.15</u>					
		<u>0.67</u>		0.67	98	10	980
TOTALS							4490

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 45

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 9 TOTAL AREA 7.81 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS - GOOD	5.02		39	64	2496
Res	9 X 3750 =	0.77				
PUM'T	24 X 536 =	0.30				
		1.07		98	14	1372
	POND (WET)		1.72	98	22	2156
TOTALS					6024	6024

PRODUCT COVERAGE =  $\bar{CN}$  = 60

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 10 TOTAL AREA 13.60 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS - GOOD	10.29		39	74	2964
Res	32 X 3750 =	2.75				
PUM'T	0.27 + 0.29 =	0.54				
		3.31		98	24	2352
TOTALS						5316

PRODUCT COVERAGE =  $\bar{CN}$  = 53

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 11 TOTAL AREA 11.52 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	8.97		39	78	3042
RES		27 X 3750 = 1.81					
PUM'T		24 X 1336 = 0.74					
		2.55		2.55	98	22	2154
TOTALS							5198

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\overline{CN}$  = 52

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 12 TOTAL AREA 14.39 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	10.90		39	76	2964
RES		27 X 3750 = 2.32					
PUM'T		24 X 2127 = 1.17					
		3.49		3.49	98	24	2352
TOTALS							5316

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\overline{CN}$  = 53

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_

PRE-DEVELOPMENT  
 POST-DEVELOPMENT

BASIN NO. \_\_\_\_\_ TOTAL AREA \_\_\_\_\_ STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
TOTALS						

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = \_\_\_\_\_

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.

RUNOFF R = \_\_\_\_\_ in.

\_\_\_\_\_ ac.ft.

\_\_\_\_\_ cu.ft.

BASIN NO. 14 TOTAL AREA 4.79 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS-GOOD	3.45		39	72	2808
RES	13 X 3750 = 1.12					
PUMT	$\frac{0.22}{1.34}$		1.34	98	28	2744
TOTALS						5552

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 56

$$S = \frac{1000}{CN} - 10$$

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.

RUNOFF R = \_\_\_\_\_ in.

\_\_\_\_\_ ac.ft.

\_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 15 TOTAL AREA 16.02 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	12.74		39	80	3120
		20 X 4725 = 94,500					
		24 X 2021 = 48,504					
		<u>143,004</u>		3.28	98	20	1960
TOTALS							5080

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 51$

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 16 TOTAL AREA 17.16 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	12.79		39	72	2808
		33 X 4725 = 155,925					
		24 X 2353 = 56,472					
		<u>212,397</u>		4.27	98	28	2744
TOTALS							5552

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 54$

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_

PROJECT: \_\_\_\_\_

DATE: \_\_\_\_\_

 PRE-DEVELOPMENT  
 POST-DEVELOPMENT

BASIN NO. 17

TOTAL AREA 0.42

STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS-GOOD	0.42		39	100	3900
TOTALS						3900

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

 PRODUCT COVERAGE =  $\bar{CN}$  = 39

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
 P = rainfall (in.)

 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 18

 ON SITE + OFF SITE  
 TOTAL AREA 24.03

STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	23.37 ON SITE					
A	GREEN GRASS-GOOD	18.11		39	75	2925
	24 X 2479 = 59,496					
	42 X 4725 = 198,450					
	257,946		5.92	98	25	2450
TOTALS						5375

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

 PRODUCT COVERAGE =  $\bar{CN}$  = 54

$$S = \frac{1000}{CN} - 10$$

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

Q = runoff (in.)  
 P = rainfall (in.)

 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 19 TOTAL AREA 11.26 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - 6000	8.91		39	79	3081	
PUMT		24 X 1315 = 3,154						
RES		21 X 4725 = 99,225						
		102,381		2.35	98	21	2058	
TOTALS								5139

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 51

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 20 TOTAL AREA 8.70 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - 6000	6.95		39	80	3120	
RES		13 X 3750 = 48,750						
PUMT		24 X 1142 = 27,408						
		76,158		1.75	98	20	1960	
TOTALS								5080

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 51

$$S = \frac{1000}{CN} - 10$$

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

Q = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.



# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. <b>21</b>	TOTAL AREA <b>23.79</b>	STORM: <b>25</b> YEAR <b>96</b> HOUR				
SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<b>A GREEN GRASS - GOOD</b>	<b>16.50</b>		<b>39</b>	<b>69</b>	<b>2691</b>
<i>RES</i>	<i>65 X 3750 = 243,750</i>					
<i>PUMT</i>	<i>24 X 3077 = 73,848</i>					
	<u><b>317,598</b></u>		<b>7.29</b>	<b>98</b>	<b>31</b>	<b>3038</b>
TOTALS						<b>5721</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = **57**

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. <b>22</b>	ONSITE + OFFSITE TOTAL AREA <b>14.35</b> <del>16.50</del>	STORM: <b>25</b> YEAR <b>96</b> HOUR				
SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<b>13.43</b>					
	<b>A GREEN GRASS - GOOD</b>	<b>12.12</b>		<b>39</b>	<b>84</b>	<b>3274</b>
<i>RES</i>	<i>23 X 3750 = 1.98</i>					
<i>PUMT</i>	<i>24 X 450 = 0.25</i>					
	<u><b>2.23</b></u>		<b>2.23</b>	<b>98</b>	<b>16</b>	<b>1568</b>
TOTALS						<b>4844</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = **48**

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_

PRE-DEVELOPMENT  
 POST-DEVELOPMENT

BASIN NO. **23** *ON SITE + OFF SITE* TOTAL AREA **50.90** STORM: **25** YEAR **96** HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<i>38.13 ON</i> GREEN GRASS - GOOD	41.75		39	82	3198
<i>RES</i>	<i>65 X 4725 = 274,625</i>					
<i>PUMT</i>	<i>24 X 5166 = 123,984</i>					
	<i>398,609</i>		<i>9.15</i>	<i>98</i>	<i>18</i>	<i>1764</i>
TOTALS						<b>4962</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 50$

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. **24** *ON SITE + OFF SITE* TOTAL AREA **83.94** STORM: **25** YEAR **96** HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<i>56.64</i> <i>SAF ON</i> GREEN GRASS - GOOD	72.75		39	84	3276
<i>PUMT</i>	<i>24 X 5750 = 13.7</i>					
<i>RES (65')</i>	<i>78 X 3750 = 6.11</i>					
<i>RES (30')</i>	<i>38 X 4725 = 4.12</i>					
	<i>13.40</i>		<i>13.40</i>	<i>98</i>	<i>16</i>	<i>1568</i>
TOTALS						<b>4844</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 48$

$$S = \frac{1000}{CN} - 10$$

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

Q = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

ICPR INPUT DATA

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 1           Base Flow(cfs): 0           Init Stage(ft): 200  
Group: BASE        Length(ft): 0           Warn Stage(ft): 205  
Comment:

Stage(ft)	Area(ac)
200	0.257
201	0.345
202	0.444
203	0.551
204	0.676
205	0.807

-----Class: Node-----

Name: 10          Base Flow(cfs): 0           Init Stage(ft): 210  
Group: BASE        Length(ft): 0           Warn Stage(ft): 219  
Comment:

Stage(ft)	Area(ac)
210	0.093
211	0.178
212	0.37
213	0.706
214	1.089
215	1.268
216	1.412
217	1.558
218	1.727
219	1.934

-----Class: Node-----

Name: 11          Base Flow(cfs): 0           Init Stage(ft): 214  
Group: BASE        Length(ft): 0           Warn Stage(ft): 218  
Comment:

Stage(ft)	Area(ac)
214	0.5136
215	0.593
216	0.6747
217	0.7587
218	0.845

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 12            Base Flow(cfs): 0            Init Stage(ft): 205  
Group: BASE            Length(ft): 0            Warn Stage(ft): 216  
Comment:

Stage(ft)	Area(ac)
205	0.0414
206	0.0692
207	0.0994
208	0.1319
209	0.1667
210	0.2038
211	0.2433
212	0.285
213	0.329
214	0.4849
215	0.5685
216	0.6545

-----Class: Node-----

Name: 14            Base Flow(cfs): 0            Init Stage(ft): 234  
Group: BASE            Length(ft): 0            Warn Stage(ft): 238  
Comment:

Stage(ft)	Area(ac)
234	0.2709
235	0.3179
236	0.3673
237	0.419
238	0.473

-----Class: Node-----

Name: 15            Base Flow(cfs): 0            Init Stage(ft): 194  
Group: BASE            Length(ft): 0            Warn Stage(ft): 201  
Comment:

Stage(ft)	Area(ac)
194	0.366
195	0.458
196	0.615
197	0.746
198	0.886
199	1.071
200	1.236
201	1.406

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 16      Base Flow(cfs): 0      Init Stage(ft): 163  
Group: BASE      Length(ft): 0      Warn Stage(ft): 169

Comment:

Stage(ft)	Area(ac)
163	1.0387
164	1.1677
165	1.4637
166	1.6103
167	1.98
168	2.1693
169	2.3738

-----Class: Node-----

Name: 18      Base Flow(cfs): 0      Init Stage(ft): 165  
Group: BASE      Length(ft): 0      Warn Stage(ft): 171

Comment:

Stage(ft)	Area(ac)
165	1.261
166	1.466
167	1.714
168	1.975
169	2.351
170	2.705
171	3.31

-----Class: Node-----

Name: 19      Base Flow(cfs): 0      Init Stage(ft): 178  
Group: BASE      Length(ft): 0      Warn Stage(ft): 183

Comment:

Stage(ft)	Area(ac)
178	0.726
179	0.798
180	0.873
181	0.949
182	1.028
183	1.11

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 20      Base Flow(cfs): 0      Init Stage(ft): 191  
Group: BASE      Length(ft): 0      Warn Stage(ft): 196  
Comment:

Stage(ft)	Area(ac)
191	0.41
192	0.492
193	0.626
194	0.787
195	0.954
196	1.156

-----Class: Node-----

Name: 21      Base Flow(cfs): 0      Init Stage(ft): 185  
Group: BASE      Length(ft): 0      Warn Stage(ft): 196  
Comment:

Stage(ft)	Area(ac)
185	0.227
186	0.275
187	0.326
188	0.379
189	0.434
190	0.492
191	0.803
192	1.115
193	1.374
194	1.642
195	1.872
196	2.138

-----Class: Node-----

Name: 22      Base Flow(cfs): 0      Init Stage(ft): 169  
Group: BASE      Length(ft): 0      Warn Stage(ft): 176  
Comment:

Stage(ft)	Area(ac)
169	0.262
170	0.338
171	0.42
172	0.505
173	0.641
174	0.811
175	1.181
176	1.581

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 23           Base Flow(cfs): 0           Init Stage(ft): 130  
Group: BASE           Length(ft): 0           Warn Stage(ft): 150  
Comment:

Stage(ft)	Area(ac)
130	0.013
131	0.072
132	0.124
133	0.182
134	0.246
135	0.33
140	0.825
145	1.521
150	2.406

-----Class: Node-----

Name: 24           Base Flow(cfs): 0           Init Stage(ft): 112  
Group: BASE           Length(ft): 0           Warn Stage(ft): 119  
Comment:

Stage(ft)	Area(ac)
112	1.9
113	2.1
114	2.33
115	2.82
116	3.002
117	3.504
118	3.998
119	4.31

-----Class: Node-----

Name: 2A           Base Flow(cfs): 0           Init Stage(ft): 192  
Group: BASE           Length(ft): 0           Warn Stage(ft): 198  
Comment:

Stage(ft)	Area(ac)
192	0.1961
193	0.2407
194	0.2876
195	0.3368
196	0.3883
197	0.4421
198	0.4982



LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 2B           Base Flow(cfs): 0           Init Stage(ft): 182  
Group: BASE           Length(ft): 0           Warn Stage(ft): 185  
Comment:

Stage(ft)	Area(ac)
182	1.2315
183	1.3956
184	1.5621
185	1.7308

-----Class: Node-----

Name: 2C           Base Flow(cfs): 0           Init Stage(ft): 163  
Group: BASE           Length(ft): 0           Warn Stage(ft): 167  
Comment:

Stage(ft)	Area(ac)
163	0.605
164	0.693
165	0.782
166	1.05
167	1.357

-----Class: Node-----

Name: 3           Base Flow(cfs): 0           Init Stage(ft): 165  
Group: BASE           Length(ft): 0           Warn Stage(ft): 175  
Comment:

Stage(ft)	Area(ac)
165	0.595
166	0.685
167	0.779
168	0.879
169	0.987
170	1.102
171	1.226
172	1.354
173	1.489
174	1.824
175	1.987

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 4           Base Flow(cfs): 0           Init Stage(ft): 177  
Group: BASE        Length(ft): 0           Warn Stage(ft): 185  
Comment:

Stage(ft)	Area(ac)
177	0.729
178	0.846
179	0.971
180	1.102
181	1.231
182	1.363
183	1.614
184	2.041
185	2.704

-----Class: Node-----

Name: 6           Base Flow(cfs): 0           Init Stage(ft): 203  
Group: BASE        Length(ft): 0           Warn Stage(ft): 204  
Comment:

Stage(ft)	Area(ac)
203	1.294
204	1.4067

-----Class: Node-----

Name: 7           Base Flow(cfs): 0           Init Stage(ft): 149  
Group: BASE        Length(ft): 0           Warn Stage(ft): 170  
Comment:

Stage(ft)	Area(ac)
149	0.057
150	0.115
155	0.557
160	1.064
165	1.689
170	3.575

-----Class: Node-----

Name: 8           Base Flow(cfs): 0           Init Stage(ft): 235  
Group: BASE        Length(ft): 0           Warn Stage(ft): 240  
Comment:

Stage(ft)	Area(ac)
235	0.292
236	0.391
237	0.488
238	0.697
239	1.192
240	2.442

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 9            Base Flow(cfs): 0            Init Stage(ft): 236  
Group: BASE        Length(ft): 0            Warn Stage(ft): 240  
Comment:

Stage(ft)	Area(ac)
236	1.719
237	1.886
238	2.059
239	2.236
240	3.255

-----Class: Node-----

Name: 999         Base Flow(cfs): 0            Init Stage(ft): 195  
Group: BASE       Length(ft): 0            Warn Stage(ft): 200  
Comment:

Time(hrs)	Stage(ft)
30	196
60	197
96	198

-----Class: Basin-----

Basin: 1         Node: 1            Status: On Site    Type: Santa Barbara  
Group: BASE  
  Rainfall File: SJRWMD96        Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2        Lag Time(hrs): 0  
Time Increment(min): 15          Concentration Time(min): 15  
  Area(ac): 7.841                DCIA(%): 0  
  Curve #: 50

-----Class: Basin-----

Basin: 10        Node: 10           Status: On Site    Type: Santa Barbara  
Group: BASE  
  Rainfall File: SJRWMD96        Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2        Lag Time(hrs): 0  
Time Increment(min): 15          Concentration Time(min): 15  
  Area(ac): 13.602               DCIA(%): 0  
  Curve #: 53

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Basin-----  
Basin: 11      Node: 11      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 11.515      DCIA(%): 0  
    Curve #: 52

-----Class: Basin-----  
Basin: 12      Node: 12      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 14.39      DCIA(%): 0  
    Curve #: 53

-----Class: Basin-----  
Basin: 14      Node: 14      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 4.45      DCIA(%): 0  
    Curve #: 56

-----Class: Basin-----  
Basin: 15      Node: 15      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 16.368      DCIA(%): 0  
    Curve #: 51

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Basin-----  
Basin: 16          Node: 16          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2            Lag Time(hrs): 0  
Time Increment(min): 15              Concentration Time(min): 15  
    Area(ac): 17.157                  DCIA(%): 0  
    Curve #: 56

-----Class: Basin-----  
Basin: 17          Node: 17          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2            Lag Time(hrs): 0  
Time Increment(min): 15              Concentration Time(min): 15  
    Area(ac): 0.42                    DCIA(%): 0  
    Curve #: 39

-----Class: Basin-----  
Basin: 18          Node: 18          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2            Lag Time(hrs): 0  
Time Increment(min): 15              Concentration Time(min): 15  
    Area(ac): 23.369                  DCIA(%): 0  
    Curve #: 54

-----Class: Basin-----  
Basin: 19          Node: 19          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2            Lag Time(hrs): 0  
Time Increment(min): 15              Concentration Time(min): 15  
    Area(ac): 11.257                  DCIA(%): 0  
    Curve #: 51

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Basin-----  
Basin: 20          Node: 20          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2          Lag Time(hrs): 0  
Time Increment(min): 15          Concentration Time(min): 15  
    Area(ac): 8.699                  DCIA(%): 0  
    Curve #: 51

-----Class: Basin-----  
Basin: 21          Node: 21          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2          Lag Time(hrs): 0  
Time Increment(min): 15          Concentration Time(min): 15  
    Area(ac): 23.79                  DCIA(%): 0  
    Curve #: 57

-----Class: Basin-----  
Basin: 22          Node: 22          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2          Lag Time(hrs): 0  
Time Increment(min): 15          Concentration Time(min): 15  
    Area(ac): 14.35                  DCIA(%): 0  
    Curve #: 48

-----Class: Basin-----  
Basin: 23          Node: 23          Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96          Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2          Lag Time(hrs): 0  
Time Increment(min): 15          Concentration Time(min): 15  
    Area(ac): 50.9                  DCIA(%): 0  
    Curve #: 50

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Basin-----  
Basin: 24      Node: 24      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 86.15      DCIA(%): 0  
    Curve #: 48

-----Class: Basin-----  
Basin: 2A      Node: 2A      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 8.637      DCIA(%): 0  
    Curve #: 55

-----Class: Basin-----  
Basin: 2B      Node: 2B      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 18.74      DCIA(%): 0  
    Curve #: 54

-----Class: Basin-----  
Basin: 2C      Node: 2C      Status: On Site      Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96      Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2      Lag Time(hrs): 0  
Time Increment(min): 15      Concentration Time(min): 15  
    Area(ac): 14.836      DCIA(%): 0  
    Curve #: 49

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Basin-----  
Basin: 3           Node: 3           Status: On Site   Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96           Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2           Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 23.589           DCIA(%): 0  
    Curve #: 62

-----Class: Basin-----  
Basin: 4           Node: 4           Status: On Site   Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96           Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2           Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 18.387           DCIA(%): 0  
    Curve #: 48

-----Class: Basin-----  
Basin: 5           Node: 5           Status: On Site   Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96           Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2           Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 2.765           DCIA(%): 0  
    Curve #: 39

-----Class: Basin-----  
Basin: 6           Node: 6           Status: On Site   Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96           Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2           Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 10.474           DCIA(%): 0  
    Curve #: 39



LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Basin-----  
Basin: 7           Node: 7           Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96       Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2         Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 32.645               DCIA(%): 0  
    Curve #: 51

-----Class: Basin-----  
Basin: 8           Node: 8           Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96       Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2         Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 6.92                 DCIA(%): 0  
    Curve #: 45

-----Class: Basin-----  
Basin: 9           Node: 9           Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96       Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2         Lag Time(hrs): 0  
Time Increment(min): 15           Concentration Time(min): 15  
    Area(ac): 7.806                DCIA(%): 0  
    Curve #: 60

-----Class: Basin-----  
Basin: 999         Node: 999         Status: On Site    Type: Santa Barbara  
Group: BASE  
    Rainfall File: SJRWMD96       Storm Duration(hrs): 96  
Rainfall Amount(in): 11.2         Lag Time(hrs): 0  
Time Increment(min): 30           Concentration Time(min): 999  
    Area(ac): 2                    DCIA(%): 0  
    Curve #: 40

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Simulation-----

C:\ICPR2\DATA\LEGENDS

Execution: Hydraulics

Header: LEGENDS OF CLERMONT 25YR96HR STORM EVENT

-----HYDRAULICS-----HYDROLOGY-----

Max Delta Z (ft): 1

Delta Z Factor: 0.05           Override Defaults: No

Time Step Optimizer: 10

Drop Structure Optimizer: 10

Sim Start Time(hrs): 0

Sim End Time(hrs): 96

Min Calc Time(sec): 60

Max Calc Time(sec): 300

To Hour:   PInc(min):                   To Hour:   PInc(min):

96        60                            96        60

-----GROUP SELECTIONS-----

+ BASE    [09/23/98]

**ICPR NODE MAX CONDITIONS  
(STORMWATER ROUTING SUMMARY)  
25 YEAR-96 HOUR STORM**

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Maximum Conditions - LEGENDS \*\*\*\*\*

(Time units - hours)

Node Name	Group Name	Max Time Conditions	Max Stage (ft)	Warning Stage (ft)	Max Delta Stage (ft)	Max Surface Area (sf)	Max Time Inflow	Max Inflow (cfs)	Max Time Outflow	Max Outflow (cfs)
1	BASE	60.87	202.53	205.00	0.0431	21803.90	60.01	12.42	0.00	0.00
10	BASE	60.84	214.19	219.00	0.0513	48930.60	60.01	24.97	0.00	0.00
11	BASE	60.99	216.77	218.00	0.0458	32224.38	60.01	21.10	0.00	0.00
12	BASE	61.01	215.61	216.00	0.1196	27043.90	60.01	29.22	0.00	0.00
14	BASE	61.42	236.48	238.00	0.0393	17076.60	60.01	9.53	0.00	0.00
15	BASE	60.99	198.07	201.00	0.0609	39126.55	60.01	29.99	0.00	0.00
16	BASE	60.89	165.00	169.00	0.0366	63785.19	60.01	31.93	0.00	0.00
18	BASE	60.86	166.99	171.00	0.0366	74586.89	60.01	39.72	0.00	0.00
19	BASE	61.01	180.02	183.00	0.0338	38081.62	60.01	19.70	0.00	0.00
20	BASE	60.97	193.36	196.00	0.0393	29794.57	60.01	15.33	0.00	0.00
21	BASE	61.91	193.52	196.00	0.1230	65924.40	60.01	55.42	0.00	0.00
22	BASE	61.47	173.68	176.00	0.0695	32948.25	60.01	24.87	0.00	0.00
23	BASE	62.47	145.31	150.00	0.1397	68683.30	60.01	98.66	0.00	0.00
24	BASE	61.37	116.83	119.00	0.0745	148969.49	60.01	144.61	0.00	0.00
2A	BASE	61.21	197.07	198.00	0.0753	19427.48	60.01	18.42	0.00	0.00
2B	BASE	60.92	183.91	185.00	0.0334	67413.96	60.01	33.97	0.00	0.00
2C	BASE	62.55	166.66	167.00	-0.0496	54557.99	60.01	28.16	0.00	0.00
3	BASE	61.66	171.12	175.00	0.0882	54073.75	60.01	60.27	0.00	0.00
4	BASE	60.91	179.38	185.00	0.0420	44466.78	60.01	27.02	0.00	0.00
6	BASE	60.71	203.24	204.00	-0.0096	57565.80	60.01	5.63	0.00	0.00
7	BASE	60.52	155.62	170.00	0.0809	26995.99	60.01	29.56	0.00	0.00
8	BASE	60.99	237.05	240.00	0.0334	21692.22	60.01	9.83	0.00	0.00
9	BASE	96.02	238.14	240.00	0.0154	90804.87	60.01	20.74	0.00	0.00
999	BASE	96.02	198.00	200.00	1.0000	0.00	64.00	0.17	0.00	0.00

**ICPR ROUTED HYDROGRAPH  
BY BASIN  
WITH INFILTRATION INPUTED FROM "PONDS"**

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!				Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)		
*** Group: BASE		Node: 1						
0.000	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
1.050	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
2.019	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
3.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
4.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
5.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
6.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
7.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
8.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
9.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
10.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
11.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
12.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
13.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
14.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
15.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
16.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
17.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
18.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
19.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
20.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
21.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
22.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
23.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
24.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
25.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
26.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
27.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
28.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
29.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
30.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
31.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
32.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
33.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
34.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
35.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
36.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
37.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
38.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
39.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
40.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
41.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
42.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
43.014	200.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
44.014	200.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
45.014	200.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
46.014	200.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
47.003	200.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
48.035	200.00	0.00	0.00	0.02	-0.03	0.00	0.00	0.00	
49.022	200.00	0.26	0.00	0.04	-0.04	0.00	0.00	0.00	
50.017	200.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
51.031	200.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
52.025	200.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00	
53.030	200.00	0.00	0.00	0.13	-0.13	0.00	0.00	0.00	
54.008	200.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
55.018	200.00	0.00	0.00	0.21	-0.22	0.00	0.00	0.00	
56.035	200.00	0.00	0.00	0.29	-0.31	0.00	0.00	0.00	
57.032	200.00	0.00	0.00	0.43	-0.45	0.00	0.00	0.00	
58.009	200.00	0.00	0.00	0.62	-0.75	0.00	0.00	0.00	
59.001	199.99	0.00	0.00	1.32	-1.84	0.00	0.00	0.00	
60.005	201.54	0.40	0.00	15.87	-3.46	0.00	0.00	0.00	
61.005	202.51	0.50	0.00	2.80	-4.71	0.00	0.00	0.00	
62.005	202.05	0.45	0.00	1.65	-4.93	0.00	0.00	0.00	
63.016	201.42	0.39	0.00	1.20	-4.28	0.00	0.00	0.00	
64.031	200.77	0.32	0.00	1.04	-3.41	0.00	0.00	0.00	
65.024	200.31	0.28	0.00	0.74	-1.82	0.00	0.00	0.00	
66.031	200.15	0.27	0.00	0.74	-0.74	0.00	0.00	0.00	
67.049	200.15	0.27	0.00	0.75	-0.72	0.00	0.00	0.00	
68.034	200.16	0.27	0.00	0.66	-0.65	0.00	0.00	0.00	
69.067	200.16	0.27	0.00	0.51	-0.55	0.00	0.00	0.00	
70.021	200.15	0.27	0.00	0.51	-0.51	0.00	0.00	0.00	
71.054	200.16	0.27	0.00	0.51	-0.49	0.00	0.00	0.00	
72.008	200.16	0.27	0.00	0.43	-0.41	0.00	0.00	0.00	
73.041	200.16	0.27	0.00	0.27	-0.31	0.00	0.00	0.00	
74.074	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
75.028	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
76.061	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
77.014	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
78.048	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
79.001	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
80.034	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
81.010	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
82.028	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
83.004	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
84.062	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
85.063	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
86.048	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
87.048	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
88.048	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
89.048	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
90.048	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	

91.048	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00
92.048	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!				Link Q (cfs)	Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)			
93.031	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
94.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
95.007	200.16	0.27	0.00	0.28	-0.25	0.00	0.00	0.00	
96.021	200.19	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	200.19	0.27	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 10

0.000	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
1.050	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
2.019	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
3.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
4.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
5.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
6.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
7.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
8.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
9.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
10.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
11.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
12.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
13.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
14.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
15.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
16.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
17.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
18.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
19.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
20.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
21.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
22.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
23.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
24.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
25.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
26.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
27.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
28.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
29.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
30.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
31.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
32.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
33.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
34.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
35.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
36.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
37.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00

38.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
39.014	210.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Q (cfs)	Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)			
40.014	210.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	
41.014	210.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	
42.014	210.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	0.00	
43.014	210.00	0.09	0.00	0.02	-0.02	0.00	0.00	0.00	0.00	
44.014	210.00	0.09	0.00	0.04	-0.03	0.00	0.00	0.00	0.00	
45.014	210.00	0.09	0.00	0.05	-0.05	0.00	0.00	0.00	0.00	
46.014	210.00	0.09	0.00	0.06	-0.06	0.00	0.00	0.00	0.00	
47.003	210.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	0.00	
48.035	210.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00	0.00	
49.022	210.00	0.09	0.00	0.13	-0.13	0.00	0.00	0.00	0.00	
50.017	210.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	0.00	
51.031	210.00	0.00	0.00	0.20	-0.20	0.00	0.00	0.00	0.00	
52.025	210.00	0.00	0.00	0.24	-0.25	0.00	0.00	0.00	0.00	
53.030	210.00	0.09	0.00	0.31	-0.31	0.00	0.00	0.00	0.00	
54.008	210.00	0.00	0.00	0.38	-0.39	0.00	0.00	0.00	0.00	
55.018	210.00	0.00	0.00	0.49	-0.50	0.00	0.00	0.00	0.00	
56.035	210.00	0.00	0.00	0.64	-0.67	0.00	0.00	0.00	0.00	
57.032	210.02	0.09	0.00	0.93	-0.86	0.00	0.00	0.00	0.00	
58.009	210.17	0.11	0.00	1.30	-1.00	0.00	0.00	0.00	0.00	
59.001	210.69	0.15	0.00	2.69	-1.31	0.00	0.00	0.00	0.00	
60.005	213.33	0.83	0.00	30.25	-5.28	0.00	0.00	0.00	0.00	
61.005	214.16	1.12	0.00	5.23	-10.14	0.00	0.00	0.00	0.00	
62.005	213.68	0.97	0.00	3.07	-10.42	0.00	0.00	0.00	0.00	
63.016	213.02	0.71	0.00	2.21	-8.16	0.00	0.00	0.00	0.00	
64.031	212.35	0.49	0.00	1.92	-5.61	0.00	0.00	0.00	0.00	
65.024	211.72	0.32	0.00	1.37	-3.65	0.00	0.00	0.00	0.00	
66.031	211.22	0.22	0.00	1.37	-2.35	0.00	0.00	0.00	0.00	
67.049	210.93	0.17	0.00	1.37	-1.73	0.00	0.00	0.00	0.00	
68.034	210.76	0.16	0.00	1.22	-1.54	0.00	0.00	0.00	0.00	
69.067	210.55	0.14	0.00	0.93	-1.36	0.00	0.00	0.00	0.00	
70.021	210.35	0.12	0.00	0.93	-1.16	0.00	0.00	0.00	0.00	
71.054	210.25	0.11	0.00	0.93	-0.97	0.00	0.00	0.00	0.00	
72.008	210.24	0.11	0.00	0.79	-0.77	0.00	0.00	0.00	0.00	
73.041	210.22	0.11	0.00	0.49	-0.56	0.00	0.00	0.00	0.00	
74.074	210.19	0.11	0.00	0.49	-0.49	0.00	0.00	0.00	0.00	
75.028	210.19	0.11	0.00	0.49	-0.49	0.00	0.00	0.00	0.00	
76.061	210.19	0.11	0.00	0.49	-0.49	0.00	0.00	0.00	0.00	
77.014	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
78.048	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
79.001	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
80.034	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
81.010	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
82.028	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
83.004	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	
84.062	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	0.00	

85.063	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00
86.048	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
87.048	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
88.048	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
89.048	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
90.048	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
91.048	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
92.048	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
93.031	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
94.005	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
95.007	210.21	0.11	0.00	0.51	-0.46	0.00	0.00	0.00	
96.021	210.34	0.12	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	210.34	0.12	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 11

0.000	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
1.050	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
2.019	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
3.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
4.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
5.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
6.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
7.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
8.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
9.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
10.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
11.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
12.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
13.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
14.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
15.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
16.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
17.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
18.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
19.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
20.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
21.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
22.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
23.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
24.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
25.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
26.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
27.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
28.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
29.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
30.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
31.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00

32.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00
33.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
34.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	214.00	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	214.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
42.014	214.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
43.014	214.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
44.014	214.00	0.51	0.00	0.02	-0.02	0.00	0.00	0.00	
45.014	214.00	0.51	0.00	0.03	-0.03	0.00	0.00	0.00	
46.014	214.00	0.51	0.00	0.04	-0.04	0.00	0.00	0.00	
47.003	214.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
48.035	214.00	0.00	0.00	0.06	-0.07	0.00	0.00	0.00	
49.022	214.00	0.51	0.00	0.09	-0.09	0.00	0.00	0.00	
50.017	214.00	0.00	0.00	0.11	-0.12	0.00	0.00	0.00	
51.031	214.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	
52.025	214.00	0.00	0.00	0.18	-0.19	0.00	0.00	0.00	
53.030	214.00	0.51	0.00	0.24	-0.24	0.00	0.00	0.00	
54.008	214.00	0.00	0.00	0.29	-0.30	0.00	0.00	0.00	
55.018	214.00	0.00	0.00	0.38	-0.39	0.00	0.00	0.00	
56.035	214.00	0.00	0.00	0.50	-0.53	0.00	0.00	0.00	
57.032	214.00	0.00	0.00	0.73	-0.76	0.00	0.00	0.00	
58.009	214.00	0.00	0.00	1.04	-1.24	0.00	0.00	0.00	
59.001	214.00	0.00	0.00	2.16	-2.48	0.00	0.00	0.00	
60.005	215.52	0.64	0.00	24.85	-3.76	0.00	0.00	0.00	
61.005	216.77	0.74	0.00	4.33	-4.49	0.00	0.00	0.00	
62.005	216.64	0.73	0.00	2.54	-4.79	0.00	0.00	0.00	
63.016	216.34	0.70	0.00	1.84	-4.66	0.00	0.00	0.00	
64.031	216.00	0.67	0.00	1.60	-4.48	0.00	0.00	0.00	
65.024	215.62	0.64	0.00	1.14	-4.28	0.00	0.00	0.00	
66.031	215.22	0.61	0.00	1.14	-4.07	0.00	0.00	0.00	
67.049	214.82	0.58	0.00	1.14	-3.85	0.00	0.00	0.00	
68.034	214.44	0.55	0.00	1.01	-3.44	0.00	0.00	0.00	
69.067	214.16	0.53	0.00	0.78	-1.92	0.00	0.00	0.00	
70.021	214.08	0.52	0.00	0.78	-0.78	0.00	0.00	0.00	
71.054	214.08	0.52	0.00	0.77	-0.74	0.00	0.00	0.00	
72.008	214.09	0.52	0.00	0.65	-0.62	0.00	0.00	0.00	
73.041	214.08	0.52	0.00	0.41	-0.47	0.00	0.00	0.00	
74.074	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	
75.028	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	
76.061	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	
77.014	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	
78.048	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	

79.001	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00
80.034	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
81.010	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	
82.028	214.08	0.52	0.00	0.41	-0.41	0.00	0.00	0.00	
83.004	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
84.062	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
85.063	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
86.048	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
87.048	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
88.048	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
89.048	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
90.048	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
91.048	214.08	0.52	0.00	0.43	-0.43	0.00	0.00	0.00	
92.048	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
93.031	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
94.005	214.08	0.52	0.00	0.42	-0.42	0.00	0.00	0.00	
95.007	214.08	0.52	0.00	0.42	-0.39	0.00	0.00	0.00	
96.021	214.11	0.52	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	214.11	0.52	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 12

0.000	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
1.050	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
2.019	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
3.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
4.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
5.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
6.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
7.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
8.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
9.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
10.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
11.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
12.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
13.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
14.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
15.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
16.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
17.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
18.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
19.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
20.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
21.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
22.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
23.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
24.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
25.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00

26.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00
27.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
28.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	205.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	205.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	205.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
41.014	205.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
42.014	205.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
43.014	205.00	0.04	0.00	0.02	-0.02	0.00	0.00	0.00	
44.014	205.00	0.04	0.00	0.04	-0.04	0.00	0.00	0.00	
45.014	205.00	0.04	0.00	0.05	-0.05	0.00	0.00	0.00	
46.014	205.00	0.04	0.00	0.06	-0.06	0.00	0.00	0.00	
47.003	205.00	0.00	0.00	0.07	-0.08	0.00	0.00	0.00	
48.035	205.00	0.00	0.00	0.10	-0.10	0.00	0.00	0.00	
49.022	205.00	0.04	0.00	0.14	-0.13	0.00	0.00	0.00	
50.017	205.00	0.00	0.00	0.17	-0.17	0.00	0.00	0.00	
51.031	205.00	0.00	0.00	0.21	-0.21	0.00	0.00	0.00	
52.025	205.00	0.00	0.00	0.26	-0.26	0.00	0.00	0.00	
53.030	205.00	0.04	0.00	0.33	-0.33	0.00	0.00	0.00	
54.008	205.00	0.00	0.00	0.40	-0.41	0.00	0.00	0.00	
55.018	205.05	0.04	0.00	0.51	-0.46	0.00	0.00	0.00	
56.035	205.26	0.05	0.00	0.68	-0.50	0.00	0.00	0.00	
57.032	205.68	0.06	0.00	0.98	-0.61	0.00	0.00	0.00	
58.009	206.26	0.08	0.00	1.38	-0.77	0.00	0.00	0.00	
59.001	207.31	0.11	0.00	2.85	-1.05	0.00	0.00	0.00	
60.005	213.27	0.37	0.00	32.00	-2.78	0.00	0.00	0.00	
61.005	215.61	0.62	0.00	5.53	-5.63	0.00	0.00	0.00	
62.005	215.36	0.60	0.00	3.25	-6.78	0.00	0.00	0.00	
63.016	214.81	0.55	0.00	2.34	-6.37	0.00	0.00	0.00	
64.031	214.12	0.50	0.00	2.04	-6.60	0.00	0.00	0.00	
65.024	213.41	0.39	0.00	1.45	-4.66	0.00	0.00	0.00	
66.031	212.99	0.33	0.00	1.45	-1.94	0.00	0.00	0.00	
67.049	212.91	0.33	0.00	1.45	-1.55	0.00	0.00	0.00	
68.034	212.90	0.32	0.00	1.29	-1.34	0.00	0.00	0.00	
69.067	212.86	0.32	0.00	0.99	-1.20	0.00	0.00	0.00	
70.021	212.82	0.32	0.00	0.99	-1.10	0.00	0.00	0.00	
71.054	212.80	0.32	0.00	0.98	-1.02	0.00	0.00	0.00	
72.008	212.78	0.32	0.00	0.83	-0.96	0.00	0.00	0.00	

73.041	212.71	0.32	0.00	0.52	-0.89	0.00	0.00	0.00
74.074	212.62	0.31	0.00	0.52	-0.83	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
75.028	212.55	0.31	0.00	0.52	-0.79	0.00	0.00	0.00	
76.061	212.48	0.31	0.00	0.52	-0.75	0.00	0.00	0.00	
77.014	212.42	0.30	0.00	0.53	-0.73	0.00	0.00	0.00	
78.048	212.37	0.30	0.00	0.53	-0.70	0.00	0.00	0.00	
79.001	212.33	0.30	0.00	0.53	-0.68	0.00	0.00	0.00	
80.034	212.29	0.30	0.00	0.53	-0.66	0.00	0.00	0.00	
81.010	212.25	0.30	0.00	0.53	-0.64	0.00	0.00	0.00	
82.028	212.22	0.29	0.00	0.53	-0.63	0.00	0.00	0.00	
83.004	212.20	0.29	0.00	0.53	-0.61	0.00	0.00	0.00	
84.062	212.17	0.29	0.00	0.53	-0.60	0.00	0.00	0.00	
85.063	212.16	0.29	0.00	0.53	-0.59	0.00	0.00	0.00	
86.048	212.14	0.29	0.00	0.53	-0.58	0.00	0.00	0.00	
87.048	212.13	0.29	0.00	0.53	-0.57	0.00	0.00	0.00	
88.048	212.12	0.29	0.00	0.53	-0.56	0.00	0.00	0.00	
89.048	212.11	0.29	0.00	0.54	-0.55	0.00	0.00	0.00	
90.048	212.11	0.29	0.00	0.54	-0.55	0.00	0.00	0.00	
91.048	212.11	0.29	0.00	0.54	-0.54	0.00	0.00	0.00	
92.048	212.11	0.29	0.00	0.54	-0.53	0.00	0.00	0.00	
93.031	212.11	0.29	0.00	0.54	-0.53	0.00	0.00	0.00	
94.005	212.12	0.29	0.00	0.54	-0.52	0.00	0.00	0.00	
95.007	212.12	0.29	0.00	0.54	-0.51	0.00	0.00	0.00	
96.021	212.17	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	212.17	0.29	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 14

0.000	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
1.050	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
2.019	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
3.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
4.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
5.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
6.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
7.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
8.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
9.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
10.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
11.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
12.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
13.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
14.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
15.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
16.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
17.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
18.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
19.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00

20.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00
21.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
22.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	234.00	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	234.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
37.014	234.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
38.014	234.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	234.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	234.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
41.014	234.00	0.27	0.00	0.01	-0.01	0.00	0.00	0.00	
42.014	234.00	0.27	0.00	0.02	-0.02	0.00	0.00	0.00	
43.014	234.00	0.27	0.00	0.02	-0.02	0.00	0.00	0.00	
44.014	234.00	0.27	0.00	0.03	-0.03	0.00	0.00	0.00	
45.014	234.00	0.27	0.00	0.03	-0.03	0.00	0.00	0.00	
46.014	234.00	0.27	0.00	0.03	-0.03	0.00	0.00	0.00	
47.003	234.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
48.035	234.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
49.022	234.00	0.27	0.00	0.06	-0.06	0.00	0.00	0.00	
50.017	234.00	0.27	0.00	0.07	-0.07	0.00	0.00	0.00	
51.031	234.00	0.00	0.00	0.09	-0.09	0.00	0.00	0.00	
52.025	234.00	0.00	0.00	0.11	-0.11	0.00	0.00	0.00	
53.030	234.00	0.27	0.00	0.13	-0.13	0.00	0.00	0.00	
54.008	234.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
55.018	234.00	0.00	0.00	0.20	-0.20	0.00	0.00	0.00	
56.035	234.00	0.00	0.00	0.26	-0.27	0.00	0.00	0.00	
57.032	234.00	0.00	0.00	0.36	-0.37	0.00	0.00	0.00	
58.009	234.00	0.00	0.00	0.50	-0.59	0.00	0.00	0.00	
59.001	234.01	0.27	0.00	1.01	-0.92	0.00	0.00	0.00	
60.005	235.34	0.33	0.00	10.75	-1.22	0.00	0.00	0.00	
61.005	236.46	0.39	0.00	1.82	-1.46	0.00	0.00	0.00	
62.005	236.45	0.39	0.00	1.06	-1.57	0.00	0.00	0.00	
63.016	236.31	0.38	0.00	0.77	-1.55	0.00	0.00	0.00	
64.031	236.12	0.37	0.00	0.67	-1.52	0.00	0.00	0.00	
65.024	235.92	0.36	0.00	0.47	-1.48	0.00	0.00	0.00	
66.031	235.69	0.35	0.00	0.47	-1.45	0.00	0.00	0.00	

67.049	235.39	0.34	0.00	0.47	-1.88	0.00	0.00	0.00
68.034	235.07	0.32	0.00	0.42	-1.58	0.00	0.00	0.00





14.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
15.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
16.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	194.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
43.014	194.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
44.014	194.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
45.014	194.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	
46.014	194.00	0.37	0.00	0.03	-0.03	0.00	0.00	0.00	
47.003	194.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
48.035	194.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
49.022	194.00	0.37	0.00	0.10	-0.10	0.00	0.00	0.00	
50.017	194.00	0.00	0.00	0.14	-0.14	0.00	0.00	0.00	
51.031	194.00	0.00	0.00	0.18	-0.18	0.00	0.00	0.00	
52.025	194.00	0.00	0.00	0.23	-0.23	0.00	0.00	0.00	
53.030	194.00	0.37	0.00	0.30	-0.30	0.00	0.00	0.00	
54.008	194.00	0.00	0.00	0.37	-0.38	0.00	0.00	0.00	
55.018	194.00	0.00	0.00	0.49	-0.50	0.00	0.00	0.00	
56.035	194.00	0.00	0.00	0.66	-0.69	0.00	0.00	0.00	
57.032	194.00	0.00	0.00	0.97	-1.00	0.00	0.00	0.00	
58.009	194.00	0.00	0.00	1.38	-1.65	0.00	0.00	0.00	
59.001	194.02	0.37	0.00	2.91	-2.54	0.00	0.00	0.00	
60.005	196.52	0.68	0.00	34.24	-4.25	0.00	0.00	0.00	

61.005	198.07	0.90	0.00	6.00	-6.39	0.00	0.00	0.00
62.005	197.88	0.87	0.00	3.53	-7.11	0.00	0.00	0.00

LEGENDS OF CLEARMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
63.016	197.49	0.82	0.00	2.56	-6.74	0.00	0.00	0.00	
64.031	197.06	0.75	0.00	2.22	-6.31	0.00	0.00	0.00	
65.024	196.49	0.68	0.00	1.58	-7.27	0.00	0.00	0.00	
66.031	195.89	0.60	0.00	1.59	-5.05	0.00	0.00	0.00	
67.049	195.66	0.56	0.00	1.59	-1.49	0.00	0.00	0.00	
68.034	195.69	0.57	0.00	1.41	-1.19	0.00	0.00	0.00	
69.067	195.71	0.57	0.00	1.08	-1.02	0.00	0.00	0.00	
70.021	195.72	0.57	0.00	1.08	-0.92	0.00	0.00	0.00	
71.054	195.75	0.58	0.00	1.08	-0.85	0.00	0.00	0.00	
72.008	195.78	0.58	0.00	0.91	-0.79	0.00	0.00	0.00	
73.041	195.77	0.58	0.00	0.57	-0.72	0.00	0.00	0.00	
74.074	195.76	0.58	0.00	0.57	-0.67	0.00	0.00	0.00	
75.028	195.74	0.57	0.00	0.57	-0.64	0.00	0.00	0.00	
76.061	195.74	0.57	0.00	0.57	-0.61	0.00	0.00	0.00	
77.014	195.73	0.57	0.00	0.58	-0.59	0.00	0.00	0.00	
78.048	195.73	0.57	0.00	0.58	-0.56	0.00	0.00	0.00	
79.001	195.74	0.57	0.00	0.58	-0.55	0.00	0.00	0.00	
80.034	195.74	0.57	0.00	0.58	-0.53	0.00	0.00	0.00	
81.010	195.75	0.58	0.00	0.58	-0.52	0.00	0.00	0.00	
82.028	195.76	0.58	0.00	0.58	-0.51	0.00	0.00	0.00	
83.004	195.77	0.58	0.00	0.58	-0.50	0.00	0.00	0.00	
84.062	195.78	0.58	0.00	0.58	-0.49	0.00	0.00	0.00	
85.063	195.80	0.58	0.00	0.58	-0.48	0.00	0.00	0.00	
86.048	195.81	0.59	0.00	0.58	-0.47	0.00	0.00	0.00	
87.048	195.83	0.59	0.00	0.59	-0.47	0.00	0.00	0.00	
88.048	195.85	0.59	0.00	0.59	-0.46	0.00	0.00	0.00	
89.048	195.87	0.59	0.00	0.59	-0.45	0.00	0.00	0.00	
90.048	195.88	0.60	0.00	0.59	-0.45	0.00	0.00	0.00	
91.048	195.90	0.60	0.00	0.59	-0.45	0.00	0.00	0.00	
92.048	195.93	0.60	0.00	0.59	-0.44	0.00	0.00	0.00	
93.031	195.95	0.61	0.00	0.59	-0.44	0.00	0.00	0.00	
94.005	195.97	0.61	0.00	0.59	-0.43	0.00	0.00	0.00	
95.007	195.99	0.61	0.00	0.59	-0.42	0.00	0.00	0.00	
96.021	196.03	0.62	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	196.03	0.62	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 16

0.000	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
1.050	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
2.019	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
3.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
4.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
5.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
6.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00
7.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
10.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	163.00	1.04	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
37.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
38.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	163.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
40.014	163.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
41.014	163.00	1.04	0.00	0.05	-0.05	0.00	0.00	0.00	
42.014	163.00	1.04	0.00	0.07	-0.07	0.00	0.00	0.00	
43.014	163.00	1.04	0.00	0.09	-0.09	0.00	0.00	0.00	
44.014	163.00	1.04	0.00	0.10	-0.10	0.00	0.00	0.00	
45.014	163.00	1.04	0.00	0.12	-0.12	0.00	0.00	0.00	
46.014	163.00	1.04	0.00	0.13	-0.13	0.00	0.00	0.00	
47.003	163.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	
48.035	163.00	0.00	0.00	0.18	-0.19	0.00	0.00	0.00	
49.022	163.00	1.04	0.00	0.24	-0.24	0.00	0.00	0.00	
50.017	163.00	1.04	0.00	0.28	-0.29	0.00	0.00	0.00	
51.031	163.00	0.00	0.00	0.34	-0.35	0.00	0.00	0.00	
52.025	163.00	0.00	0.00	0.41	-0.42	0.00	0.00	0.00	
53.030	163.00	1.04	0.00	0.51	-0.51	0.00	0.00	0.00	
54.008	163.00	0.00	0.00	0.60	-0.62	0.00	0.00	0.00	

55.018	163.00	0.00	0.00	0.76	-0.78	0.00	0.00	0.00
56.035	163.00	0.00	0.00	0.99	-1.04	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow				Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)		
57.032	163.00	0.00	0.00	1.40	-1.44	0.00	0.00	0.00
58.009	163.00	0.00	0.00	1.93	-2.30	0.00	0.00	0.00
59.001	162.99	0.00	0.00	3.90	-5.90	0.00	0.00	0.00
60.005	164.14	1.21	0.00	41.44	-9.51	0.00	0.00	0.00
61.005	164.99	1.46	0.00	7.03	-11.24	0.00	0.00	0.00
62.005	164.64	1.36	0.00	4.10	-11.85	0.00	0.00	0.00
63.016	164.13	1.21	0.00	2.95	-10.66	0.00	0.00	0.00
64.031	163.61	1.12	0.00	2.56	-9.09	0.00	0.00	0.00
65.024	163.25	1.07	0.00	1.82	-5.04	0.00	0.00	0.00
66.031	163.13	1.06	0.00	1.82	-1.82	0.00	0.00	0.00
67.049	163.13	1.06	0.00	1.82	-1.77	0.00	0.00	0.00
68.034	163.13	1.06	0.00	1.62	-1.58	0.00	0.00	0.00
69.067	163.13	1.06	0.00	1.24	-1.33	0.00	0.00	0.00
70.021	163.13	1.06	0.00	1.24	-1.24	0.00	0.00	0.00
71.054	163.13	1.06	0.00	1.23	-1.18	0.00	0.00	0.00
72.008	163.13	1.06	0.00	1.04	-0.99	0.00	0.00	0.00
73.041	163.13	1.06	0.00	0.65	-0.75	0.00	0.00	0.00
74.074	163.13	1.06	0.00	0.65	-0.65	0.00	0.00	0.00
75.028	163.13	1.06	0.00	0.65	-0.65	0.00	0.00	0.00
76.061	163.13	1.06	0.00	0.65	-0.65	0.00	0.00	0.00
77.014	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
78.048	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
79.001	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
80.034	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
81.010	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
82.028	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
83.004	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
84.062	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
85.063	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
86.048	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
87.048	163.13	1.06	0.00	0.66	-0.66	0.00	0.00	0.00
88.048	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
89.048	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
90.048	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
91.048	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
92.048	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
93.031	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
94.005	163.13	1.06	0.00	0.67	-0.67	0.00	0.00	0.00
95.007	163.13	1.06	0.00	0.67	-0.61	0.00	0.00	0.00
96.021	163.15	1.06	0.00	0.00	0.00	0.00	0.00	0.00
96.054	163.15	1.06	0.00	0.00	0.00	0.00	0.00	0.00

\*\*\* Group: BASE Node: 18  
 0.000 165.00 1.26 0.00 0.00 0.00 0.00 0.00 0.00  
 1.050 165.00 1.26 0.00 0.00 0.00 0.00 0.00 0.00

2.019	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00
3.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)			
4.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	
39.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	
40.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	
41.014	165.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	0.00	
42.014	165.00	1.26	0.00	0.04	-0.04	0.00	0.00	0.00	0.00	
43.014	165.00	1.26	0.00	0.07	-0.06	0.00	0.00	0.00	0.00	
44.014	165.00	1.26	0.00	0.09	-0.09	0.00	0.00	0.00	0.00	
45.014	165.00	1.26	0.00	0.11	-0.11	0.00	0.00	0.00	0.00	
46.014	165.00	1.26	0.00	0.13	-0.13	0.00	0.00	0.00	0.00	
47.003	165.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	0.00	
48.035	165.00	0.00	0.00	0.19	-0.19	0.00	0.00	0.00	0.00	

49.022	165.00	1.26	0.00	0.26	-0.25	0.00	0.00	0.00
50.017	165.00	1.26	0.00	0.31	-0.31	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
51.031	165.00	0.00	0.00	0.38	-0.38	0.00	0.00	0.00	
52.025	165.00	0.00	0.00	0.46	-0.47	0.00	0.00	0.00	
53.030	165.00	1.26	0.00	0.59	-0.59	0.00	0.00	0.00	
54.008	165.00	0.00	0.00	0.70	-0.72	0.00	0.00	0.00	
55.018	165.00	0.00	0.00	0.90	-0.92	0.00	0.00	0.00	
56.035	165.00	0.00	0.00	1.18	-1.24	0.00	0.00	0.00	
57.032	165.00	0.00	0.00	1.70	-1.75	0.00	0.00	0.00	
58.009	165.00	0.00	0.00	2.37	-2.84	0.00	0.00	0.00	
59.001	164.99	0.00	0.00	4.85	-8.15	0.00	0.00	0.00	
60.005	166.12	1.50	0.00	53.48	-13.76	0.00	0.00	0.00	
61.005	166.97	1.71	0.00	9.18	-15.88	0.00	0.00	0.00	
62.005	166.53	1.60	0.00	5.38	-16.35	0.00	0.00	0.00	
63.016	165.92	1.45	0.00	3.88	-14.93	0.00	0.00	0.00	
64.031	165.41	1.34	0.00	3.37	-9.30	0.00	0.00	0.00	
65.024	165.19	1.30	0.00	2.39	-3.51	0.00	0.00	0.00	
66.031	165.16	1.29	0.00	2.40	-2.40	0.00	0.00	0.00	
67.049	165.16	1.29	0.00	2.40	-2.33	0.00	0.00	0.00	
68.034	165.17	1.29	0.00	2.13	-2.08	0.00	0.00	0.00	
69.067	165.16	1.29	0.00	1.63	-1.75	0.00	0.00	0.00	
70.021	165.16	1.29	0.00	1.63	-1.63	0.00	0.00	0.00	
71.054	165.16	1.29	0.00	1.62	-1.56	0.00	0.00	0.00	
72.008	165.17	1.29	0.00	1.37	-1.31	0.00	0.00	0.00	
73.041	165.16	1.29	0.00	0.86	-0.98	0.00	0.00	0.00	
74.074	165.16	1.29	0.00	0.86	-0.86	0.00	0.00	0.00	
75.028	165.16	1.29	0.00	0.86	-0.86	0.00	0.00	0.00	
76.061	165.16	1.29	0.00	0.86	-0.86	0.00	0.00	0.00	
77.014	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
78.048	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
79.001	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
80.034	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
81.010	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
82.028	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
83.004	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
84.062	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
85.063	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
86.048	165.16	1.29	0.00	0.88	-0.88	0.00	0.00	0.00	
87.048	165.16	1.29	0.00	0.88	-0.88	0.00	0.00	0.00	
88.048	165.16	1.29	0.00	0.88	-0.88	0.00	0.00	0.00	
89.048	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
90.048	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
91.048	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
92.048	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
93.031	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
94.005	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
95.007	165.16	1.29	0.00	0.89	-0.81	0.00	0.00	0.00	



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
*** Group: BASE Node: 19									
0.000	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
1.050	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
2.019	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
3.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
4.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	178.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
43.014	178.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	

44.014	178.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00
45.014	178.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
46.014	178.00	0.73	0.00	0.02	-0.02	0.00	0.00	0.00	
47.003	178.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
48.035	178.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
49.022	178.00	0.73	0.00	0.07	-0.07	0.00	0.00	0.00	
50.017	178.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00	
51.031	178.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
52.025	178.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
53.030	178.00	0.73	0.00	0.21	-0.21	0.00	0.00	0.00	
54.008	178.00	0.00	0.00	0.26	-0.26	0.00	0.00	0.00	
55.018	178.00	0.00	0.00	0.34	-0.34	0.00	0.00	0.00	
56.035	178.00	0.00	0.00	0.45	-0.48	0.00	0.00	0.00	
57.032	178.00	0.00	0.00	0.67	-0.69	0.00	0.00	0.00	
58.009	178.00	0.00	0.00	0.95	-1.14	0.00	0.00	0.00	
59.001	178.00	0.00	0.00	2.00	-2.56	0.00	0.00	0.00	
60.005	179.05	0.80	0.00	23.55	-3.84	0.00	0.00	0.00	
61.005	180.02	0.87	0.00	4.13	-4.21	0.00	0.00	0.00	
62.005	179.92	0.87	0.00	2.43	-4.37	0.00	0.00	0.00	
63.016	179.70	0.85	0.00	1.76	-4.31	0.00	0.00	0.00	
64.831	179.44	0.83	0.00	1.53	-4.22	0.00	0.00	0.00	
65.024	179.15	0.81	0.00	1.09	-4.11	0.00	0.00	0.00	
66.031	178.85	0.79	0.00	1.09	-4.00	0.00	0.00	0.00	
67.049	178.54	0.76	0.00	1.09	-3.86	0.00	0.00	0.00	
68.034	178.27	0.75	0.00	0.97	-3.09	0.00	0.00	0.00	
69.067	178.11	0.73	0.00	0.74	-1.53	0.00	0.00	0.00	
70.021	178.07	0.73	0.00	0.74	-0.74	0.00	0.00	0.00	
71.054	178.07	0.73	0.00	0.74	-0.71	0.00	0.00	0.00	
72.008	178.07	0.73	0.00	0.63	-0.60	0.00	0.00	0.00	
73.041	178.07	0.73	0.00	0.39	-0.45	0.00	0.00	0.00	
74.074	178.07	0.73	0.00	0.39	-0.39	0.00	0.00	0.00	
75.028	178.07	0.73	0.00	0.39	-0.39	0.00	0.00	0.00	
76.061	178.07	0.73	0.00	0.39	-0.39	0.00	0.00	0.00	
77.014	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
78.048	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
79.001	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
80.034	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
81.010	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
82.028	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
83.004	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
84.062	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
85.063	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
86.048	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
87.048	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
88.048	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
89.048	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	
90.048	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	

91.048	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00
92.048	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	{<-----Inflow----->}					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
93.031	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	
94.005	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	
95.007	178.07	0.73	0.00	0.41	-0.37	0.00	0.00	0.00	
96.021	178.08	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	178.08	0.73	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 20

0.000	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
1.050	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
2.019	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
3.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
4.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
5.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
6.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
7.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
8.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
9.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
10.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
11.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
12.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
13.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
14.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
15.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
16.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
17.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
18.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
19.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
20.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
21.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
22.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
23.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
24.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
25.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
26.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
27.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
28.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
29.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
30.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
31.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
32.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
33.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
34.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
35.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
36.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
37.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00

38.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
39.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
40.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	191.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
43.014	191.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
44.014	191.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
45.014	191.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
46.014	191.00	0.41	0.00	0.02	-0.02	0.00	0.00	0.00	
47.003	191.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
48.035	191.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
49.022	191.00	0.41	0.00	0.06	-0.06	0.00	0.00	0.00	
50.017	191.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
51.031	191.00	0.00	0.00	0.10	-0.10	0.00	0.00	0.00	
52.025	191.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
53.030	191.00	0.41	0.00	0.16	-0.16	0.00	0.00	0.00	
54.008	191.00	0.00	0.00	0.20	-0.20	0.00	0.00	0.00	
55.018	191.00	0.00	0.00	0.26	-0.27	0.00	0.00	0.00	
56.035	191.00	0.00	0.00	0.35	-0.37	0.00	0.00	0.00	
57.032	191.00	0.00	0.00	0.51	-0.53	0.00	0.00	0.00	
58.009	191.00	0.00	0.00	0.74	-0.88	0.00	0.00	0.00	
59.001	191.00	0.00	0.00	1.55	-1.81	0.00	0.00	0.00	
60.005	192.35	0.54	0.00	18.20	-2.86	0.00	0.00	0.00	
61.005	193.36	0.68	0.00	3.19	-3.68	0.00	0.00	0.00	
62.005	193.20	0.66	0.00	1.88	-4.02	0.00	0.00	0.00	
63.016	192.89	0.61	0.00	1.36	-3.80	0.00	0.00	0.00	
64.031	192.53	0.56	0.00	1.18	-3.80	0.00	0.00	0.00	
65.024	192.22	0.52	0.00	0.84	-2.35	0.00	0.00	0.00	
66.031	192.11	0.51	0.00	0.84	-0.65	0.00	0.00	0.00	
67.049	192.16	0.51	0.00	0.84	-0.53	0.00	0.00	0.00	
68.034	192.21	0.52	0.00	0.75	-0.46	0.00	0.00	0.00	
69.067	192.24	0.52	0.00	0.57	-0.41	0.00	0.00	0.00	
70.021	192.27	0.53	0.00	0.57	-0.38	0.00	0.00	0.00	
71.054	192.30	0.53	0.00	0.57	-0.36	0.00	0.00	0.00	
72.008	192.33	0.54	0.00	0.49	-0.34	0.00	0.00	0.00	
73.041	192.34	0.54	0.00	0.30	-0.31	0.00	0.00	0.00	
74.074	192.34	0.54	0.00	0.30	-0.30	0.00	0.00	0.00	
75.028	192.34	0.54	0.00	0.30	-0.28	0.00	0.00	0.00	
76.061	192.34	0.54	0.00	0.30	-0.27	0.00	0.00	0.00	
77.014	192.35	0.54	0.00	0.31	-0.26	0.00	0.00	0.00	
78.048	192.36	0.54	0.00	0.31	-0.25	0.00	0.00	0.00	
79.001	192.37	0.54	0.00	0.31	-0.25	0.00	0.00	0.00	
80.034	192.38	0.54	0.00	0.31	-0.24	0.00	0.00	0.00	
81.010	192.39	0.54	0.00	0.31	-0.24	0.00	0.00	0.00	
82.028	192.40	0.55	0.00	0.31	-0.23	0.00	0.00	0.00	
83.004	192.41	0.55	0.00	0.31	-0.23	0.00	0.00	0.00	
84.062	192.42	0.55	0.00	0.31	-0.22	0.00	0.00	0.00	

85.063	192.44	0.55	0.00	0.31	-0.22	0.00	0.00	0.00
86.048	192.45	0.55	0.00	0.31	-0.22	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
87.048	192.47	0.55	0.00	0.31	-0.21	0.00	0.00	0.00	
88.048	192.48	0.56	0.00	0.31	-0.21	0.00	0.00	0.00	
89.048	192.50	0.56	0.00	0.31	-0.21	0.00	0.00	0.00	
90.048	192.51	0.56	0.00	0.32	-0.21	0.00	0.00	0.00	
91.048	192.53	0.56	0.00	0.32	-0.20	0.00	0.00	0.00	
92.048	192.54	0.56	0.00	0.32	-0.20	0.00	0.00	0.00	
93.031	192.56	0.57	0.00	0.31	-0.20	0.00	0.00	0.00	
94.005	192.58	0.57	0.00	0.32	-0.20	0.00	0.00	0.00	
95.007	192.59	0.57	0.00	0.32	-0.20	0.00	0.00	0.00	
96.021	192.62	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	192.62	0.57	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 21

0.000	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
1.050	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
2.019	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
3.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
4.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
5.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
6.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
7.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
8.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
9.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
10.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
11.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
12.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
13.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
14.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
15.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
16.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
17.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
18.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
19.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
20.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
21.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
22.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
23.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
24.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
25.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
26.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
27.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
28.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
29.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
30.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
31.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
34.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	185.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
36.014	185.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
37.014	185.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00	
38.014	185.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	
39.014	185.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
40.014	185.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
41.014	185.00	0.23	0.00	0.10	-0.10	0.00	0.00	0.00	
42.014	185.00	0.23	0.00	0.12	-0.12	0.00	0.00	0.00	
43.014	185.00	0.23	0.00	0.15	-0.15	0.00	0.00	0.00	
44.014	185.00	0.23	0.00	0.17	-0.17	0.00	0.00	0.00	
45.014	185.00	0.23	0.00	0.19	-0.19	0.00	0.00	0.00	
46.014	185.00	0.23	0.00	0.21	-0.21	0.00	0.00	0.00	
47.003	185.00	0.00	0.00	0.23	-0.24	0.00	0.00	0.00	
48.035	185.00	0.00	0.00	0.28	-0.29	0.00	0.00	0.00	
49.022	185.00	0.23	0.00	0.37	-0.37	0.00	0.00	0.00	
50.017	185.00	0.23	0.00	0.43	-0.44	0.00	0.00	0.00	
51.031	185.00	0.00	0.00	0.52	-0.52	0.00	0.00	0.00	
52.025	185.00	0.00	0.00	0.61	-0.63	0.00	0.00	0.00	
53.030	185.00	0.23	0.00	0.77	-0.76	0.00	0.00	0.00	
54.008	185.00	0.00	0.00	0.90	-0.92	0.00	0.00	0.00	
55.018	185.00	0.00	0.00	1.13	-1.15	0.00	0.00	0.00	
56.035	185.00	0.00	0.00	1.46	-1.51	0.00	0.00	0.00	
57.032	185.05	0.23	0.00	2.05	-1.73	0.00	0.00	0.00	
58.009	185.27	0.24	0.00	2.82	-1.80	0.00	0.00	0.00	
59.001	186.00	0.28	0.00	5.65	-2.04	0.00	0.00	0.00	
60.005	191.37	0.92	0.00	58.93	-3.51	0.00	0.00	0.00	
61.005	193.41	1.48	0.00	9.94	-5.49	0.00	0.00	0.00	
62.005	193.52	1.51	0.00	5.79	-6.23	0.00	0.00	0.00	
63.016	193.45	1.49	0.00	4.17	-6.24	0.00	0.00	0.00	
64.031	193.32	1.46	0.00	3.62	-6.17	0.00	0.00	0.00	
65.024	193.14	1.41	0.00	2.56	-6.06	0.00	0.00	0.00	
66.031	192.94	1.36	0.00	2.57	-5.93	0.00	0.00	0.00	
67.049	192.73	1.30	0.00	2.57	-5.79	0.00	0.00	0.00	
68.034	192.52	1.25	0.00	2.28	-5.64	0.00	0.00	0.00	
69.067	192.27	1.19	0.00	1.74	-5.46	0.00	0.00	0.00	
70.021	192.02	1.12	0.00	1.74	-5.28	0.00	0.00	0.00	
71.054	191.77	1.04	0.00	1.73	-4.64	0.00	0.00	0.00	
72.008	191.59	0.99	0.00	1.47	-3.17	0.00	0.00	0.00	
73.041	191.48	0.95	0.00	0.92	-1.80	0.00	0.00	0.00	
74.074	191.42	0.93	0.00	0.91	-1.39	0.00	0.00	0.00	
75.028	191.38	0.92	0.00	0.91	-1.19	0.00	0.00	0.00	
76.061	191.36	0.92	0.00	0.92	-1.06	0.00	0.00	0.00	
77.014	191.36	0.91	0.00	0.93	-0.97	0.00	0.00	0.00	
78.048	191.36	0.91	0.00	0.93	-0.90	0.00	0.00	0.00	

79.001	191.36	0.92	0.00	0.93	-0.84	0.00	0.00	0.00
80.034	191.37	0.92	0.00	0.93	-0.80	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
81.010	191.38	0.92	0.00	0.92	-0.76	0.00	0.00	0.00	
82.028	191.40	0.93	0.00	0.93	-0.73	0.00	0.00	0.00	
83.004	191.42	0.93	0.00	0.93	-0.70	0.00	0.00	0.00	
84.062	191.44	0.94	0.00	0.93	-0.68	0.00	0.00	0.00	
85.063	191.46	0.95	0.00	0.93	-0.66	0.00	0.00	0.00	
86.048	191.49	0.96	0.00	0.93	-0.64	0.00	0.00	0.00	
87.048	191.51	0.96	0.00	0.93	-0.62	0.00	0.00	0.00	
88.048	191.54	0.97	0.00	0.94	-0.61	0.00	0.00	0.00	
89.048	191.57	0.98	0.00	0.94	-0.59	0.00	0.00	0.00	
90.048	191.60	0.99	0.00	0.94	-0.58	0.00	0.00	0.00	
91.048	191.63	1.00	0.00	0.94	-0.57	0.00	0.00	0.00	
92.048	191.66	1.01	0.00	0.94	-0.56	0.00	0.00	0.00	
93.031	191.69	1.02	0.00	0.94	-0.55	0.00	0.00	0.00	
94.005	191.72	1.03	0.00	0.94	-0.55	0.00	0.00	0.00	
95.007	191.76	1.04	0.00	0.94	-0.53	0.00	0.00	0.00	
96.021	191.80	1.05	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	191.80	1.05	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 22

0.000	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
1.050	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
2.019	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
3.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
4.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
5.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
6.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
7.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
8.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
9.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
10.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
11.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
12.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
13.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
14.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
15.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
16.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
17.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
18.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
19.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
20.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
21.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
22.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
23.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
24.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
25.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00

26.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
27.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
28.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	169.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
46.014	169.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
47.003	169.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
48.035	169.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
49.022	169.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
50.017	169.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
51.031	169.00	0.00	0.00	0.08	-0.08	0.00	0.00	0.00	
52.025	169.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
53.030	169.00	0.00	0.00	0.17	-0.17	0.00	0.00	0.00	
54.008	169.00	0.00	0.00	0.22	-0.23	0.00	0.00	0.00	
55.018	169.00	0.00	0.00	0.31	-0.32	0.00	0.00	0.00	
56.035	169.00	0.00	0.00	0.43	-0.46	0.00	0.00	0.00	
57.032	169.00	0.00	0.00	0.66	-0.69	0.00	0.00	0.00	
58.009	169.00	0.00	0.00	0.97	-1.17	0.00	0.00	0.00	
59.001	169.07	0.27	0.00	2.12	-1.52	0.00	0.00	0.00	
60.005	171.89	0.50	0.00	27.08	-2.21	0.00	0.00	0.00	
61.005	173.65	0.75	0.00	4.86	-3.62	0.00	0.00	0.00	
62.005	173.64	0.75	0.00	2.88	-4.34	0.00	0.00	0.00	
63.016	173.43	0.71	0.00	2.09	-4.20	0.00	0.00	0.00	
64.031	173.17	0.67	0.00	1.82	-3.97	0.00	0.00	0.00	
65.024	172.88	0.62	0.00	1.30	-3.72	0.00	0.00	0.00	
66.031	172.57	0.58	0.00	1.30	-3.46	0.00	0.00	0.00	
67.049	172.26	0.54	0.00	1.31	-3.21	0.00	0.00	0.00	
68.034	171.97	0.50	0.00	1.16	-2.99	0.00	0.00	0.00	
69.067	171.64	0.47	0.00	0.89	-2.80	0.00	0.00	0.00	
70.021	171.33	0.45	0.00	0.89	-2.66	0.00	0.00	0.00	
71.054	170.93	0.41	0.00	0.89	-3.14	0.00	0.00	0.00	
72.008	170.54	0.38	0.00	0.75	-2.43	0.00	0.00	0.00	

73.041	170.30	0.36	0.00	0.47	-0.92	0.00	0.00	0.00
74.074	170.22	0.36	0.00	0.47	-0.70	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96RR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
75.028	170.18	0.35	0.00	0.47	-0.59	0.00	0.00	0.00	
76.061	170.16	0.35	0.00	0.47	-0.53	0.00	0.00	0.00	
77.014	170.15	0.35	0.00	0.48	-0.48	0.00	0.00	0.00	
78.048	170.16	0.35	0.00	0.48	-0.45	0.00	0.00	0.00	
79.001	170.17	0.35	0.00	0.48	-0.43	0.00	0.00	0.00	
80.034	170.18	0.35	0.00	0.48	-0.41	0.00	0.00	0.00	
81.010	170.20	0.35	0.00	0.48	-0.40	0.00	0.00	0.00	
82.028	170.22	0.36	0.00	0.48	-0.38	0.00	0.00	0.00	
83.004	170.24	0.36	0.00	0.48	-0.38	0.00	0.00	0.00	
84.062	170.27	0.36	0.00	0.48	-0.37	0.00	0.00	0.00	
85.063	170.29	0.36	0.00	0.48	-0.36	0.00	0.00	0.00	
86.048	170.32	0.36	0.00	0.48	-0.36	0.00	0.00	0.00	
87.048	170.35	0.37	0.00	0.49	-0.35	0.00	0.00	0.00	
88.048	170.38	0.37	0.00	0.49	-0.35	0.00	0.00	0.00	
89.048	170.42	0.37	0.00	0.49	-0.34	0.00	0.00	0.00	
90.048	170.45	0.37	0.00	0.49	-0.34	0.00	0.00	0.00	
91.048	170.48	0.38	0.00	0.49	-0.34	0.00	0.00	0.00	
92.048	170.52	0.38	0.00	0.49	-0.34	0.00	0.00	0.00	
93.031	170.55	0.38	0.00	0.49	-0.33	0.00	0.00	0.00	
94.005	170.58	0.39	0.00	0.49	-0.33	0.00	0.00	0.00	
95.007	170.62	0.39	0.00	0.49	-0.33	0.00	0.00	0.00	
96.021	170.67	0.39	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	170.67	0.39	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 23

0.000	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
1.050	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
2.019	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
3.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
4.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
5.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
6.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
7.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
8.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
9.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
10.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
11.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
12.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
13.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
14.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
15.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
16.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
17.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
18.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
19.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00

20.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
21.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
22.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
23.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
24.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
25.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
26.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
27.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
28.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
29.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
30.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
31.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
32.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
33.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
34.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
35.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
36.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
37.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
38.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
39.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
40.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
41.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
42.014	130.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00
43.014	130.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
44.014	130.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
45.014	129.99	0.00	0.00	0.01	-0.02	0.00	0.00	0.00
46.014	130.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00
47.003	130.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00
48.035	129.99	0.00	0.00	0.15	-0.16	0.00	0.00	0.00
49.022	130.00	0.01	0.00	0.25	-0.25	0.00	0.00	0.00
50.017	130.00	0.00	0.00	0.34	-0.35	0.00	0.00	0.00
51.031	130.00	0.00	0.00	0.47	-0.47	0.00	0.00	0.00
52.025	129.99	0.00	0.00	0.60	-0.62	0.00	0.00	0.00
53.030	130.00	0.00	0.00	0.82	-0.82	0.00	0.00	0.00
54.008	129.99	0.00	0.00	1.03	-1.06	0.00	0.00	0.00
55.018	130.10	0.02	0.00	1.38	-1.31	0.00	0.00	0.00
56.035	130.67	0.05	0.00	1.87	-1.44	0.00	0.00	0.00
57.032	131.57	0.10	0.00	2.79	-1.53	0.00	0.00	0.00
58.009	132.66	0.16	0.00	4.02	-1.71	0.00	0.00	0.00
59.001	134.32	0.27	0.00	8.54	-2.11	0.00	0.00	0.00
60.005	141.44	1.03	0.00	103.04	-4.38	0.00	0.00	0.00
61.005	144.98	1.52	0.00	18.20	-7.75	0.00	0.00	0.00
62.005	145.30	1.57	0.00	10.74	-9.28	0.00	0.00	0.00
63.016	145.29	1.57	0.00	7.77	-9.42	0.00	0.00	0.00
64.031	145.18	1.55	0.00	6.77	-9.36	0.00	0.00	0.00
65.024	144.99	1.52	0.00	4.81	-9.21	0.00	0.00	0.00
66.031	144.75	1.49	0.00	4.83	-8.99	0.00	0.00	0.00

67.049	144.52	1.45	0.00	4.84	-8.78	0.00	0.00	0.00
68.034	144.29	1.42	0.00	4.31	-8.59	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
69.067	144.00	1.38	0.00	3.30	-8.39	0.00	0.00	0.00
70.021	143.72	1.34	0.00	3.30	-8.17	0.00	0.00	0.00
71.054	143.41	1.30	0.00	3.28	-7.93	0.00	0.00	0.00
72.008	143.11	1.26	0.00	2.79	-7.70	0.00	0.00	0.00
73.041	142.75	1.21	0.00	1.75	-7.44	0.00	0.00	0.00
74.074	142.34	1.15	0.00	1.74	-7.14	0.00	0.00	0.00
75.028	141.98	1.10	0.00	1.74	-6.85	0.00	0.00	0.00
76.061	141.58	1.05	0.00	1.75	-6.55	0.00	0.00	0.00
77.014	141.22	1.00	0.00	1.76	-6.27	0.00	0.00	0.00
78.048	140.84	0.94	0.00	1.77	-5.98	0.00	0.00	0.00
79.001	140.49	0.89	0.00	1.77	-5.71	0.00	0.00	0.00
80.034	140.12	0.84	0.00	1.77	-5.59	0.00	0.00	0.00
81.010	139.53	0.78	0.00	1.77	-9.74	0.00	0.00	0.00
82.028	138.58	0.68	0.00	1.77	-10.10	0.00	0.00	0.00
83.004	137.84	0.61	0.00	1.77	-5.36	0.00	0.00	0.00
84.062	137.42	0.57	0.00	1.78	-3.98	0.00	0.00	0.00
85.063	137.14	0.54	0.00	1.78	-3.31	0.00	0.00	0.00
86.048	136.94	0.52	0.00	1.78	-2.90	0.00	0.00	0.00
87.048	136.78	0.51	0.00	1.79	-2.61	0.00	0.00	0.00
88.048	136.66	0.49	0.00	1.80	-2.40	0.00	0.00	0.00
89.048	136.58	0.49	0.00	1.81	-2.24	0.00	0.00	0.00
90.048	136.51	0.48	0.00	1.81	-2.12	0.00	0.00	0.00
91.048	136.47	0.48	0.00	1.82	-2.02	0.00	0.00	0.00
92.048	136.44	0.47	0.00	1.82	-1.94	0.00	0.00	0.00
93.031	136.43	0.47	0.00	1.81	-1.87	0.00	0.00	0.00
94.005	136.42	0.47	0.00	1.81	-1.81	0.00	0.00	0.00
95.007	136.43	0.47	0.00	1.81	-1.73	0.00	0.00	0.00
96.021	136.54	0.48	0.00	0.00	0.00	0.00	0.00	0.00
96.054	136.54	0.48	0.00	0.00	0.00	0.00	0.00	0.00

\*\*\* Group: BASE Node: 24

0.000	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
1.050	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
2.019	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
3.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
4.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
5.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
6.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
7.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
8.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
9.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
10.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
11.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
12.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
13.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
16.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	112.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
46.014	112.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
47.003	112.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00	
48.035	112.00	0.00	0.00	0.06	-0.07	0.00	0.00	0.00	
49.022	112.00	0.00	0.00	0.18	-0.18	0.00	0.00	0.00	
50.017	112.00	0.00	0.00	0.31	-0.32	0.00	0.00	0.00	
51.031	112.00	0.00	0.00	0.49	-0.50	0.00	0.00	0.00	
52.025	112.00	0.00	0.00	0.70	-0.72	0.00	0.00	0.00	
53.030	112.00	0.00	0.00	1.01	-1.01	0.00	0.00	0.00	
54.008	112.00	0.00	0.00	1.32	-1.37	0.00	0.00	0.00	
55.018	112.00	0.00	0.00	1.84	-1.89	0.00	0.00	0.00	
56.035	112.00	0.00	0.00	2.59	-2.75	0.00	0.00	0.00	
57.032	112.00	0.00	0.00	3.96	-4.12	0.00	0.00	0.00	
58.009	112.00	0.00	0.00	5.84	-7.05	0.00	0.00	0.00	
59.001	112.00	1.90	0.00	12.75	-12.03	0.00	0.00	0.00	
60.005	114.75	2.70	0.00	162.56	-17.95	0.00	0.00	0.00	

61.005	116.81	3.41	0.00	29.19	-23.78	0.00	0.00	0.00
62.005	116.76	3.38	0.00	17.29	-26.41	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
63.016	116.48	3.24	0.00	12.53	-25.69	0.00	0.00	0.00	
64.031	116.13	3.07	0.00	10.93	-24.52	0.00	0.00	0.00	
65.024	115.69	2.95	0.00	7.78	-25.86	0.00	0.00	0.00	
66.031	115.29	2.87	0.00	7.81	-17.26	0.00	0.00	0.00	
67.049	115.19	2.85	0.00	7.84	-6.03	0.00	0.00	0.00	
68.034	115.25	2.86	0.00	6.99	-4.83	0.00	0.00	0.00	
69.067	115.30	2.87	0.00	5.35	-4.16	0.00	0.00	0.00	
70.021	115.33	2.88	0.00	5.35	-3.75	0.00	0.00	0.00	
71.054	115.39	2.89	0.00	5.33	-3.44	0.00	0.00	0.00	
72.008	115.43	2.90	0.00	4.52	-3.21	0.00	0.00	0.00	
73.041	115.45	2.90	0.00	2.84	-2.97	0.00	0.00	0.00	
74.074	115.44	2.90	0.00	2.82	-2.79	0.00	0.00	0.00	
75.028	115.45	2.90	0.00	2.83	-2.65	0.00	0.00	0.00	
76.061	115.45	2.90	0.00	2.85	-2.53	0.00	0.00	0.00	
77.014	115.46	2.90	0.00	2.87	-2.44	0.00	0.00	0.00	
78.048	115.48	2.91	0.00	2.87	-2.35	0.00	0.00	0.00	
79.001	115.49	2.91	0.00	2.88	-2.28	0.00	0.00	0.00	
80.034	115.51	2.91	0.00	2.88	-2.21	0.00	0.00	0.00	
81.010	115.53	2.92	0.00	2.87	-2.16	0.00	0.00	0.00	
82.028	115.55	2.92	0.00	2.88	-2.11	0.00	0.00	0.00	
83.004	115.57	2.92	0.00	2.89	-2.06	0.00	0.00	0.00	
84.062	115.60	2.93	0.00	2.89	-2.02	0.00	0.00	0.00	
85.063	115.63	2.93	0.00	2.90	-1.98	0.00	0.00	0.00	
86.048	115.65	2.94	0.00	2.91	-1.95	0.00	0.00	0.00	
87.048	115.68	2.94	0.00	2.91	-1.92	0.00	0.00	0.00	
88.048	115.71	2.95	0.00	2.93	-1.89	0.00	0.00	0.00	
89.048	115.74	2.95	0.00	2.95	-1.86	0.00	0.00	0.00	
90.048	115.77	2.96	0.00	2.96	-1.84	0.00	0.00	0.00	
91.048	115.80	2.97	0.00	2.96	-1.82	0.00	0.00	0.00	
92.048	115.83	2.97	0.00	2.96	-1.80	0.00	0.00	0.00	
93.031	115.86	2.98	0.00	2.95	-1.78	0.00	0.00	0.00	
94.005	115.90	2.98	0.00	2.96	-1.77	0.00	0.00	0.00	
95.007	115.93	2.99	0.00	2.96	-1.73	0.00	0.00	0.00	
96.021	115.97	3.00	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	115.97	3.00	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 2A

0.000	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
1.050	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
2.019	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
3.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
4.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
5.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
6.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
7.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
10.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
11.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
12.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
13.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
14.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
15.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
16.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
17.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
18.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
19.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
20.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
21.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
22.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
23.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
24.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
25.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
26.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
27.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
28.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
29.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
30.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
31.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
32.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
33.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
34.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
35.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
36.014	192.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
37.014	192.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
38.014	192.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
39.014	192.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
40.014	192.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00
41.014	192.00	0.20	0.00	0.02	-0.02	0.00	0.00	0.00
42.014	192.00	0.20	0.00	0.03	-0.03	0.00	0.00	0.00
43.014	192.00	0.20	0.00	0.03	-0.03	0.00	0.00	0.00
44.014	192.00	0.20	0.00	0.04	-0.04	0.00	0.00	0.00
45.014	192.00	0.20	0.00	0.05	-0.05	0.00	0.00	0.00
46.014	192.00	0.20	0.00	0.06	-0.06	0.00	0.00	0.00
47.003	192.00	0.00	0.00	0.06	-0.07	0.00	0.00	0.00
48.035	192.00	0.00	0.00	0.08	-0.08	0.00	0.00	0.00
49.022	192.00	0.20	0.00	0.11	-0.11	0.00	0.00	0.00
50.017	192.00	0.20	0.00	0.13	-0.13	0.00	0.00	0.00
51.031	192.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00
52.025	192.00	0.00	0.00	0.19	-0.19	0.00	0.00	0.00
53.030	192.00	0.20	0.00	0.24	-0.24	0.00	0.00	0.00
54.008	192.00	0.00	0.00	0.28	-0.29	0.00	0.00	0.00

55.018	192.00	0.00	0.00	0.36	-0.37	0.00	0.00	0.00
56.035	192.00	0.00	0.00	0.47	-0.49	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
57.032	192.00	0.00	0.00	0.67	-0.69	0.00	0.00	0.00	
58.009	191.99	0.00	0.00	0.92	-1.09	0.00	0.00	0.00	
59.001	192.07	0.20	0.00	1.88	-1.39	0.00	0.00	0.00	
60.005	195.04	0.34	0.00	20.32	-1.89	0.00	0.00	0.00	
61.005	197.06	0.45	0.00	3.47	-2.77	0.00	0.00	0.00	
62.005	196.87	0.44	0.00	2.03	-4.64	0.00	0.00	0.00	
63.016	196.36	0.41	0.00	1.46	-3.98	0.00	0.00	0.00	
64.031	196.07	0.39	0.00	1.27	-1.63	0.00	0.00	0.00	
65.024	195.99	0.39	0.00	0.90	-1.27	0.00	0.00	0.00	
66.031	195.93	0.38	0.00	0.90	-1.08	0.00	0.00	0.00	
67.049	195.91	0.38	0.00	0.90	-0.96	0.00	0.00	0.00	
68.034	195.89	0.38	0.00	0.80	-0.87	0.00	0.00	0.00	
69.067	195.86	0.38	0.00	0.61	-0.80	0.00	0.00	0.00	
70.021	195.83	0.38	0.00	0.61	-0.74	0.00	0.00	0.00	
71.054	195.81	0.38	0.00	0.61	-0.70	0.00	0.00	0.00	
72.008	195.78	0.38	0.00	0.52	-0.65	0.00	0.00	0.00	
73.041	195.73	0.37	0.00	0.32	-0.61	0.00	0.00	0.00	
74.074	195.67	0.37	0.00	0.32	-0.57	0.00	0.00	0.00	
75.028	195.62	0.37	0.00	0.32	-0.54	0.00	0.00	0.00	
76.061	195.57	0.37	0.00	0.32	-0.52	0.00	0.00	0.00	
77.014	195.54	0.36	0.00	0.33	-0.50	0.00	0.00	0.00	
78.048	195.50	0.36	0.00	0.33	-0.48	0.00	0.00	0.00	
79.001	195.47	0.36	0.00	0.33	-0.46	0.00	0.00	0.00	
80.034	195.44	0.36	0.00	0.33	-0.45	0.00	0.00	0.00	
81.010	195.41	0.36	0.00	0.33	-0.44	0.00	0.00	0.00	
82.028	195.39	0.36	0.00	0.33	-0.42	0.00	0.00	0.00	
83.004	195.37	0.36	0.00	0.33	-0.41	0.00	0.00	0.00	
84.062	195.35	0.35	0.00	0.33	-0.40	0.00	0.00	0.00	
85.063	195.33	0.35	0.00	0.33	-0.40	0.00	0.00	0.00	
86.048	195.31	0.35	0.00	0.33	-0.39	0.00	0.00	0.00	
87.048	195.30	0.35	0.00	0.33	-0.38	0.00	0.00	0.00	
88.048	195.29	0.35	0.00	0.33	-0.37	0.00	0.00	0.00	
89.048	195.28	0.35	0.00	0.33	-0.37	0.00	0.00	0.00	
90.048	195.27	0.35	0.00	0.33	-0.36	0.00	0.00	0.00	
91.048	195.27	0.35	0.00	0.33	-0.36	0.00	0.00	0.00	
92.048	195.26	0.35	0.00	0.33	-0.35	0.00	0.00	0.00	
93.031	195.26	0.35	0.00	0.33	-0.35	0.00	0.00	0.00	
94.005	195.25	0.35	0.00	0.33	-0.35	0.00	0.00	0.00	
95.007	195.25	0.35	0.00	0.33	-0.34	0.00	0.00	0.00	
96.021	195.28	0.35	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	195.28	0.35	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 2B  
 0.000 182.00 1.23 0.00 0.00 0.00 0.00 0.00 0.00  
 1.050 182.00 1.23 0.00 0.00 0.00 0.00 0.00 0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
4.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	182.00	1.23	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	182.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	182.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	182.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
41.014	182.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
42.014	182.00	1.23	0.00	0.03	-0.03	0.00	0.00	0.00	
43.014	182.00	1.23	0.00	0.05	-0.05	0.00	0.00	0.00	
44.014	182.00	1.23	0.00	0.07	-0.07	0.00	0.00	0.00	
45.014	182.00	1.23	0.00	0.08	-0.09	0.00	0.00	0.00	
46.014	182.00	1.23	0.00	0.10	-0.10	0.00	0.00	0.00	
47.003	182.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
48.035	182.00	0.00	0.00	0.15	-0.16	0.00	0.00	0.00	

49.022	182.00	1.23	0.00	0.20	-0.20	0.00	0.00	0.00
50.017	182.00	1.23	0.00	0.25	-0.25	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
51.031	182.00	0.00	0.00	0.31	-0.31	0.00	0.00	0.00	
52.025	182.00	0.00	0.00	0.37	-0.38	0.00	0.00	0.00	
53.030	182.00	1.23	0.00	0.47	-0.47	0.00	0.00	0.00	
54.008	182.00	0.00	0.00	0.56	-0.58	0.00	0.00	0.00	
55.018	182.00	0.00	0.00	0.72	-0.74	0.00	0.00	0.00	
56.035	182.00	0.00	0.00	0.95	-1.00	0.00	0.00	0.00	
57.032	182.00	0.00	0.00	1.36	-1.40	0.00	0.00	0.00	
58.009	182.00	0.00	0.00	1.90	-2.27	0.00	0.00	0.00	
59.001	182.00	0.00	0.00	3.89	-5.63	0.00	0.00	0.00	
60.005	183.03	1.40	0.00	42.89	-8.92	0.00	0.00	0.00	
61.005	183.91	1.55	0.00	7.37	-9.95	0.00	0.00	0.00	
62.005	183.67	1.51	0.00	4.31	-10.31	0.00	0.00	0.00	
63.016	183.31	1.45	0.00	3.11	-9.96	0.00	0.00	0.00	
64.031	182.91	1.38	0.00	2.70	-9.50	0.00	0.00	0.00	
65.024	182.50	1.31	0.00	1.92	-8.52	0.00	0.00	0.00	
66.031	182.19	1.26	0.00	1.92	-4.83	0.00	0.00	0.00	
67.049	182.10	1.25	0.00	1.92	-1.87	0.00	0.00	0.00	
68.034	182.10	1.25	0.00	1.71	-1.66	0.00	0.00	0.00	
69.067	182.10	1.25	0.00	1.31	-1.41	0.00	0.00	0.00	
70.021	182.10	1.25	0.00	1.31	-1.31	0.00	0.00	0.00	
71.054	182.10	1.25	0.00	1.30	-1.25	0.00	0.00	0.00	
72.008	182.10	1.25	0.00	1.10	-1.05	0.00	0.00	0.00	
73.041	182.10	1.25	0.00	0.69	-0.79	0.00	0.00	0.00	
74.074	182.10	1.25	0.00	0.69	-0.69	0.00	0.00	0.00	
75.028	182.10	1.25	0.00	0.69	-0.69	0.00	0.00	0.00	
76.061	182.10	1.25	0.00	0.69	-0.69	0.00	0.00	0.00	
77.014	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
78.048	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
79.001	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
80.034	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
81.010	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
82.028	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
83.004	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
84.062	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
85.063	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
86.048	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
87.048	182.10	1.25	0.00	0.70	-0.70	0.00	0.00	0.00	
88.048	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
89.048	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
90.048	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
91.048	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
92.048	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
93.031	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
94.005	182.10	1.25	0.00	0.71	-0.71	0.00	0.00	0.00	
95.007	182.10	1.25	0.00	0.71	-0.65	0.00	0.00	0.00	





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
*** Group: BASE		Node: 2C							
0.000	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
1.050	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
2.019	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
3.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
4.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	

44.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
45.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	{<-----Inflow----->}					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
46.014	163.00	0.61	0.00	0.00	-0.00	0.00	0.00	0.00
47.003	163.00	0.61	0.00	0.01	-0.00	0.00	0.00	0.00
48.035	163.00	0.61	0.00	0.03	-0.00	0.00	0.00	0.00
49.022	163.01	0.61	0.00	0.05	-0.01	0.00	0.00	0.00
50.017	163.02	0.61	0.00	0.08	-0.01	0.00	0.00	0.00
51.031	163.03	0.61	0.00	0.11	-0.02	0.00	0.00	0.00
52.025	163.04	0.61	0.00	0.15	-0.03	0.00	0.00	0.00
53.030	163.06	0.61	0.00	0.21	-0.04	0.00	0.00	0.00
54.008	163.09	0.61	0.00	0.26	-0.05	0.00	0.00	0.00
55.018	163.12	0.62	0.00	0.36	-0.07	0.00	0.00	0.00
56.035	163.17	0.62	0.00	0.50	-0.10	0.00	0.00	0.00
57.032	163.23	0.63	0.00	0.75	-0.13	0.00	0.00	0.00
58.009	163.33	0.63	0.00	1.09	-0.18	0.00	0.00	0.00
59.001	163.52	0.65	0.00	2.34	-0.26	0.00	0.00	0.00
60.005	165.25	0.85	0.00	29.02	-0.86	0.00	0.00	0.00
61.005	166.52	1.21	0.00	5.17	-1.89	0.00	0.00	0.00
62.005	166.65	1.25	0.00	3.06	-2.51	0.00	0.00	0.00
63.016	166.65	1.25	0.00	2.21	-2.64	0.00	0.00	0.00
64.031	166.62	1.24	0.00	1.93	-2.60	0.00	0.00	0.00
65.024	166.56	1.22	0.00	1.37	-2.50	0.00	0.00	0.00
66.031	166.48	1.20	0.00	1.38	-2.39	0.00	0.00	0.00
67.049	166.41	1.18	0.00	1.38	-2.32	0.00	0.00	0.00
68.034	166.34	1.16	0.00	1.23	-2.27	0.00	0.00	0.00
69.067	166.26	1.13	0.00	0.94	-2.20	0.00	0.00	0.00
70.021	165.17	1.10	0.00	0.94	-2.14	0.00	0.00	0.00
71.054	166.08	1.07	0.00	0.94	-2.06	0.00	0.00	0.00
72.008	165.99	1.05	0.00	0.80	-2.00	0.00	0.00	0.00
73.041	165.89	1.02	0.00	0.50	-1.92	0.00	0.00	0.00
74.074	165.77	0.99	0.00	0.50	-1.84	0.00	0.00	0.00
75.028	165.66	0.96	0.00	0.50	-1.76	0.00	0.00	0.00
76.061	165.55	0.93	0.00	0.50	-1.68	0.00	0.00	0.00
77.014	165.45	0.90	0.00	0.50	-1.61	0.00	0.00	0.00
78.048	165.35	0.88	0.00	0.51	-1.54	0.00	0.00	0.00
79.001	165.26	0.85	0.00	0.51	-1.48	0.00	0.00	0.00
80.034	165.17	0.83	0.00	0.51	-1.41	0.00	0.00	0.00
81.010	165.08	0.80	0.00	0.50	-1.36	0.00	0.00	0.00
82.028	164.99	0.78	0.00	0.51	-1.30	0.00	0.00	0.00
83.004	164.91	0.77	0.00	0.51	-1.25	0.00	0.00	0.00
84.062	164.83	0.77	0.00	0.51	-1.20	0.00	0.00	0.00
85.063	164.76	0.76	0.00	0.51	-1.16	0.00	0.00	0.00
86.048	164.69	0.75	0.00	0.51	-1.12	0.00	0.00	0.00
87.048	164.62	0.75	0.00	0.51	-1.08	0.00	0.00	0.00
88.048	164.56	0.74	0.00	0.51	-1.04	0.00	0.00	0.00
89.048	164.51	0.74	0.00	0.52	-1.01	0.00	0.00	0.00
90.048	164.45	0.73	0.00	0.52	-0.98	0.00	0.00	0.00

- 91.048	164.40	0.73	0.00	0.52	-0.95	0.00	0.00	0.00
92.048	164.36	0.72	0.00	0.52	-1.15	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
93.031	164.01	0.69	0.00	0.52	-5.81	0.00	0.00	0.00	
94.005	163.30	0.63	0.00	0.52	-6.91	0.00	0.00	0.00	
95.007	162.98	0.00	0.00	0.52	-1.82	0.00	0.00	0.00	
96.021	163.01	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	163.01	0.61	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 3

0.000	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
1.050	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
2.019	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
3.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
4.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
5.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
6.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
7.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
8.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
9.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
10.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
11.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
12.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
13.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
14.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
15.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
16.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
17.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
18.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
19.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
20.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
21.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
22.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
23.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
24.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
25.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
26.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
27.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
28.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
29.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
30.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
31.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
32.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
33.014	165.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00
34.014	165.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00
35.014	165.00	0.60	0.00	0.07	-0.07	0.00	0.00	0.00
36.014	165.00	0.60	0.00	0.10	-0.10	0.00	0.00	0.00
37.014	165.00	0.60	0.00	0.13	-0.13	0.00	0.00	0.00

- 38.014	165.00	0.60	0.00	0.15	-0.15	0.00	0.00	0.00
39.014	165.00	0.60	0.00	0.18	-0.18	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	{<-----Inflow----->}					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
40.014	165.00	0.60	0.00	0.21	-0.21	0.00	0.00	0.00	
41.014	165.00	0.60	0.00	0.24	-0.24	0.00	0.00	0.00	
42.014	165.00	0.60	0.00	0.27	-0.27	0.00	0.00	0.00	
43.014	165.00	0.60	0.00	0.29	-0.29	0.00	0.00	0.00	
44.014	165.00	0.60	0.00	0.31	-0.31	0.00	0.00	0.00	
45.014	165.00	0.60	0.00	0.33	-0.33	0.00	0.00	0.00	
46.014	165.00	0.60	0.00	0.35	-0.35	0.00	0.00	0.00	
47.003	165.00	0.00	0.00	0.37	-0.38	0.00	0.00	0.00	
48.035	165.00	0.00	0.00	0.44	-0.46	0.00	0.00	0.00	
49.022	165.00	0.60	0.00	0.56	-0.55	0.00	0.00	0.00	
50.017	165.00	0.60	0.00	0.64	-0.65	0.00	0.00	0.00	
51.031	165.00	0.60	0.00	0.75	-0.75	0.00	0.00	0.00	
52.025	165.00	0.00	0.00	0.86	-0.88	0.00	0.00	0.00	
53.030	165.00	0.60	0.00	1.05	-1.04	0.00	0.00	0.00	
54.008	165.00	0.00	0.00	1.20	-1.23	0.00	0.00	0.00	
55.018	165.00	0.00	0.00	1.48	-1.50	0.00	0.00	0.00	
56.035	165.00	0.00	0.00	1.86	-1.95	0.00	0.00	0.00	
57.032	165.00	0.00	0.00	2.57	-2.61	0.00	0.00	0.00	
58.009	165.00	0.00	0.00	3.46	-3.45	0.00	0.00	0.00	
59.001	165.19	0.61	0.00	6.75	-3.95	0.00	0.00	0.00	
60.005	168.61	0.95	0.00	65.38	-5.10	0.00	0.00	0.00	
61.005	171.04	1.23	0.00	10.73	-7.14	0.00	0.00	0.00	
62.005	171.10	1.24	0.00	6.21	-8.08	0.00	0.00	0.00	
63.016	170.91	1.22	0.00	4.46	-8.02	0.00	0.00	0.00	
64.031	170.65	1.18	0.00	3.86	-7.83	0.00	0.00	0.00	
65.024	170.34	1.14	0.00	2.73	-7.60	0.00	0.00	0.00	
66.031	169.99	1.10	0.00	2.73	-7.33	0.00	0.00	0.00	
67.049	169.64	1.06	0.00	2.73	-7.05	0.00	0.00	0.00	
68.034	169.30	1.02	0.00	2.42	-6.80	0.00	0.00	0.00	
69.067	168.91	0.98	0.00	1.85	-6.52	0.00	0.00	0.00	
70.021	168.54	0.94	0.00	1.84	-6.29	0.00	0.00	0.00	
71.054	168.06	0.89	0.00	1.83	-7.40	0.00	0.00	0.00	
72.008	167.62	0.84	0.00	1.55	-5.74	0.00	0.00	0.00	
73.041	167.34	0.81	0.00	0.97	-2.28	0.00	0.00	0.00	
74.074	167.23	0.80	0.00	0.97	-1.76	0.00	0.00	0.00	
75.028	167.16	0.80	0.00	0.97	-1.51	0.00	0.00	0.00	
76.061	167.11	0.79	0.00	0.97	-1.33	0.00	0.00	0.00	
77.014	167.08	0.79	0.00	0.98	-1.22	0.00	0.00	0.00	
78.048	167.06	0.79	0.00	0.98	-1.13	0.00	0.00	0.00	
79.001	167.05	0.78	0.00	0.98	-1.06	0.00	0.00	0.00	
80.034	167.05	0.78	0.00	0.98	-1.00	0.00	0.00	0.00	
81.010	167.04	0.78	0.00	0.97	-0.96	0.00	0.00	0.00	
82.028	167.05	0.78	0.00	0.97	-0.92	0.00	0.00	0.00	
83.004	167.06	0.78	0.00	0.98	-0.89	0.00	0.00	0.00	
84.062	167.07	0.79	0.00	0.98	-0.86	0.00	0.00	0.00	

-	85.063	167.08	0.79	0.00	0.98	-0.83	0.00	0.00	0.00
	86.048	167.10	0.79	0.00	0.98	-0.81	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
87.048	167.12	0.79	0.00	0.98	-0.79	0.00	0.00	0.00	
88.048	167.14	0.79	0.00	0.98	-0.78	0.00	0.00	0.00	
89.048	167.16	0.79	0.00	0.99	-0.76	0.00	0.00	0.00	
90.048	167.18	0.80	0.00	0.99	-0.75	0.00	0.00	0.00	
91.048	167.21	0.80	0.00	0.99	-0.74	0.00	0.00	0.00	
92.048	167.24	0.80	0.00	0.99	-0.73	0.00	0.00	0.00	
93.031	167.26	0.81	0.00	0.99	-0.72	0.00	0.00	0.00	
94.005	167.29	0.81	0.00	0.99	-0.71	0.00	0.00	0.00	
95.007	167.32	0.81	0.00	0.99	-0.69	0.00	0.00	0.00	
96.021	167.37	0.82	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	167.37	0.82	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Nodes: 4

0.000	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
1.050	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
2.019	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
3.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
4.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
5.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
6.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
7.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
8.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
9.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
10.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
11.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
12.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
13.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
14.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
15.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
16.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
17.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
18.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
19.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
20.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
21.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
22.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
23.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
24.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
25.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
26.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
27.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
28.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
29.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
30.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
31.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00

- 32.014	177.00	0.73	0.00	0.00	0.00	0.00
33.014	177.00	0.73	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
34.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	177.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
46.014	177.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
47.003	177.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
48.035	177.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
49.022	177.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
50.017	177.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
51.031	177.00	0.00	0.00	0.10	-0.11	0.00	0.00	0.00	
52.025	177.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	
53.030	177.00	0.00	0.00	0.21	-0.22	0.00	0.00	0.00	
54.008	177.00	0.00	0.00	0.28	-0.29	0.00	0.00	0.00	
55.018	177.00	0.00	0.00	0.39	-0.40	0.00	0.00	0.00	
56.035	177.00	0.00	0.00	0.55	-0.59	0.00	0.00	0.00	
57.032	177.00	0.00	0.00	0.84	-0.88	0.00	0.00	0.00	
58.009	177.00	0.00	0.00	1.25	-1.52	0.00	0.00	0.00	
59.001	176.99	0.00	0.00	2.72	-4.47	0.00	0.00	0.00	
60.005	178.32	0.89	0.00	34.70	-7.68	0.00	0.00	0.00	
61.005	179.37	1.02	0.00	6.23	-9.02	0.00	0.00	0.00	
62.005	179.02	0.97	0.00	3.69	-9.42	0.00	0.00	0.00	
63.016	178.49	0.91	0.00	2.68	-8.84	0.00	0.00	0.00	
64.031	177.91	0.84	0.00	2.33	-8.11	0.00	0.00	0.00	
65.024	177.42	0.78	0.00	1.66	-5.40	0.00	0.00	0.00	
66.031	177.19	0.75	0.00	1.67	-2.36	0.00	0.00	0.00	
67.049	177.15	0.75	0.00	1.67	-1.62	0.00	0.00	0.00	
68.034	177.16	0.75	0.00	1.49	-1.45	0.00	0.00	0.00	
69.067	177.16	0.75	0.00	1.14	-1.23	0.00	0.00	0.00	
70.021	177.15	0.75	0.00	1.14	-1.14	0.00	0.00	0.00	
71.054	177.15	0.75	0.00	1.14	-1.09	0.00	0.00	0.00	
72.008	177.16	0.75	0.00	0.97	-0.92	0.00	0.00	0.00	
73.041	177.16	0.75	0.00	0.61	-0.69	0.00	0.00	0.00	
74.074	177.15	0.75	0.00	0.60	-0.60	0.00	0.00	0.00	
75.028	177.15	0.75	0.00	0.60	-0.60	0.00	0.00	0.00	
76.061	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
77.014	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
78.048	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
79.001	177.15	0.75	0.00	0.62	-0.61	0.00	0.00	0.00	
80.034	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
81.010	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
82.028	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
83.004	177.15	0.75	0.00	0.62	-0.62	0.00	0.00	0.00	
84.062	177.15	0.75	0.00	0.62	-0.62	0.00	0.00	0.00	
85.063	177.15	0.75	0.00	0.62	-0.62	0.00	0.00	0.00	
86.048	177.15	0.75	0.00	0.62	-0.62	0.00	0.00	0.00	
87.048	177.15	0.75	0.00	0.62	-0.62	0.00	0.00	0.00	
88.048	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
89.048	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
90.048	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
91.048	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
92.048	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
93.031	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
94.005	177.15	0.75	0.00	0.63	-0.63	0.00	0.00	0.00	
95.007	177.15	0.75	0.00	0.63	-0.58	0.00	0.00	0.00	
96.021	177.18	0.75	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	177.18	0.75	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 6

0.000	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
1.050	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
2.019	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
3.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
4.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
5.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
6.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
7.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
8.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
9.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
10.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
11.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
12.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
13.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
14.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
15.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
16.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
17.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
18.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
19.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
20.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
21.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
22.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
23.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
24.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00
25.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
28.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
46.014	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
47.003	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
48.035	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
49.022	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
50.017	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
51.031	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
52.025	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
53.030	203.00	1.29	0.00	0.00	0.00	0.00	0.00	0.00	
54.008	203.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
55.018	203.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
56.035	203.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
57.032	203.00	0.00	0.00	0.08	-0.09	0.00	0.00	0.00	
58.009	203.00	0.00	0.00	0.19	-0.29	0.00	0.00	0.00	
59.001	202.99	0.00	0.00	0.61	-3.58	0.00	0.00	0.00	
60.005	203.12	1.31	0.00	12.87	-7.24	0.00	0.00	0.00	
61.005	203.22	1.32	0.00	2.57	-4.89	0.00	0.00	0.00	
62.005	203.14	1.31	0.00	1.56	-1.71	0.00	0.00	0.00	
63.016	203.14	1.31	0.00	1.14	-1.21	0.00	0.00	0.00	
64.031	203.14	1.31	0.00	1.01	-0.97	0.00	0.00	0.00	
65.024	203.14	1.31	0.00	0.72	-0.79	0.00	0.00	0.00	
66.031	203.13	1.31	0.00	0.73	-0.73	0.00	0.00	0.00	
67.049	203.13	1.31	0.00	0.73	-0.71	0.00	0.00	0.00	
68.034	203.14	1.31	0.00	0.66	-0.64	0.00	0.00	0.00	
69.067	203.13	1.31	0.00	0.50	-0.54	0.00	0.00	0.00	
70.021	203.13	1.31	0.00	0.50	-0.50	0.00	0.00	0.00	
71.054	203.13	1.31	0.00	0.50	-0.48	0.00	0.00	0.00	
72.008	203.14	1.31	0.00	0.43	-0.41	0.00	0.00	0.00	

73.041	203.13	1.31	0.00	0.27	-0.31	0.00	0.00	0.00
74.074	203.13	1.31	0.00	0.27	-0.27	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
75.028	203.13	1.31	0.00	0.27	-0.27	0.00	0.00	0.00	
76.061	203.13	1.31	0.00	0.27	-0.27	0.00	0.00	0.00	
77.014	203.13	1.31	0.00	0.27	-0.27	0.00	0.00	0.00	
78.048	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
79.001	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
80.034	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
81.010	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
82.028	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
83.004	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
84.062	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
85.063	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
86.048	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
87.048	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
88.048	203.13	1.31	0.00	0.28	-0.28	0.00	0.00	0.00	
89.048	203.13	1.31	0.00	0.29	-0.29	0.00	0.00	0.00	
90.048	203.13	1.31	0.00	0.29	-0.29	0.00	0.00	0.00	
91.048	203.13	1.31	0.00	0.29	-0.29	0.00	0.00	0.00	
92.048	203.13	1.31	0.00	0.29	-0.29	0.00	0.00	0.00	
93.031	203.13	1.31	0.00	0.29	-0.29	0.00	0.00	0.00	
94.005	203.13	1.31	0.00	0.29	-0.29	0.00	0.00	0.00	
95.007	203.13	1.31	0.00	0.29	-0.26	0.00	0.00	0.00	
96.021	203.14	1.31	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	203.14	1.31	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 7

0.000	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
1.050	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
2.019	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
3.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
4.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
5.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
6.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
7.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
8.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
9.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
10.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
11.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
12.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
13.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
14.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
15.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
16.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
17.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
18.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
19.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00



20.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
22.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	149.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
44.014	149.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
45.014	149.02	0.06	0.00	0.04	-0.02	0.00	0.00	0.00	
46.014	149.03	0.06	0.00	0.07	-0.07	0.00	0.00	0.00	
47.003	149.05	0.06	0.00	0.10	-0.07	0.00	0.00	0.00	
48.035	149.06	0.06	0.00	0.14	-0.14	0.00	0.00	0.00	
49.022	149.10	0.06	0.00	0.21	-0.15	0.00	0.00	0.00	
50.017	149.14	0.07	0.00	0.27	-0.27	0.00	0.00	0.00	
51.031	149.19	0.07	0.00	0.36	-0.28	0.00	0.00	0.00	
52.025	149.22	0.07	0.00	0.45	-0.46	0.00	0.00	0.00	
53.030	149.30	0.07	0.00	0.60	-0.47	0.00	0.00	0.00	
54.008	149.35	0.08	0.00	0.74	-0.76	0.00	0.00	0.00	
55.018	149.45	0.08	0.00	0.98	-0.77	0.00	0.00	0.00	
56.035	149.52	0.09	0.00	1.31	-1.36	0.00	0.00	0.00	
57.032	149.74	0.10	0.00	1.93	-1.43	0.00	0.00	0.00	
58.009	149.72	0.10	0.00	2.76	-3.28	0.00	0.00	0.00	
59.001	150.38	0.15	0.00	5.81	-3.32	0.00	0.00	0.00	
60.005	154.48	0.51	0.00	68.28	-38.73	0.00	0.00	0.00	
61.005	154.69	0.53	0.00	11.97	-38.56	0.00	0.00	0.00	
62.005	151.95	0.29	0.00	7.05	-7.82	0.00	0.00	0.00	
63.016	151.05	0.21	0.00	5.10	-9.52	0.00	0.00	0.00	
64.031	150.31	0.14	0.00	4.44	-3.30	0.00	0.00	0.00	
65.024	150.69	0.18	0.00	3.15	-2.79	0.00	0.00	0.00	
66.031	150.92	0.20	0.00	3.16	-2.51	0.00	0.00	0.00	

67.049	151.22	0.22	0.00	3.17	-2.36	0.00	0.00	0.00
68.034	151.47	0.24	0.00	2.82	-2.20	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
69.067	151.59	0.26	0.00	2.16	-2.02	0.00	0.00	0.00	
70.021	151.65	0.26	0.00	2.16	-1.90	0.00	0.00	0.00	
71.054	151.75	0.27	0.00	2.15	-1.80	0.00	0.00	0.00	
72.008	151.82	0.28	0.00	1.82	-1.68	0.00	0.00	0.00	
73.041	151.78	0.27	0.00	1.14	-1.50	0.00	0.00	0.00	
74.074	151.69	0.26	0.00	1.14	-1.37	0.00	0.00	0.00	
75.028	151.63	0.26	0.00	1.14	-1.30	0.00	0.00	0.00	
76.061	151.59	0.26	0.00	1.14	-1.24	0.00	0.00	0.00	
77.014	151.57	0.25	0.00	1.15	-1.20	0.00	0.00	0.00	
78.048	151.56	0.25	0.00	1.16	-1.17	0.00	0.00	0.00	
79.001	151.56	0.25	0.00	1.16	-1.15	0.00	0.00	0.00	
80.034	151.56	0.25	0.00	1.16	-1.12	0.00	0.00	0.00	
81.010	151.58	0.25	0.00	1.15	-1.11	0.00	0.00	0.00	
82.028	151.59	0.26	0.00	1.16	-1.09	0.00	0.00	0.00	
83.004	151.62	0.26	0.00	1.16	-1.08	0.00	0.00	0.00	
84.062	151.65	0.26	0.00	1.16	-1.07	0.00	0.00	0.00	
85.063	151.68	0.26	0.00	1.16	-1.06	0.00	0.00	0.00	
86.048	151.71	0.27	0.00	1.17	-1.05	0.00	0.00	0.00	
87.048	151.75	0.27	0.00	1.17	-1.05	0.00	0.00	0.00	
88.048	151.79	0.27	0.00	1.17	-1.04	0.00	0.00	0.00	
89.048	151.83	0.28	0.00	1.18	-1.04	0.00	0.00	0.00	
90.048	151.87	0.28	0.00	1.18	-1.03	0.00	0.00	0.00	
91.048	151.92	0.28	0.00	1.19	-1.03	0.00	0.00	0.00	
92.048	151.96	0.29	0.00	1.18	-1.03	0.00	0.00	0.00	
93.031	152.01	0.29	0.00	1.18	-1.02	0.00	0.00	0.00	
94.005	152.05	0.30	0.00	1.18	-1.02	0.00	0.00	0.00	
95.007	152.10	0.30	0.00	1.18	-0.99	0.00	0.00	0.00	
96.021	152.23	0.31	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	152.23	0.31	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 8

0.000	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
1.050	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
2.019	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
3.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
4.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
5.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
6.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
7.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
8.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
9.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
10.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
11.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
12.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
13.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
16.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
17.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
18.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
19.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
20.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
21.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
22.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
23.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
24.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
25.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
26.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
27.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
28.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
29.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
30.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
31.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
32.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
33.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
34.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
35.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
36.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
37.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
38.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
39.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
40.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
41.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
42.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
43.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
44.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
45.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
46.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
47.003	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
48.035	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
49.022	235.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
50.017	235.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
51.031	235.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00
52.025	235.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00
53.030	235.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00
54.008	235.00	0.00	0.00	0.06	-0.06	0.00	0.00	0.00
55.018	235.00	0.00	0.00	0.09	-0.09	0.00	0.00	0.00
56.035	235.00	0.00	0.00	0.14	-0.15	0.00	0.00	0.00
57.032	235.00	0.00	0.00	0.23	-0.24	0.00	0.00	0.00
58.009	235.00	0.00	0.00	0.35	-0.44	0.00	0.00	0.00
59.001	235.00	0.00	0.00	0.82	-1.03	0.00	0.00	0.00
60.005	236.16	0.41	0.00	11.59	-1.76	0.00	0.00	0.00

61.005	237.05	0.50	0.00	2.14	-2.26	0.00	0.00	0.00
62.005	236.94	0.48	0.00	1.28	-2.45	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
63.016	236.71	0.46	0.00	0.93	-2.35	0.00	0.00	0.00	
64.031	236.44	0.43	0.00	0.81	-2.23	0.00	0.00	0.00	
65.024	236.16	0.41	0.00	0.58	-2.09	0.00	0.00	0.00	
66.031	235.85	0.38	0.00	0.58	-1.94	0.00	0.00	0.00	
67.049	235.55	0.35	0.00	0.58	-1.78	0.00	0.00	0.00	
68.034	235.29	0.32	0.00	0.52	-1.44	0.00	0.00	0.00	
69.067	235.12	0.30	0.00	0.40	-0.78	0.00	0.00	0.00	
70.021	235.07	0.30	0.00	0.40	-0.40	0.00	0.00	0.00	
71.054	235.07	0.30	0.00	0.40	-0.38	0.00	0.00	0.00	
72.008	235.08	0.30	0.00	0.34	-0.32	0.00	0.00	0.00	
73.041	235.07	0.30	0.00	0.21	-0.24	0.00	0.00	0.00	
74.074	235.07	0.30	0.00	0.21	-0.21	0.00	0.00	0.00	
75.028	235.07	0.30	0.00	0.21	-0.21	0.00	0.00	0.00	
76.061	235.07	0.30	0.00	0.21	-0.21	0.00	0.00	0.00	
77.014	235.07	0.30	0.00	0.22	-0.21	0.00	0.00	0.00	
78.048	235.07	0.30	0.00	0.22	-0.22	0.00	0.00	0.00	
79.001	235.07	0.30	0.00	0.22	-0.22	0.00	0.00	0.00	
80.034	235.07	0.30	0.00	0.22	-0.21	0.00	0.00	0.00	
81.010	235.08	0.30	0.00	0.22	-0.18	0.00	0.00	0.00	
82.028	235.09	0.30	0.00	0.22	-0.14	0.00	0.00	0.00	
83.004	235.11	0.30	0.00	0.22	-0.15	0.00	0.00	0.00	
84.062	235.13	0.30	0.00	0.22	-0.15	0.00	0.00	0.00	
85.063	235.15	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
86.048	235.17	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
87.048	235.19	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
88.048	235.21	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
89.048	235.23	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
90.048	235.25	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
91.048	235.28	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
92.048	235.30	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
93.031	235.32	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
94.005	235.34	0.33	0.00	0.22	-0.14	0.00	0.00	0.00	
95.007	235.36	0.33	0.00	0.22	-0.13	0.00	0.00	0.00	
96.021	235.39	0.33	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	235.39	0.33	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 9

0.000	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
1.050	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
2.019	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
3.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
4.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
5.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
6.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
7.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
10.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	236.00	1.72	0.00	0.01	0.00	0.00	0.00	0.00	
37.014	236.00	1.72	0.00	0.02	0.00	0.00	0.00	0.00	
38.014	236.00	1.72	0.00	0.03	0.00	0.00	0.00	0.00	
39.014	236.00	1.72	0.00	0.04	0.00	0.00	0.00	0.00	
40.014	236.01	1.72	0.00	0.05	0.00	0.00	0.00	0.00	
41.014	236.01	1.72	0.00	0.06	0.00	0.00	0.00	0.00	
42.014	236.01	1.72	0.00	0.07	0.00	0.00	0.00	0.00	
43.014	236.02	1.72	0.00	0.08	0.00	0.00	0.00	0.00	
44.014	236.02	1.72	0.00	0.08	0.00	0.00	0.00	0.00	
45.014	236.02	1.72	0.00	0.09	0.00	0.00	0.00	0.00	
46.014	236.03	1.72	0.00	0.10	0.00	0.00	0.00	0.00	
47.003	236.03	1.72	0.00	0.10	0.00	0.00	0.00	0.00	
48.035	236.04	1.73	0.00	0.13	0.00	0.00	0.00	0.00	
49.022	236.05	1.73	0.00	0.16	0.00	0.00	0.00	0.00	
50.017	236.05	1.73	0.00	0.18	0.00	0.00	0.00	0.00	
51.031	236.06	1.73	0.00	0.22	0.00	0.00	0.00	0.00	
52.025	236.07	1.73	0.00	0.25	0.00	0.00	0.00	0.00	
53.030	236.09	1.73	0.00	0.31	0.00	0.00	0.00	0.00	
54.008	236.10	1.74	0.00	0.36	0.00	0.00	0.00	0.00	

55.018	236.12	1.74	0.00	0.44	0.00	0.00	0.00	0.00
56.035	236.15	1.74	0.00	0.56	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
57.032	236.18	1.75	0.00	0.78	0.00	0.00	0.00	0.00	
58.009	236.22	1.76	0.00	1.06	0.00	0.00	0.00	0.00	
59.001	236.29	1.77	0.00	2.08	0.00	0.00	0.00	0.00	
60.005	236.82	1.86	0.00	20.74	0.00	0.00	0.00	0.00	
61.005	237.34	1.95	0.00	3.44	0.00	0.00	0.00	0.00	
62.005	237.46	1.97	0.00	2.00	0.00	0.00	0.00	0.00	
63.016	237.53	1.98	0.00	1.43	0.00	0.00	0.00	0.00	
64.031	237.59	1.99	0.00	1.24	0.00	0.00	0.00	0.00	
65.024	237.63	2.00	0.00	0.88	0.00	0.00	0.00	0.00	
66.031	237.67	2.00	0.00	0.88	0.00	0.00	0.00	0.00	
67.049	237.71	2.01	0.00	0.88	0.00	0.00	0.00	0.00	
68.034	237.74	2.01	0.00	0.78	0.00	0.00	0.00	0.00	
69.067	237.77	2.02	0.00	0.60	0.00	0.00	0.00	0.00	
70.021	237.79	2.02	0.00	0.60	0.00	0.00	0.00	0.00	
71.054	237.82	2.03	0.00	0.59	0.00	0.00	0.00	0.00	
72.008	237.84	2.03	0.00	0.50	0.00	0.00	0.00	0.00	
73.041	237.85	2.03	0.00	0.31	0.00	0.00	0.00	0.00	
74.074	237.87	2.04	0.00	0.31	0.00	0.00	0.00	0.00	
75.028	237.88	2.04	0.00	0.31	0.00	0.00	0.00	0.00	
76.061	237.89	2.04	0.00	0.31	0.00	0.00	0.00	0.00	
77.014	237.90	2.04	0.00	0.32	0.00	0.00	0.00	0.00	
78.048	237.92	2.04	0.00	0.32	0.00	0.00	0.00	0.00	
79.001	237.93	2.05	0.00	0.32	0.00	0.00	0.00	0.00	
80.034	237.94	2.05	0.00	0.32	0.00	0.00	0.00	0.00	
81.010	237.96	2.05	0.00	0.31	0.00	0.00	0.00	0.00	
82.028	237.97	2.05	0.00	0.32	0.00	0.00	0.00	0.00	
83.004	237.98	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
84.062	237.99	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
85.063	238.01	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
86.048	238.02	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
87.048	238.03	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
88.048	238.05	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
89.048	238.06	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
90.048	238.07	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
91.048	238.08	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
92.048	238.10	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
93.031	238.11	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
94.005	238.12	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
95.007	238.13	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
96.021	238.14	2.08	0.00	0.00	0.00	0.00	0.00	0.00	
96.054	238.14	2.08	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 999  
 0.000 196.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 1.050 196.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00







LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
51.031	196.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
52.025	196.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
53.030	196.77	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
54.008	196.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
55.018	196.83	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
56.035	196.87	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
57.032	196.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
58.009	196.93	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
59.001	196.97	0.00	0.00	0.01	0.00	0.00	0.00	0.00	
60.005	197.00	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
61.005	197.03	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
62.005	197.06	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
63.016	197.08	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
64.031	197.11	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
65.024	197.14	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
66.031	197.17	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
67.049	197.20	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
68.034	197.22	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
69.067	197.25	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
70.021	197.28	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
71.054	197.31	0.00	0.00	0.15	0.00	0.00	0.00	0.00	
72.008	197.33	0.00	0.00	0.15	0.00	0.00	0.00	0.00	
73.041	197.36	0.00	0.00	0.14	0.00	0.00	0.00	0.00	
74.074	197.39	0.00	0.00	0.14	0.00	0.00	0.00	0.00	
75.028	197.42	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
76.061	197.45	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
77.014	197.47	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
78.048	197.50	0.00	0.00	0.12	0.00	0.00	0.00	0.00	
79.001	197.53	0.00	0.00	0.12	0.00	0.00	0.00	0.00	
80.034	197.56	0.00	0.00	0.11	0.00	0.00	0.00	0.00	
81.010	197.58	0.00	0.00	0.11	0.00	0.00	0.00	0.00	
82.028	197.61	0.00	0.00	0.11	0.00	0.00	0.00	0.00	
83.004	197.64	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
84.062	197.67	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
85.063	197.70	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
86.048	197.72	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
87.048	197.75	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
88.048	197.78	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
89.048	197.81	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
90.048	197.83	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
91.048	197.86	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
92.048	197.89	0.00	0.00	0.08	0.00	0.00	0.00	0.00	
93.031	197.92	0.00	0.00	0.08	0.00	0.00	0.00	0.00	
94.005	197.94	0.00	0.00	0.08	0.00	0.00	0.00	0.00	
95.007	197.97	0.00	0.00	0.08	0.00	0.00	0.00	0.00	





**"PONDS" INFILTRATION ANALYSIS  
25 YEAR-96 HOUR STORM**

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And Robert D. Casper

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND1  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 450.00  
Equivalent Pond Width, [W] (ft): 85.00

Base Of Aquifer Elevation, [B] (ft above datum): 189.18  
Water Table Elevation, [WT] (ft above datum): 189.28  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 42.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 21.00  
Maximum area for unsaturated infiltration, (sq ft): 35165

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
200.000	11173.0
201.000	15030.0
202.000	19325.0
203.000	24007.0
204.000	29436.0
205.000	35165.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	15.94
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	134436

Stage

-----

Peak Stage, (ft datum):	202.47
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	4.9360
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	134436

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND2A  
Engineer: KK  
Date: 6/22/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 60.00

Base Of Aquifer Elevation, [B] (ft above datum): 186.00  
Water Table Elevation, [WT] (ft above datum): 186.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 28.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 14.00  
Maximum area for unsaturated infiltration, (sq ft): 21703

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
192.000	8544.0
193.000	10486.0
194.000	12528.0
195.000	14671.0
196.000	16915.0
197.000	19259.0
198.000	21703.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	20.41
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	172484

Stage

-----

Peak Stage, (ft datum):	197.05
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	4.6433
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	135103



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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND2B  
Engineer: XX  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 830.00  
Equivalent Pond Width, [W] (ft): 80.00

Base Of Aquifer Elevation, [B] (ft above datum): 159.00  
Water Table Elevation, [WT] (ft above datum): 159.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 27.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 13.50  
Maximum area for unsaturated infiltration, (sq ft): 75394

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
182.000	53642.0
183.000	60792.0
184.000	68043.0
185.000	75394.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	43.08
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	363741

Stage  
-----

Peak Stage, (ft datum):	183.84
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	10.3128
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	363741

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND2C  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 580.00  
Equivalent Pond Width, [W] (ft): 220.00

Base Of Aquifer Elevation, [B] (ft above datum): 150.00  
Water Table Elevation, [WT] (ft above datum): 150.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 29.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes

Unsaturated vertical infiltration rate, (ft/day): 14.50

Maximum area for unsaturated infiltration, (sq ft): 53126

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
163.000	59806.0
164.000	66928.0
165.000	74127.0
166.000	92834.0
167.000	112932.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	30.17
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	254366

Stage  
-----

Peak Stage, (ft datum):	165.08
Time, (hrs):	63.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	6.9325
Time, (hrs):	94.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	254368

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Retention Pond Recovery Analysis - Inflow Hydrograph

---

1. Job Information

Job Name: POND3  
Engineer: KK  
Date: 6/29/98

2. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 120.00

Base Of Aquifer Elevation, [B] (ft above datum): 154.30  
Water Table Elevation, [WT] (ft above datum): 154.40  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 26.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 13.00  
Maximum area for unsaturated infiltration, (sq ft): 86562

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
165.000	25902.0
166.000	29827.0
167.000	33926.0
168.000	38307.0
169.000	42990.0
170.000	47981.0
171.000	53382.0
172.000	58983.0
173.000	64842.0
174.000	79437.0
175.000	86562.0



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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----  
Peak Inflow Rate, (cfs): 65.67  
Time, (hrs): 60.00  
  
Cumulative Inflow Volume, (ft<sup>3</sup>): 561960

Stage

-----  
Peak Stage, (ft datum): 171.08  
Time, (hrs): 62.00

Overflow Discharge

-----  
Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00  
  
Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----  
Peak Infiltration Rate, (cfs): 8.0853  
Time, (hrs): 62.00  
  
Cumulative Infiltration Volume, (ft<sup>3</sup>): 491994

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND4  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 166.78  
Water Table Elevation, [WT] (ft above datum): 166.88  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 38.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 19.00  
Maximum area for unsaturated infiltration, (sq ft): 71144

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
177.000	31738.0
178.000	36864.0
179.000	42308.0
180.000	48005.0
181.000	53614.0
182.000	59360.0
183.000	70317.0
184.000	88888.0
185.000	117772.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	34.85
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	294210

Stage

-----

Peak Stage, (ft datum):	179.29
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	9.4196
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	294210

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Retention Pond Recovery Analysis - Inflow Hydrograph

---

Job Information

Job Name: POND6  
Engineer: KK  
Date: 7/20/98

Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 169.51  
Water Table Elevation, [WT] (ft above datum): 169.61  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 43.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 20.00  
Maximum area for unsaturated infiltration, (sq ft): 61200

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
203.000	56366.0
204.000	61276.0

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II. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----  
Peak Inflow Rate, (cfs): 12.92  
Time, (hrs): 60.00  
Cumulative Inflow Volume, (ft<sup>3</sup>): 113080

Stage

-----  
Peak Stage, (ft datum): 175.77  
Time, (hrs): 96.00

Overflow Discharge

-----  
Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00  
Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----  
Peak Infiltration Rate, (cfs): 7.2553  
Time, (hrs): 60.00  
Cumulative Infiltration Volume, (ft<sup>3</sup>): 113080

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND7  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 360.00

Base Of Aquifer Elevation, [B] (ft above datum): 141.00  
Water Table Elevation, [WT] (ft above datum): 141.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 25.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 82379.00  
Maximum area for unsaturated infiltration, (sq ft): 13

Groundwater mound intersects pond bottom?: Yes



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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
149.000	2470.0
150.000	4992.0
155.000	24257.0
160.000	46329.0
165.000	73571.0
170.000	155713.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	68.59
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	578292

Stage  
-----

Peak Stage, (ft datum):	156.99
Time, (hrs):	60.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	38.7256
Time, (hrs):	60.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	556190

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Retention Pond Recovery Analysis - Inflow Hydrograph

---

Job Information

Job Name: PONDS  
Engineer: KK  
Date: 7/20/98

Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 232.00  
Water Table Elevation, [WT] (ft above datum): 232.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 19.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length?: No

Is there a ditch parallel to the pond width?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 10.00  
Maximum area for unsaturated infiltration, (sq ft): 51038

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
235.000	12733.0
236.000	17045.0
237.000	21240.0
238.000	30362.0
239.000	51919.0
240.000	106391.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----  
Peak Inflow Rate, (cfs): 11.64  
Time, (hrs): 60.00  
  
Cumulative Inflow Volume, (ft<sup>3</sup>): 98770

Stage

-----  
Peak Stage, (ft datum): 237.03  
Time, (hrs): 61.00

Overflow Discharge

-----  
Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00  
  
Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----  
Peak Infiltration Rate, (cfs): 2.4461  
Time, (hrs): 62.00  
  
Cumulative Infiltration Volume, (ft<sup>3</sup>): 94603

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND10  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 240.00

Base Of Aquifer Elevation, [B] (ft above datum): 200.25  
Water Table Elevation, [WT] (ft above datum): 200.35  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 40.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 20.00  
Maximum area for unsaturated infiltration, (sq ft): 68074

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
210.000	4032.0
211.000	7773.0
212.000	16102.0
213.000	30736.0
214.000	47421.0
215.000	55253.0
216.000	61490.0
217.000	67885.0
218.000	75221.0
219.000	84246.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	30.38
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	256356

Stage

-----

Peak Stage, (ft datum):	214.19
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	10.4336
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	256357



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Retention Pond Recovery Analysis - Inflow Hydrograph

---

I. Job Information

Job Name: POND11  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 370.00  
Equivalent Pond Width, [W] (ft): 70.00

Base Of Aquifer Elevation, [B] (ft above datum): 197.80  
Water Table Elevation, [WT] (ft above datum): 197.90  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 26.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 13.00  
Maximum area for unsaturated infiltration, (sq ft): 36500

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
214.000	22373.0
215.000	25831.0
216.000	29390.0
217.000	33049.0
218.000	36809.0

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III. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----  
Peak Inflow Rate, (cfs): 24.96  
Time, (hrs): 60.00  
Cumulative Inflow Volume, (ft<sup>3</sup>): 210515

Stage

-----  
Peak Stage, (ft datum): 216.74  
Time, (hrs): 61.00

Overflow Discharge

-----  
Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00  
Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----  
Peak Infiltration Rate, (cfs): 4.7868  
Time, (hrs): 62.00  
Cumulative Infiltration Volume, (ft<sup>3</sup>): 210516

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND12  
Engineer: KK  
Date: 6/29

II. Input Data

Equivalent Pond Length, [L] (ft): 170.00  
Equivalent Pond Width, [W] (ft): 50.00

Base Of Aquifer Elevation, [B] (ft above datum): 197.70  
Water Table Elevation, [WT] (ft above datum): 197.80  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 44.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 22.00  
Maximum area for unsaturated infiltration, (sq ft): 28509

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
-----	-----
205.000	1802.0
206.000	3016.0
207.000	4331.0
208.000	5746.0
209.000	7262.0
210.000	8879.0
211.000	10596.0
212.000	12413.0
213.000	14331.0
214.000	21124.0
215.000	24766.0
216.000	28509.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	32.14
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	271208

Stage

-----

Peak Stage, (ft datum):	215.67
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	6.7850
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	223625

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND14  
Engineer: XX  
Date: 7/20/98

Input Data

Equivalent Pond Length, [L] (ft): 200.00  
Equivalent Pond Width, [W] (ft): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 225.35  
Water Table Elevation, [WT] (ft above datum): 225.45  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 15.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 8.00  
Maximum area for unsaturated infiltration, (sq ft): 19390

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
234.000	11799.0
235.000	13849.0
236.000	16000.0
237.000	18251.0
238.000	20603.0



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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----  
Peak Inflow Rate, (cfs): 10.80  
Time, (hrs): 60.00  
Cumulative Inflow Volume, (ft<sup>3</sup>): 91352

Stage

-----  
Peak Stage, (ft datum): 236.45  
Time, (hrs): 61.00

Overflow Discharge

-----  
Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00  
Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----  
Peak Infiltration Rate, (cfs): 1.8944  
Time, (hrs): 67.00  
Cumulative Infiltration Volume, (ft<sup>3</sup>): 88567

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND15  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 460.00  
Equivalent Pond Width, [W] (ft): 70.00

Base Of Aquifer Elevation, [B] (ft above datum): 187.50  
Water Table Elevation, [WT] (ft above datum): 187.60  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 32.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 16.00  
Maximum area for unsaturated infiltration, (sq ft): 61245

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
194.000	15942.0
195.000	19950.0
196.000	26789.0
197.000	32495.0
198.000	38594.0
199.000	46652.0
200.000	53840.0
201.000	61245.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	34.39
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	289952

Stage

-----

Peak Stage, (ft datum):	198.07
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	7.3214
Time, (hrs):	65.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	250093

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Retention Pond Recovery Analysis - Inflow Hydrograph

---

I. Job Information

Job Name: POND16  
Engineer: KK  
Date: 7/20/98

I. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 148.92  
Water Table Elevation, [WT] (ft above datum): 149.02  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 33.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 17.00  
Maximum area for unsaturated infiltration, (sq ft): 94494

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
163.000	45244.0
164.000	50863.0
165.000	63760.0
166.000	70145.0
167.000	86249.0
168.000	94494.0
169.000	103404.0

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III. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	41.62
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	352208

Stage  
-----

Peak Stage, (ft datum):	164.93
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	11.8579
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	352209

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND18  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 1120.00  
Equivalent Pond Width, [W] (ft): 115.00

Base Of Aquifer Elevation, [B] (ft above datum): 154.40  
Water Table Elevation, [WT] (ft above datum): 154.50  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 40.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 20.00  
Maximum area for unsaturated infiltration, (sq ft): 126563

Groundwater mound intersects pond bottom?: Yes



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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
165.000	54929.0
166.000	63859.0
167.000	74662.0
168.000	86031.0
169.000	102410.0
170.000	117830.0
171.000	144184.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	53.72
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	453589

Stage

-----

Peak Stage, (ft datum):	166.88
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	16.3594
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	453589

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Retention Pond Recovery Analysis - Inflow Hydrograph

---

I. Job Information

Job Name: POND19  
Engineer: KK  
Date: 6/29/98

Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 140.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.20  
Water Table Elevation, [WT] (ft above datum): 165.30  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 20.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 10.00  
Maximum area for unsaturated infiltration, (sq ft): 48337

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
178.000	31630.0
179.000	34770.0
180.000	38011.0
181.000	41352.0
182.000	44794.0
183.000	48337.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	23.65
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	199413

Stage  
-----

Peak Stage, (ft datum):	179.97
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	4.3688
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	199413

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND20  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 350.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 187.00  
Water Table Elevation, [WT] (ft above datum): 187.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 12.00  
Maximum area for unsaturated infiltration, (sq ft): 49575

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
191.000	17861.0
192.000	21422.0
193.000	27278.0
194.000	34259.0
195.000	41553.0
196.000	50338.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	18.28
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	154099

Stage

-----

Peak Stage, (ft datum):	193.34
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	4.0251
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	121789



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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND21  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 370.00  
Equivalent Pond Width, [W] (ft): 250.00

Base Of Aquifer Elevation, [B] (ft above datum): 182.00  
Water Table Elevation, [WT] (ft above datum): 182.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 14.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 7.00  
Maximum area for unsaturated infiltration, (sq ft): 93128

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
190.000	21423.0
191.000	34973.0
192.000	48552.0
193.000	59854.0
194.000	71514.0
195.000	81528.0
196.000	93128.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	59.19
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	501594

Stage  
-----

Peak Stage, (ft datum):	194.58
Time, (hrs):	62.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	6.2374
Time, (hrs):	63.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	366446

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND22  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 670.00  
Equivalent Pond Width, [W] (ft): 110.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.00  
Water Table Elevation, [WT] (ft above datum): 165.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 11.50  
Maximum area for unsaturated infiltration, (sq ft): 68868

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
169.000	11428.0
170.000	14734.0
171.000	18283.0
172.000	22005.0
173.000	27913.0
174.000	35306.0
175.000	51427.0
176.000	68868.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	27.20
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	229614

Stage

-----

Peak Stage, (ft datum):	173.66
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	4.3363
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	207526

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Retention Pond Recovery Analysis - Inflow Hydrograph

---

I. Job Information

Job Name: POND23  
Engineer: KK  
Date: 6/29/98

Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 400.00

Base Of Aquifer Elevation, [B] (ft above datum): 122.00  
Water Table Elevation, [WT] (ft above datum): 122.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 11.50  
Maximum area for unsaturated infiltration, (sq ft): 104788

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
134.000	10714.0
135.000	14385.0
136.000	18695.0
137.000	23006.0
138.000	27317.0
139.000	31627.0
140.000	35938.0
141.000	41998.0
142.000	48059.0
143.000	54120.0
144.000	60180.0
145.000	66241.0
146.000	73950.0
147.000	81660.0
150.000	104788.0



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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----  
Peak Inflow Rate, (cfs): 103.50  
Time, (hrs): 60.00  
  
Cumulative Inflow Volume, (ft<sup>3</sup>): 872691

Stage

-----  
Peak Stage, (ft datum): 145.59  
Time, (hrs): 62.00

Overflow Discharge

-----  
Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00  
  
Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----  
Peak Infiltration Rate, (cfs): 10.2308  
Time, (hrs): 82.00  
  
Cumulative Infiltration Volume, (ft<sup>3</sup>): 815997

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND24  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 530.00  
Equivalent Pond Width, [W] (ft): 480.00

Base Of Aquifer Elevation, [B] (ft above datum): 101.50  
Water Table Elevation, [WT] (ft above datum): 101.60  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 31.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 15.50  
Maximum area for unsaturated infiltration, (sq ft): 174170

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
112.000	82911.0
113.000	91524.0
114.000	101700.0
115.000	122694.0
116.000	130872.0
117.000	152453.0
118.000	173761.0
119.000	187863.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	163.28
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	1378484

Stage

-----

Peak Stage, (ft datum):	116.80
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	26.4106
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	968937

**"PONDS" RECOVERY ANALYSIS  
TREATMENT VOLUME**

Since every basin consists of less than 40 percent impervious, the following calculations for all basins are based on formula:

$$V_T = \frac{1}{2} \text{ (area)} + \frac{1}{2} \text{ (area - for volume treatment)} = 1 \text{ (area)}$$

Per 40C - 42 FAC

$$V_{\text{TPOND1}} = 1 \text{''} \times (341,508 \text{ Sq. Ft.}) = 28,459 \text{ Cu. Ft.}$$

$$V_{\text{TP2A}} = 1 \text{''} \times (376,356 \text{ Sq. Ft.}) = 31,363 \text{ Cu. Ft.}$$

$$V_{\text{TP2B}} = 1 \text{''} \times (816,312 \text{ Sq. Ft.}) = 68,026 \text{ Cu. Ft.}$$

$$V_{\text{TP2C}} = 1 \text{''} \times (646,428 \text{ Sq. Ft.}) = 53,869 \text{ Cu. Ft.}$$

$$V_{\text{TP3}} = 1 \text{''} \times (1,027,584 \text{ Sq. Ft.}) = 85,632 \text{ Cu. Ft.}$$

$$V_{\text{TP4}} = 1 \text{''} \times (801,060 \text{ Sq. Ft.}) = 66,755 \text{ Cu. Ft.}$$

$$V_{\text{TP6}} = 1 \text{''} \times (456,072 \text{ Sq. Ft.}) = 38,006 \text{ Cu. Ft.}$$

$$V_{\text{TP7}} = 1 \text{''} \times (1,422,228 \text{ Sq. Ft.}) = 118,519 \text{ Cu. Ft.}$$

$$V_{\text{TP8}} = 1 \text{''} \times (301,428 \text{ Sq. Ft.}) = 25,119 \text{ Cu. Ft.}$$

$$V_{\text{TP10}} = 1 \text{''} \times (592,416 \text{ Sq. Ft.}) = 49,368 \text{ Cu. Ft.}$$

$$V_{\text{TP11}} = 1 \text{''} \times (501,804 \text{ Sq. Ft.}) = 41,817 \text{ Cu. Ft.}$$

$$V_{\text{TP12}} = 1 \text{''} \times (626,820 \text{ Sq. Ft.}) = 52,235 \text{ Cu. Ft.}$$

$$V_{\text{TP14}} = 1 \text{''} \times (208,644 \text{ Sq. Ft.}) = 17,387 \text{ Cu. Ft.}$$

$$V_{\text{TP15}} = 1 \text{''} \times (697,824 \text{ Sq. Ft.}) = 58,152 \text{ Cu. Ft.}$$

$$V_{\text{TP16}} = 1 \text{''} \times (747,480 \text{ Sq. Ft.}) = 62,290 \text{ Cu. Ft.}$$

$$V_{\text{TP18}} = 1 \text{''} \times (1,046,736 \text{ Sq. Ft.}) = 87,228 \text{ Cu. Ft.}$$

$$V_{\text{TP19}} = 1 \text{''} \times (490,476 \text{ Sq. Ft.}) = 40,873 \text{ Cu. Ft.}$$

$$V_{\text{TP20}} = 1 \text{''} \times (378,972 \text{ Sq. Ft.}) = 31,581 \text{ Cu. Ft.}$$

$$V_{\text{TP21}} = 1 \text{''} \times (1,036,284 \text{ Sq. Ft.}) = 86,357 \text{ Cu. Ft.}$$

$$V_{TP22} = 1" \times (625,080 \text{ Sq. Ft.}) = 52,090 \text{ Cu. Ft.}$$

$$V_{TP23} = 1" \times (2,217,204 \text{ Sq. Ft.}) = 184,767 \text{ Cu. Ft.}$$

$$V_{TP24} = 1" \times (3,752,688 \text{ Sq. Ft.}) = 312,724 \text{ Cu. Ft.}$$

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND1  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	450.00
Equivalent Pond Width, [W] (ft):	85.00
Pond Bottom Elevation, [PB] (ft above datum):	200.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	189.18
Water Table Elevation, [WT] (ft above datum):	189.28
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	42.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.00
Runoff Volume, [V] (cubic feet)	28459.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0354
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	28459.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0354
Total Recovered Volume, [V] (ft <sup>3</sup> ):	28459.00



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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND2A  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	60.00
Pond Bottom Elevation, [PB] (ft above datum):	192.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	186.00
Water Table Elevation, [WT] (ft above datum):	186.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	28.00
Pillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.00
Runoff Volume, [V] (cubic feet)	31363.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0933
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	31363.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0933
Total Recovered Volume, [V] (ft <sup>3</sup> ):	31363.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND2B  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft): 830.00  
Equivalent Pond Width, [W] (ft): 80.00  
Pond Bottom Elevation, [PB] (ft above datum): 182.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 159.00  
Water Table Elevation, [WT] (ft above datum): 159.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 27.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 13.50

Runoff Volume, [V] (cubic feet) 68026.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.0759  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 68026.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.0759  
Total Recovered Volume, [V] (ft<sup>3</sup>): 68026.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND2C  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	582.00
Equivalent Pond Width, [W] (ft):	220.00
Pond Bottom Elevation, [PB] (ft above datum):	163.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	150.00
Water Table Elevation, [WT] (ft above datum):	150.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	29.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.50
Runoff Volume, [V] (cubic feet)	53869.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0290
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	53869.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0290
Total Recovered Volume, [V] (ft <sup>3</sup> ):	53869.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND3  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	330.00
Equivalent Pond Width, [W] (ft):	120.00
Pond Bottom Elevation, [PB] (ft above datum):	165.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	154.30
Water Table Elevation, [WT] (ft above datum):	154.40
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	26.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.00
Runoff Volume, [V] (cubic feet)	85632.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1663
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	85632.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1663
Total Recovered Volume, [V] (ft <sup>3</sup> ):	85632.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND4  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	177.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	166.78
Water Table Elevation, [WT] (ft above datum):	166.88
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	38.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	19.00
Runoff Volume, [V] (cubic feet)	66755.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0439
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	66755.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0439
Total Recovered Volume, [V] (ft <sup>3</sup> ):	66755.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND6  
Engineer: KR  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	420.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	203.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	169.51
Water Table Elevation, [WT] (ft above datum):	169.61
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	43.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.50
Runoff Volume, [V] (cubic feet)	38006.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0210
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	38006.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0210
Total Recovered Volume, [V] (ft <sup>3</sup> ):	38006.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND7  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	360.00
Pond Bottom Elevation, [PB] (ft above datum):	149.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	141.00
Water Table Elevation, [WT] (ft above datum):	141.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	25.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	12.50
Runoff Volume, [V] (cubic feet)	118519.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0439
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	118519.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0439
Total Recovered Volume, [V] (ft <sup>3</sup> ):	118519.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: PONDS  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	235.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	232.00
Water Table Elevation, [WT] (ft above datum):	232.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	19.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	9.50
Runoff Volume, [V] (cubic feet)	25119.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0220
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	25119.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0220
Total Recovered Volume, [V] (ft <sup>3</sup> ):	25119.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND10  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	240.00
Pond Bottom Elevation, [PB] (ft above datum):	210.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	200.25
Water Table Elevation, [WT] (ft above datum):	200.35
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	49368.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0257
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	49368.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0257
Total Recovered Volume, [V] (ft <sup>3</sup> ):	49368.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND11  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	370.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	214.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.80
Water Table Elevation, [WT] (ft above datum):	197.90
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	26.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.00
Runoff Volume, [V] (cubic feet)	41817.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1242
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	41817.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1242
Total Recovered Volume, [V] (ft <sup>3</sup> ):	41817.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND12  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	170.00
Equivalent Pond Width, [W] (ft):	50.00
Pond Bottom Elevation, [PB] (ft above datum):	205.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.70
Water Table Elevation, [WT] (ft above datum):	197.81
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	44.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	22.00
Runoff Volume, [V] (cubic feet)	52235.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0980
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	18334.51

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.6482
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	33900.49
Maximum Radius Of Influence, [R] (ft):	56.33
Maximum Driving Head, [Hmax] (ft):	11.178
Minimum Driving Head, [Hmin] (ft):	7.190

TOTAL

Total Recovery Time, [T] (days):	0.7463
Total Recovered Volume, [V] (ft <sup>3</sup> ):	52235.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND14  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	200.00
Equivalent Pond Width, [W] (ft):	100.00
Pond Bottom Elevation, [PB] (ft above datum):	234.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	225.35
Water Table Elevation, [WT] (ft above datum):	225.45
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	15.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	7.50
Runoff Volume, [V] (cubic feet)	17387.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1159
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	17387.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1159
Total Recovered Volume, [V] (ft <sup>3</sup> ):	17387.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND15  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	460.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	194.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	187.50
Water Table Elevation, [WT] (ft above datum):	187.60
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	32.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.00
Runoff Volume, [V] (cubic feet)	58152.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1129
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	58152.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1129
Total Recovered Volume, [V] (ft <sup>3</sup> ):	58152.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND16  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	163.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	148.92
Water Table Elevation, [WT] (ft above datum):	149.02
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	33.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.50
Runoff Volume, [V] (cubic feet)	62290.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0315
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	62290.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0315
Total Recovered Volume, [V] (ft <sup>3</sup> ):	62290.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND18  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	1120.00
Equivalent Pond Width, [W] (ft):	115.00
Pond Bottom Elevation, [PB] (ft above datum):	165.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	154.40
Water Table Elevation, [WT] (ft above datum):	154.50
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	87228.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0339
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	87228.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0339
Total Recovered Volume, [V] (ft <sup>3</sup> ):	87228.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND19  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	330.00
Equivalent Pond Width, [W] (ft):	140.00
Pond Bottom Elevation, [PB] (ft above datum):	178.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	165.20
Water Table Elevation, [WT] (ft above datum):	165.30
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	20.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	10.00
Runoff Volume, [V] (cubic feet)	40873.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0885
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	40873.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0885
Total Recovered Volume, [V] (ft <sup>3</sup> ):	40873.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND20  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	350.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	191.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	187.00
Water Table Elevation, [WT] (ft above datum):	187.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	23.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	11.50
Runoff Volume, [V] (cubic feet)	31581.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0392
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	31581.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0392
Total Recovered Volume, [V] (ft <sup>3</sup> ):	31581.00

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Retention Pond Recovery Analysis

I. Job Information

Job Name: POND21  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	370.00
Equivalent Pond Width, [W] (ft):	250.00
Pond Bottom Elevation, [PB] (ft above datum):	190.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	182.00
Water Table Elevation, [WT] (ft above datum):	182.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	14.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	7.00
Runoff Volume, [V] (cubic feet)	86357.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1334
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	86357.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1334
Total Recovered Volume, [V] (ft <sup>3</sup> ):	86357.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND22  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	670.00
Equivalent Pond Width, [W] (ft):	110.00
Pond Bottom Elevation, [PB] (ft above datum):	169.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	165.00
Water Table Elevation, [WT] (ft above datum):	165.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	23.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	11.50
Runoff Volume, [V] (cubic feet)	52090.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0615
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	52090.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0615
Total Recovered Volume, [V] (ft <sup>3</sup> ):	52090.00

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### Retention Pond Recovery Analysis

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#### I. Job Information

Job Name: POND23  
Engineer: KK  
Date: 7/29/98

#### II. Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 400.00  
Pond Bottom Elevation, [PB] (ft above datum): 130.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 122.00  
Water Table Elevation, [WT] (ft above datum): 122.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 11.50

Runoff Volume, [V] (cubic feet) 184767.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

#### III. Results

##### UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.0956  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 184767.00

##### SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

##### TOTAL

Total Recovery Time, [T] (days): 0.0956  
Total Recovered Volume, [V] (ft<sup>3</sup>): 184767.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND24  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	530.00
Equivalent Pond Width, [W] (ft):	480.00
Pond Bottom Elevation, [PB] (ft above datum):	112.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	101.45
Water Table Elevation, [WT] (ft above datum):	101.55
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	31.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	15.50
Runoff Volume, [V] (cubic feet)	312724.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0793
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	312724.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0793
Total Recovered Volume, [V] (ft <sup>3</sup> ):	312724.00

**"PONDS" RECOVERY ANALYSIS  
TOTAL RUNOFF VOLUME**

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND1  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	450.00
Equivalent Pond Width, [W] (ft):	85.00
Pond Bottom Elevation, [PB] (ft above datum):	200.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	189.18
Water Table Elevation, [WT] (ft above datum):	189.28
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	42.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.00
Runoff Volume, [V] (cubic feet)	125474.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1531
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	123012.02

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0003
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	2461.98
Maximum Radius Of Influence, [R] (ft):	1.43
Maximum Driving Head, [Hmax] (ft):	10.784
Minimum Driving Head, [Hmin] (ft):	10.720

TOTAL

Total Recovery Time, [T] (days):	0.1535
Total Recovered Volume, [V] (ft <sup>3</sup> ):	125474.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND2A  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	60.00
Pond Bottom Elevation, [PB] (ft above datum):	192.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	186.00
Water Table Elevation, [WT] (ft above datum):	186.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	28.00
Pillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.00
Runoff Volume, [V] (cubic feet)	161595.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1264
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	42479.96

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	4.4041
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	119115.05
Maximum Radius Of Influence, [R] (ft):	115.78
Maximum Driving Head, [Hmax] (ft):	10.863
Minimum Driving Head, [Hmin] (ft):	5.900

TOTAL

Total Recovery Time, [T] (days):	4.5305
Total Recovered Volume, [V] (ft <sup>3</sup> ):	161595.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND2B  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	830.00
Equivalent Pond Width, [W] (ft):	80.00
Pond Bottom Elevation, [PB] (ft above datum):	182.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	159.00
Water Table Elevation, [WT] (ft above datum):	159.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	27.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.50
Runoff Volume, [V] (cubic feet)	340530.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.3799
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	340530.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.3799
Total Recovered Volume, [V] (ft <sup>3</sup> ):	340530.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND2C  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 582.00  
Equivalent Pond Width, [W] (ft): 220.00  
Pond Bottom Elevation, [PB] (ft above datum): 163.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 150.00  
Water Table Elevation, [WT] (ft above datum): 150.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 29.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 14.50

Runoff Volume, [V] (cubic feet) 229315.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1235  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 229315.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.1235  
Total Recovered Volume, [V] (ft<sup>3</sup>): 229315.00

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Retention Pond Recovery Analysis

I. Job Information

Job Name: POND3  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 120.00  
Pond Bottom Elevation, [PB] (ft above datum): 165.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 154.30  
Water Table Elevation, [WT] (ft above datum): 154.40  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 26.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 13.00

Runoff Volume, [V] (cubic feet) 529004.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.2446  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 125928.08

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 8.3100  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 403075.94  
Maximum Radius Of Influence, [R] (ft): 194.05  
Maximum Driving Head, [Hmax] (ft): 20.779  
Minimum Driving Head, [Hmin] (ft): 10.600

TOTAL

Total Recovery Time, [T] (days): 8.5546  
Total Recovered Volume, [V] (ft<sup>3</sup>): 529004.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND4  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	177.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	166.78
Water Table Elevation, [WT] (ft above datum):	166.88
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	38.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	19.00
Runoff Volume, [V] (cubic feet)	274150.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1598
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	242879.89

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0538
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	31270.11
Maximum Radius Of Influence, [R] (ft):	16.68
Maximum Driving Head, [Hmax] (ft):	10.511
Minimum Driving Head, [Hmin] (ft):	10.120

TOTAL

Total Recovery Time, [T] (days):	0.2135
Total Recovered Volume, [V] (ft <sup>3</sup> ):	274150.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND6  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	420.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	203.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	169.51
Water Table Elevation, [WT] (ft above datum):	169.61
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	43.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.50
Runoff Volume, [V] (cubic feet)	104466.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0578
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	104466.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0578
Total Recovered Volume, [V] (ft <sup>3</sup> ):	104466.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND7  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 360.00  
Pond Bottom Elevation, [PB] (ft above datum): 149.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 141.00  
Water Table Elevation, [WT] (ft above datum): 141.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 25.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 12.50

Runoff Volume, [V] (cubic feet) 540164.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1896  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 511919.63

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0564  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 28244.38  
Maximum Radius Of Influence, [R] (ft): 12.25  
Maximum Driving Head, [Hmax] (ft): 8.031  
Minimum Driving Head, [Hmin] (ft): 7.900

TOTAL

Total Recovery Time, [T] (days): 0.2460  
Total Recovered Volume, [V] (ft<sup>3</sup>): 540164.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: PONDS  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	235.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	232.00
Water Table Elevation, [WT] (ft above datum):	232.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	19.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	9.50
Runoff Volume, [V] (cubic feet)	91795.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0805
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	91795.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0805
Total Recovered Volume, [V] (ft <sup>3</sup> ):	91795.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND10  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	240.00
Pond Bottom Elevation, [PB] (ft above datum):	210.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	200.35
Water Table Elevation, [WT] (ft above datum):	200.45
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	239820.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1249
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	239820.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1249
Total Recovered Volume, [V] (ft <sup>3</sup> ):	239820.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND11  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	370.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	214.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.80
Water Table Elevation, [WT] (ft above datum):	197.90
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	25.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.00
Runoff Volume, [V] (cubic feet)	196788.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.3715
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	125097.05

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.1647
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	71690.95
Maximum Radius Of Influence, [R] (ft):	31.39
Maximum Driving Head, [Hmax] (ft):	18.868
Minimum Driving Head, [Hmin] (ft):	16.100

TOTAL

Total Recovery Time, [T] (days):	0.5362
Total Recovered Volume, [V] (ft <sup>3</sup> ):	196788.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND12  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	170.00
Equivalent Pond Width, [W] (ft):	50.00
Pond Bottom Elevation, [PB] (ft above datum):	205.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.70
Water Table Elevation, [WT] (ft above datum):	197.81
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	44.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	22.00
Runoff Volume, [V] (cubic feet)	253713.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0980
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	18334.51

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	6.6094
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	235378.50
Maximum Radius Of Influence, [R] (ft):	234.43
Maximum Driving Head, [Hmax] (ft):	34.882
Minimum Driving Head, [Hmin] (ft):	7.190

TOTAL

Total Recovery Time, [T] (days):	6.7074
Total Recovered Volume, [V] (ft <sup>3</sup> ):	253713.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND14  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	200.00
Equivalent Pond Width, [W] (ft):	100.00
Pond Bottom Elevation, [PB] (ft above datum):	234.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	225.35
Water Table Elevation, [WT] (ft above datum):	225.45
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	15.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	7.50
Runoff Volume, [V] (cubic feet)	85646.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.3420
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	51300.02

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.8778
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	34345.98
Maximum Radius Of Influence, [R] (ft):	39.26
Maximum Driving Head, [Hmax] (ft):	10.267
Minimum Driving Head, [Hmin] (ft):	8.550

TOTAL

Total Recovery Time, [T] (days):	1.2198
Total Recovered Volume, [V] (ft <sup>3</sup> ):	85646.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND15  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	460.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	194.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	187.50
Water Table Elevation, [WT] (ft above datum):	187.60
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	32.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.00
Runoff Volume, [V] (cubic feet)	270835.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1200
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	61823.95

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	6.2372
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	209011.06
Maximum Radius Of Influence, [R] (ft):	156.81
Maximum Driving Head, [Hmax] (ft):	12.891
Minimum Driving Head, [Hmin] (ft):	6.400

TOTAL

Total Recovery Time, [T] (days):	6.3572
Total Recovered Volume, [V] (ft <sup>3</sup> ):	270835.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND16  
Engineer: KK  
Date: 9/23/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	163.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	148.92
Water Table Elevation, [WT] (ft above datum):	149.02
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	33.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.50
Runoff Volume, [V] (cubic feet)	330209.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1668
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	330209.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1668
Total Recovered Volume, [V] (ft <sup>3</sup> ):	330209.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND18  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	1120.00
Equivalent Pond Width, [W] (ft):	115.00
Pond Bottom Elevation, [PB] (ft above datum):	165.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	154.40
Water Table Elevation, [WT] (ft above datum):	154.50
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	424644.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1575
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	405720.03

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0041
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	18923.97
Maximum Radius Of Influence, [R] (ft):	4.84
Maximum Driving Head, [Hmax] (ft):	10.647
Minimum Driving Head, [Hmin] (ft):	10.500

TOTAL

Total Recovery Time, [T] (days):	0.1616
Total Recovered Volume, [V] (ft <sup>3</sup> ):	424644.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND19  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 140.00  
Pond Bottom Elevation, [PB] (ft above datum): 178.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.20  
Water Table Elevation, [WT] (ft above datum): 165.30  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 20.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 10.00

Runoff Volume, [V] (cubic feet) 186265.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.3810  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 176021.97

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0093  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 10243.03  
Maximum Radius Of Influence, [R] (ft): 5.65  
Maximum Driving Head, [Hmax] (ft): 12.922  
Minimum Driving Head, [Hmin] (ft): 12.700

TOTAL

Total Recovery Time, [T] (days): 0.3903  
Total Recovered Volume, [V] (ft<sup>3</sup>): 186265.00

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And Robert D. Casper

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND20  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	350.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	191.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	187.00
Water Table Elevation, [WT] (ft above datum):	187.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	23.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	11.50
Runoff Volume, [V] (cubic feet)	143939.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1017
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	81899.88

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	5.5814
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	62039.13
Maximum Radius Of Influence, [R] (ft):	83.22
Maximum Driving Head, [Hmax] (ft):	4.786
Minimum Driving Head, [Hmin] (ft):	3.900

TOTAL

Total Recovery Time, [T] (days):	5.6832
Total Recovered Volume, [V] (ft <sup>3</sup> ):	143939.00



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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND21  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 370.00  
Equivalent Pond Width, [W] (ft): 250.00  
Pond Bottom Elevation, [PB] (ft above datum): 190.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 182.00  
Water Table Elevation, [WT] (ft above datum): 182.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 14.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 7.00

Runoff Volume, [V] (cubic feet) 470593.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.3386  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 219224.84

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 12.5759  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 251368.16  
Maximum Radius Of Influence, [R] (ft): 138.62  
Maximum Driving Head, [Hmax] (ft): 10.617  
Minimum Driving Head, [Hmin] (ft): 7.900

TOTAL

Total Recovery Time, [T] (days): 12.9145  
Total Recovered Volume, [V] (ft<sup>3</sup>): 470593.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND22  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	670.00
Equivalent Pond Width, [W] (ft):	110.00
Pond Bottom Elevation, [PB] (ft above datum):	169.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	165.00
Water Table Elevation, [WT] (ft above datum):	165.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	23.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	11.50
Runoff Volume, [V] (cubic feet)	213958.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1017
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	86228.87

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	9.9849
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	127729.13
Maximum Radius Of Influence, [R] (ft):	120.48
Maximum Driving Head, [Hmax] (ft):	5.633
Minimum Driving Head, [Hmin] (ft):	3.900

TOTAL

Total Recovery Time, [T] (days):	10.0867
Total Recovered Volume, [V] (ft <sup>3</sup> ):	213958.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND23  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 400.00  
Pond Bottom Elevation, [PB] (ft above datum): 130.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 122.00  
Water Table Elevation, [WT] (ft above datum): 122.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 11.50

Runoff Volume, [V] (cubic feet) 814515.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.2061  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 398160.09

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 12.3604  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 416354.91  
Maximum Radius Of Influence, [R] (ft): 175.09  
Maximum Driving Head, [Hmax] (ft): 10.378  
Minimum Driving Head, [Hmin] (ft): 7.900

TOTAL

Total Recovery Time, [T] (days): 12.5665  
Total Recovered Volume, [V] (ft<sup>3</sup>): 814515.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND24  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	530.00
Equivalent Pond Width, [W] (ft):	480.00
Pond Bottom Elevation, [PB] (ft above datum):	112.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	101.45
Water Table Elevation, [WT] (ft above datum):	101.55
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	31.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	15.50
Runoff Volume, [V] (cubic feet)	1284497.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.2023
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	797543.81

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	4.1882
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	486953.19
Maximum Radius Of Influence, [R] (ft):	134.92
Maximum Driving Head, [Hmax] (ft):	12.364
Minimum Driving Head, [Hmin] (ft):	10.450

TOTAL

Total Recovery Time, [T] (days):	4.3904
Total Recovered Volume, [V] (ft <sup>3</sup> ):	1284497.00

**GEOTECHNICAL  
INVESTIGATION OF  
LEGENDS SUDIVISION  
Clermont  
Lake County, Florida**



# Andreyev Engineering, Inc.

SANFORD OFFICE  
105 Coastline Road  
Sanford, Florida 32771  
407-330-7763  
Fax: 407-330-7765  
Email: ANDENGI@AOL.COM

▼ Groundwater ▼ Environmental ▼ Geotechnical ▼ Construction Materials Testing

July 22, 1998  
Project No: TPGT 98-061

**TO:** Lennar Homes  
c/o Farner Barley & Associates, Inc.  
350 North Sinclair  
Tavares, Florida 32778

**Attention:** Duane Booth, P.E.

**SUBJECT:** Geotechnical Investigation of Legends Subdivision, Stormwater Retention Systems,  
Clermont, Lake County, Florida

Dear Mr. Booth

As requested, Andreyev Engineering, Inc. (AEI) has completed a geotechnical investigation for the subject site. The following report presents the results of our field and laboratory investigation along with evaluation and recommendations for the proposed site.

## SITE LOCATION AND DESCRIPTION

The subject site property is located just south of Clermont on the west side of U.S. 27 across from the KingsRidge Subdivision. We understand that the property will be used for residential development. Approximately twenty (20) stormwater retention areas associated with the proposed development will be located as shown on the attached site plan labeled **Figure 1**.

## PURPOSE AND SCOPE OF SERVICES

The purpose of this study was to explore shallow subsurface conditions at the proposed retention areas to determine the suitability for stormwater retention. The field exploration consisted of drilling twenty-five (25) auger borings to depths of 10 to 20 feet within the proposed retention areas. In addition, twenty-one (21) field permeability tests and three (3) laboratory permeability tests were conducted at selected borings in order to measure the hydraulic conductivity of the soils.

Field permeability tests were conducted at selected borings within the proposed retention pond areas to measure the horizontal hydraulic conductivity of the soils. These tests were conducted by installing a screen PVC piezometer in the ground to varying depths between 10 and 20 feet below the ground surface, and conducting a constant head field permeability test, per designation E-19, Earth Manual, 1974. The results of these tests are shown adjacent to the sampled depth interval on Figures 2 & 3.

In order to measure the vertical hydraulic conductivity of the shallow soils within both proposed retention ponds, undisturbed tube sample were extracted from varying depths at borings AB-31, AB-32 and AB-34. The coefficient of permeability was measured in our laboratory using a falling head test. The results of these tests are shown adjacent to the sampled depths on Figure 3.

Samples were recovered from the borings and returned to AEI 's laboratory for visual classification and stratification. Soil strata were classified according to the Unified Soil Classification System. Approximate boring locations are shown on Figure 1 and results of the borings in profile form are presented on Figures 2 & 3. Also shown on Figures 2 & 3 next to the tested depths are the results of the permeability testing. On the profiles, horizontal lines designating the interface between differing materials represent approximate boundaries. The actual transition between layers is typically gradual.

#### **SUBSURFACE CONDITIONS**

Five (5) soil strata were identified in the borings. Strata 1 and 2 were the predominant surficial soils extending from the ground surface to the boring termination depths. Stratum 3, slightly clayey to clayey fine sand, was found at varying depths between 5 and 20 foot below ground surface. Stratum 4, slightly silty to silty fine sand, was also found at sporadic depths between 5 and 20 feet below ground surface. Stratum 5, fine sand with dry muck and organic material, was found in borings AB-32 and AB-33 from the ground surface to about 1 foot below ground surface.

Field permeability tests measured the shallow soil hydraulic conductivity at the proposed retention areas. In general, soil hydraulic conductivity measured between 15 and 50 feet per day in the strata 1 and 2 sandy soils, 1 to 4 feet per day in the slightly clayey to clayey soils, and 5 to 12 feet per day

in the slightly silty to silty soils. Results of these tests are shown next to the tested depths and borings on Figure 2 & 3.

The groundwater table was not encountered in any of the borings except AB-18, AB-19, and AB-28 where the ground water levels were encountered at depths of 10, 6, and 10 feet, respectively. However, these water table measurements are believed to be perched groundwater above the Stratum 3 soils, which resulted from the heavy rainfall at the time of measurement. The actual groundwater table at this site is estimated to be well below the termination depths of the borings.

For purposes of design and evaluation of retention area recovery, it can be assumed that the seasonal high groundwater table exists at more than 20 feet below the ground surface. However, at the locations where clayey soils of Stratum 3 are present, the groundwater table should be assumed to occur at about 1.0 foot above the top of Stratum 3.

#### **EVALUATION AND RECOMMENDATIONS**

Based on the results of borings, field permeability tests, and laboratory permeability tests, we conclude that the site is suitable for construction and long-term performance of dry stormwater retention systems. Adequate separation between the bottom of the proposed ponds and the groundwater table should not be a problem, except for possible groundwater conditions. The well-drained and, highly permeable nature of the surficial soils, and deep ground water table should be well suited for dry stormwater retention areas. However, temporary perching is expected to occur above the Stratum 3 clayey soils.

To mitigate potential negative impact of perched groundwater conditions, it is recommended that the Stratum 3 clayey soils be excavated from beneath the pond bottom to allow a hydraulic connection to deeper more permeable soils below. Provided that an effective hydraulic connection is made to the lower permeable soil, the pond will operate under true groundwater levels and not perched conditions.

For analysis and design purposes the following aquifer characteristics should be used. These aquifer characteristics were determined from the results of the field and laboratory investigations:



Boring	Bottom of Aquifer *(ft) Without Excavation of Stratum 3	Bottom of Aquifer*(ft) With Excavation of Stratum 3	Estimated Perched Wet Season GWT *(ft)	Estimated Normal Seasonal High GWT *(ft)	Kh** (ft/day)	Kv** (ft/day)
AB-10	15		20	20	-	
AB-11	15		20	20	43	
AB-12	14	20	13.5	20	-	
AB-13	10		20	20	33	
AB-14	7	15	6	20	50	
AB-15	15		15	20	31	
AB-16	15		15	20	20	
AB-17	11	20	10	20	-	
AB-18	11.5	15	10.5	20	32	
AB-19	10	15	9	20	19	
AB-20	13	13	12	20	15	
AB-21	8	N/A	7	20	-	
AB-22	6.5	N/A	5.5	20	-	
AB-23	20		20	20	28	
AB-24	10		10	20	42	
AB-25	15		15	20	40	
AB-26	16	20	15	20	44	
AB-27	20		20	20	26	
AB-28	12	15	11	20	24	
AB-29	8	20	7	20	14	
AB-30	8	20	7	20	7	
AB-30	8	20	7	20	20	
AB-31	6	15	5	20	26	
AB-31	6	15	5	20	4	
AB-31	6	15	5	20		12
AB-32	7	10	6	20	23	
AB-32	7	10	6	20		15
AB-33	13	15	12	20	-	
AB-34	7	15	6	20	5	
AB-34	7	15	6	20		31

\*-depth below existing ground surface

\*\* - See depth of tests and test intervals on soil profiles, Figures 2 & 3.

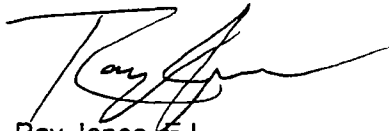
Specific Recommendations for the ponds corresponding to borings AB-14, AB-31, and AB-32 are as follows. Clayey material in the vicinity of AB-31 should be excavated from 6 to 12 feet below ground surface and replaced with clean fine sand. In the vicinity of AB-14, the clayey material should be excavated from 7 to 10 feet below ground surface and replaced with clean fine sand. Also, in order to provide effective infiltration in the area of AB-32, the clayey material and muck material should be over-excavated from ground surface to 6 foot below ground surface.

CLOSURE

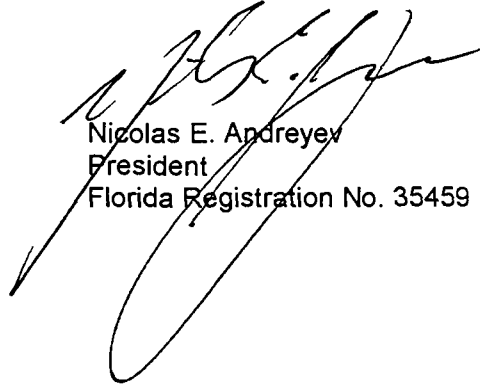
AEI appreciates the opportunity to participate in this project, and we trust that the information herein is sufficient for your immediate needs. If you have any questions or comments concerning the contents of this report, please do not hesitate to contact the undersigned.

Sincerely,

ANDREYEV ENGINEERING, INC.

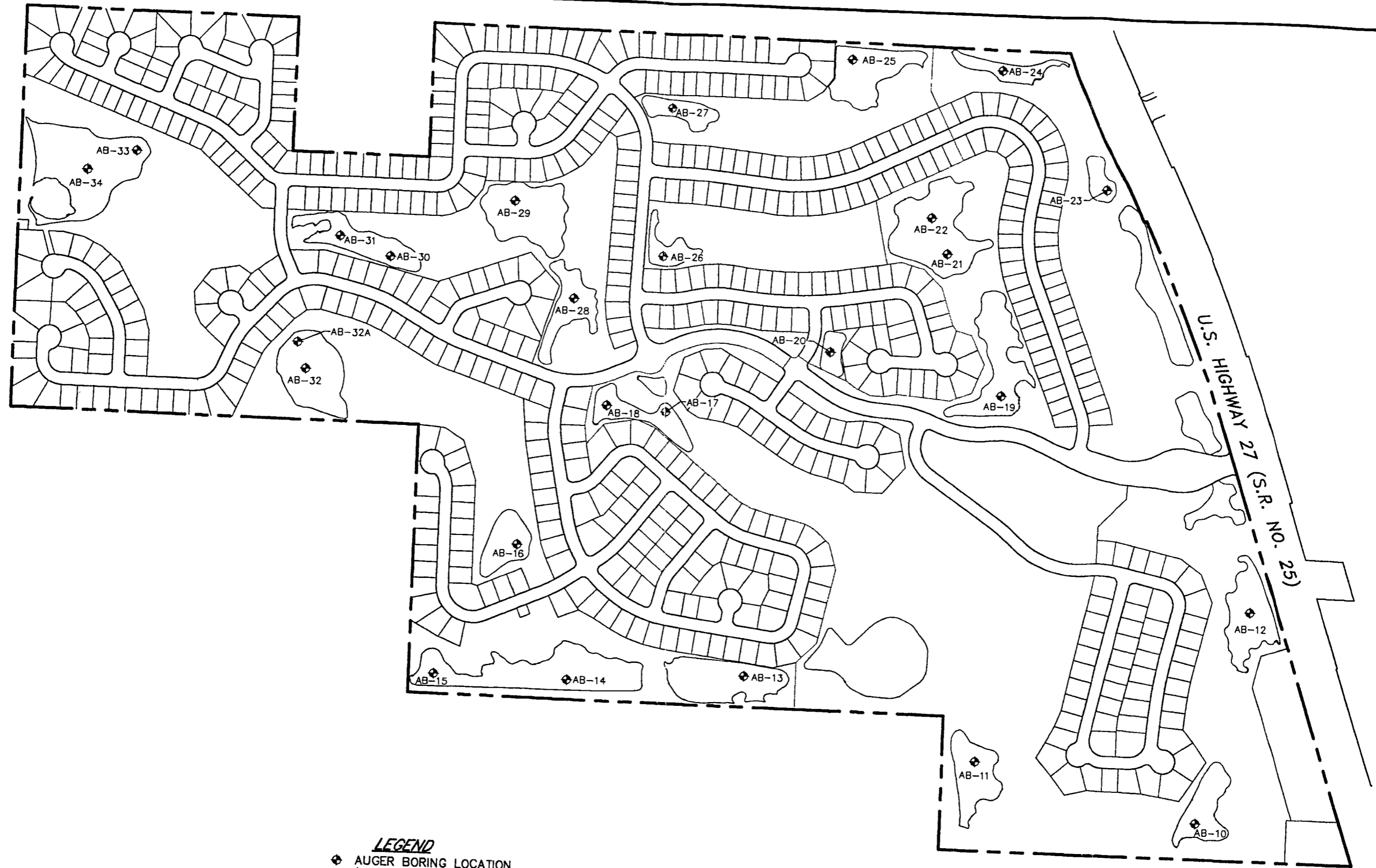


Ray Jones, E.I.  
Project Engineer  
Tavares Office



Nicolas E. Andreyev  
President  
Florida Registration No. 35459

## FIGURES



**LEGEND**  
◆ AUGER BORING LOCATION



**Andreyev  
Engineering,  
Inc.**

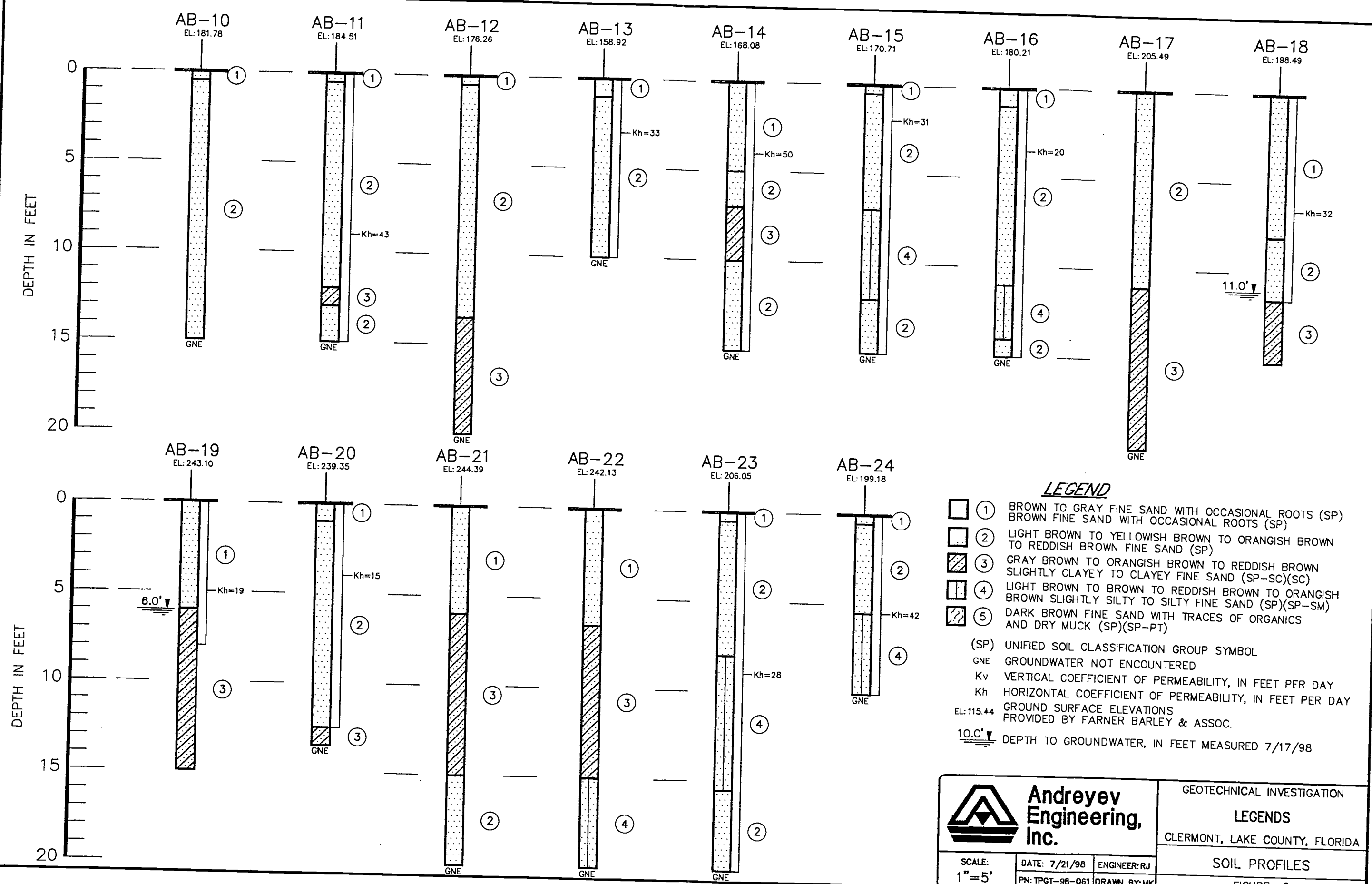
GEOTECHNICAL INVESTIGATION  
**LEGENDS**  
CLERMONT, LAKE COUNTY, FLORIDA

SCALE:  
1" = 500'

DATE: 7/22/98  
PN: TPCT-98-061

ENGINEER: RJ  
DRAWN BY: MK

SITE PLAN  
FIGURE 1

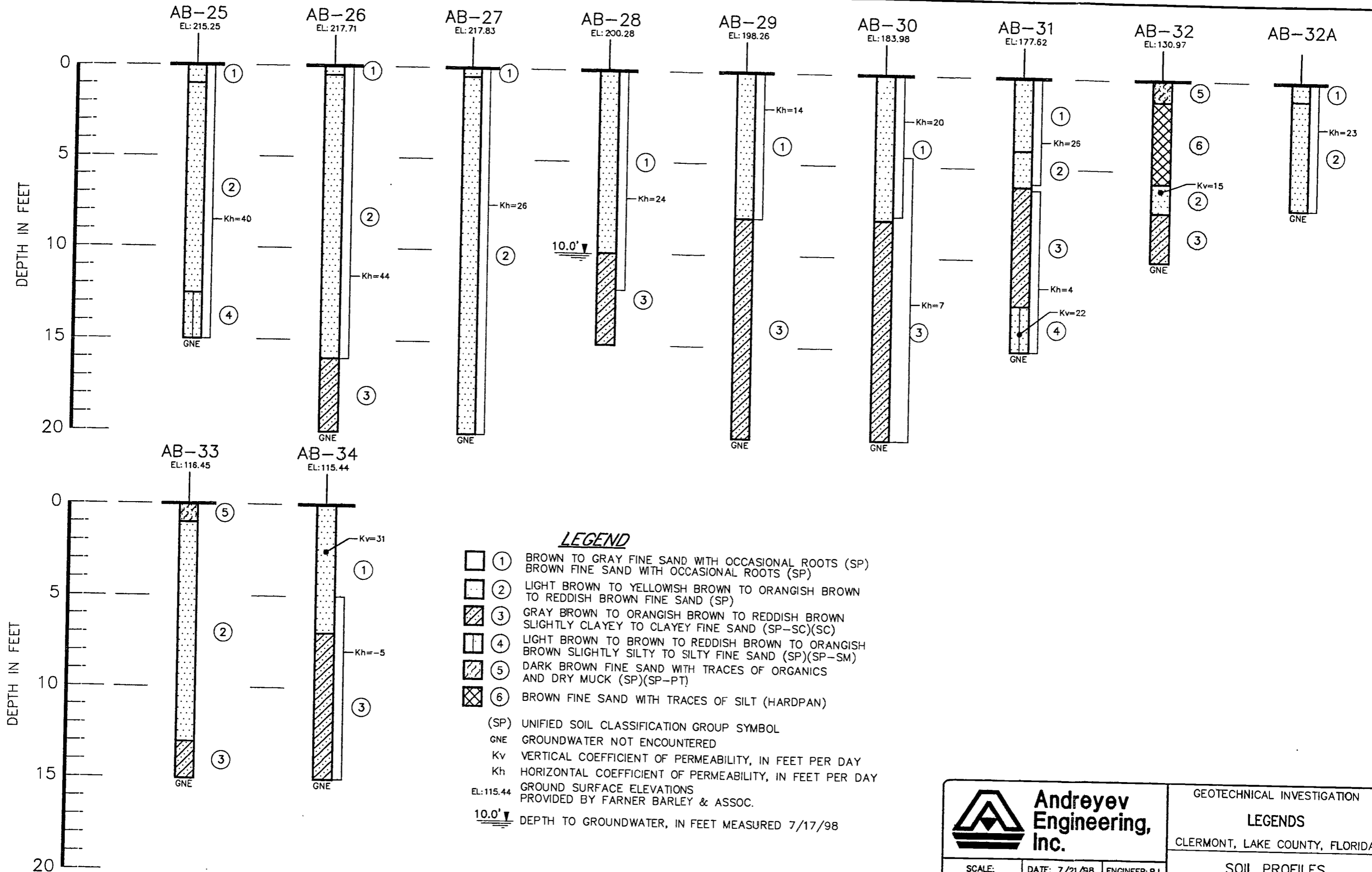


**LEGEND**

- ① BROWN TO GRAY FINE SAND WITH OCCASIONAL ROOTS (SP)  
BROWN FINE SAND WITH OCCASIONAL ROOTS (SP)
- ② LIGHT BROWN TO YELLOWISH BROWN TO ORANGISH BROWN TO REDDISH BROWN FINE SAND (SP)
- ③ GRAY BROWN TO ORANGISH BROWN TO REDDISH BROWN SLIGHTLY CLAYEY TO CLAYEY FINE SAND (SP-SC)(SC)
- ④ LIGHT BROWN TO BROWN TO REDDISH BROWN TO ORANGISH BROWN SLIGHTLY SILTY TO SILTY FINE SAND (SP)(SP-SM)
- ⑤ DARK BROWN FINE SAND WITH TRACES OF ORGANICS AND DRY MUCK (SP)(SP-PT)

(SP) UNIFIED SOIL CLASSIFICATION GROUP SYMBOL  
 GNE GROUNDWATER NOT ENCOUNTERED  
 Kv VERTICAL COEFFICIENT OF PERMEABILITY, IN FEET PER DAY  
 Kh HORIZONTAL COEFFICIENT OF PERMEABILITY, IN FEET PER DAY  
 EL: 115.44 GROUND SURFACE ELEVATIONS PROVIDED BY FARNER BARLEY & ASSOC.  
 10.0' ▾ DEPTH TO GROUNDWATER, IN FEET MEASURED 7/17/98

		GEOTECHNICAL INVESTIGATION <b>LEGENDS</b> CLERMONT, LAKE COUNTY, FLORIDA	
		<b>SOIL PROFILES</b> FIGURE 2	
SCALE: 1"=5'	DATE: 7/21/98 PN: TPGT-98-061	ENGINEER: RJ DRAWN BY: MK	



**LEGEND**

- ① BROWN TO GRAY FINE SAND WITH OCCASIONAL ROOTS (SP)  
BROWN FINE SAND WITH OCCASIONAL ROOTS (SP)
  - ② LIGHT BROWN TO YELLOWISH BROWN TO ORANGISH BROWN  
TO REDDISH BROWN FINE SAND (SP)
  - ③ GRAY BROWN TO ORANGISH BROWN TO REDDISH BROWN  
SLIGHTLY CLAYEY TO CLAYEY FINE SAND (SP-SC)(SC)
  - ④ LIGHT BROWN TO BROWN TO REDDISH BROWN TO ORANGISH  
BROWN SLIGHTLY SILTY TO SILTY FINE SAND (SP)(SP-SM)
  - ⑤ DARK BROWN FINE SAND WITH TRACES OF ORGANICS  
AND DRY MUCK (SP)(SP-PT)
  - ⑥ BROWN FINE SAND WITH TRACES OF SILT (HARDPAN)
- (SP) UNIFIED SOIL CLASSIFICATION GROUP SYMBOL  
 GNE GROUNDWATER NOT ENCOUNTERED  
 Kv VERTICAL COEFFICIENT OF PERMEABILITY, IN FEET PER DAY  
 Kh HORIZONTAL COEFFICIENT OF PERMEABILITY, IN FEET PER DAY  
 EL: 115.44 GROUND SURFACE ELEVATIONS  
 PROVIDED BY FARNER BARLEY & ASSOC.  
 10.0' ▼ DEPTH TO GROUNDWATER, IN FEET MEASURED 7/17/98

		GEOTECHNICAL INVESTIGATION <b>LEGENDS</b> CLERMONT, LAKE COUNTY, FLORIDA	
		<b>SOIL PROFILES</b> FIGURE 3	
SCALE: 1"=5'	DATE: 7/21/98 PN: TPGT-98-061	ENGINEER: RJ DRAWN BY: MK	

Geotechnical Investigation  
of Potential Karst Activity  
**LAKE LOUISA CLUB**  
Lake County, Florida



**Andreyev  
Engineering,  
Inc.**

▼ 4500 Orange Blvd.  
Sanford, Florida 32771  
TEL (407) 330-7763  
FAX (407) 330-7765

November 22, 1996  
Project No. PGT-96-165

**TO:** Farner Barley & Associates. Inc.  
350 North Sinclair Avenue  
Tavares, FL 32778

**Attention:** Mr. Robert E. Farner, P.E.

**SUBJECT:** Geotechnical Investigation of Potential Karst Activity, Lake Louisa Club,  
Lake County, Florida

---

Dear Mr. Farner:

As requested, Andreyev Engineering, Inc. (AEI) has completed a geotechnical investigation of potential karst activity at the subject site. Work was performed in general accordance with AEI proposal No. P-96-116 dated October 15, 1996.

The attached report presents the findings, evaluations and recommendations. AEI appreciates the opportunity to participate in this project and trusts that the information contained herein is sufficient for your immediate needs. If you have any questions or comments, please contact the undersigned.

Sincerely,

ANDREYEV ENGINEERING, INC.

Scott Cavin, P.E.  
Senior Project Engineer  
Florida Registration No. 48125

Nicolas E. Andreyev, P.E.  
President  
Florida Registration No. 35459



## Site and Project Description

The proposed Lake Louisa Club development is located on the west side of U.S. Highway 27 approximately four (4) miles southeast of Clermont, Florida. The property encompasses about 400 acres of land in portions of Sections 4, 5, 8 and 9 of Township 23 South, Range 26 East, Lake County, Florida. The subject site is approximately 1500 feet north of Lake Louisa. Refer to **Figure 1** for a Vicinity Map. The site topography consists of hills and depressions with an estimated elevation change on the order of 150 feet. At the time of AEI's field explorations, the property was undeveloped except for a few abandoned structures. Most of the site had been cleared except for some of the depressions which contained mature trees. It appears that the subject site was formerly a citrus grove.

It is understood that the proposed development will include single family residences, paved streets, a golf course, drainage retention areas, and lake/conservation areas. The residential lot sizes will range from approximately 0.19 to 0.24 acre.

## Purpose and Scope

The purpose of this study was to obtain information on the general subsurface conditions within existing depressions at the site, evaluate the stability of the depressions, and evaluate the potential for sinkhole activity. To accomplish this purpose, the following tasks were performed:

- Review available published data regarding the subsurface and surface conditions in the vicinity of the subject site.
- Locate and identify the boring locations within the depressions.
- Drill six (6) Standard Penetration Test (SPT) borings to a depth of 150 feet below existing ground surface.
- Visually classify and stratify samples recovered from the borings and perform index property tests on selected samples.
- Prepare a report which summarizes the work performed, the field and laboratory data generated, and engineering analyses and recommendations.

## Review of Available U.S. Geological Survey Map

The "Clermont East, Florida" topographic map published by the U.S. Geological Survey (U.S.G.S.) dated 1962 (photorevised 1986) was reviewed. Refer to **Figure 1** for a copy of a portion of this map showing the subject site location. The topography of the site is characterized by hills and depressions. The ground surface elevation ranges from approximately +100 feet, NGVD near the northwest corner of the site to about +250 feet, NGVD in the east central portion of the property.

There are two (2) relatively large circular depressions located in the western portion of the site. The largest is on the western property boundary. This largest feature is approximately 1500 to 2000 feet in diameter by 50 to 75 feet deep. The second large depression is located about 2000 feet southeast of the largest depression. The smaller feature is about 800 to 1000 feet in diameter by 40 feet deep. Three (3) other depressions and topographic low areas are identified on the map within the site boundary. These areas are located along U.S. Highway 27 on the eastern site boundary in the south central portion of the site near the south property boundary, and on the northeastern portion of this site at the northern property boundary.

The topography surrounding the site is similar to the site, consisting of hills and depressions. Swamp symbols are shown in some of the low areas on adjacent properties. The water elevations of Lake Louisa to the south and Lake Felter to the north of the subject site are shown at +94 and +85 feet, NGVD, respectively.

### **S.C.S. Soil Survey**

The "Soil Survey Report, Maps and Interpretations, Lake County Area, Florida" published by the U.S. Department of Agriculture Soil Conservation Service (S.C.S.) was reviewed. Within the subject property boundaries, the shallow soil types consist of Candler and Lake sands. These soils are deep, excessively well drained soils with a seasonal high groundwater table greater than six (6) feet below ground surface.

### **Potentiometric Surface Map**

The map "Potentiometric Surface of the Upper Floridan Aquifer in the St. John's River Water Management District and Vicinity, Florida, September 1995" published by the U.S.G.S. was reviewed. The elevation of the potentiometric surface in the vicinity of the subject site is approximately +85 feet, NGVD. Groundwater flow in the Upper Floridan Aquifer is to the northeast.

### **Area Geology**

The geology of the Central Florida areas is characterized by sedimentary strata formed during three distinct geologic periods. The surficial stratum is composed of undifferentiated Holocene/Pleistocene/Pliocene age sands, containing varying amounts of silt and clay, which extend typically to depths on the order of 40 to 60 feet below ground surface. This upper, mostly sandy zone contains the surficial (water table) aquifer. A Miocene age deposit, the Hawthorne Formation, frequently underlies the surficial sand and is typically composed of clay, clayey sand and sandy limestone containing appreciable amounts of phosphate. This relatively impermeable stratum extends to typical depths of 125 to 150 feet beneath ground surface and serves as the confining layer for the underlying Floridan aquifer. The Floridan aquifer, composed of Eocene age Ocala, Avon Park and Lake City Limestones, is highly productive and supplies most of the drinking water for Central Florida. The extremely high productivity of this aquifer is directly related to its many cavities and interconnected channels. These cavities and channels were formed by dissolution of the limestone caused by the movement of slightly acidic water through the rock.

The geology of the area, as described above, is conducive to the development of sinkholes. The solution features within the limestone can collapse or can allow the downward movement of overlying soils, known as ravelling, to produce depressions at the surface which are typically circular in shape (sinkholes). Sinkholes can occur nearly anywhere in Central Florida, but are more likely to occur in areas characterized by thin confining beds, large differences between the water table elevation and the Floridan aquifer potentiometric level and the presence of limestone in relatively close proximity to the ground surface.

### **Previous Geotechnical Reports**

The following reports were supplied to AEI for review:

- "Report of Preliminary Subsurface Exploration, Sinkhole Risk Analysis and Effluent Disposal Evaluation, West Hills, Lake County, Florida" dated August 14, 1990 by Westinghouse Environmental and Geotechnical Services, Inc.

- "Report of Subsurface Exploration and Geotechnical Engineering Evaluation for Existing Depression areas, Kings Point Subdivision (Formerly Clermont Hills), Lake County, Florida" dated February 14, 1995 by L.J. Nodarse & Associates, Inc.

The Westinghouse study was located in Sections 3, 4, 5 and 9 and the L.J. Nodarse study was located in Section 4 of Township 23 South, Range 26 East. These study areas are within or adjacent to the sections studied for the proposed Lake Louisa Club development. Both studies found relatively thick deposits of sand grading downward into silt and clayey sand at depths between 75 and 100 feet below existing ground surface. Limestone was found in only one (1) of ten (10) SPT borings performed for both studies. The limestone was encountered at approximately elevation +10 feet, NGVD. Both studies concluded that existing subsurface conditions are stable and that the risk of future sinkhole development is moderate to low.

### **Field Exploration/Laboratory Testing**

The field exploration for the Lake Louisa Club development was performed between October 22nd and November 4, 1996. Six (6) Standard Penetration Test (SPT) borings were drilled in the existing depressions and topographic low areas at the subject site. The borings were advanced to a depth of 150 feet below existing ground surface. SPT N-values were recorded continuously in the upper ten (10) feet of each boring and at five (5) foot intervals thereafter. The borings were completed using the mud rotary method and were grout sealed upon completion. Samples were recovered from each boring and returned to AEI's laboratory for classification and stratification. Index property tests, consisting of moisture content and percent passing the No. 200 sieve were performed on selected samples. Approximate locations of the borings are shown on **Figure 2** and results of the borings in profile form are presented on **Figure 3**. SPT N-values and laboratory test results are shown at the approximate depths adjacent to the profiles on **Figure 3**. On the profiles, horizontal lines designating the interface between differing intervals represent approximate boundaries. The transition between layers is typically gradual.

### **Subsurface Conditions**

In general, the borings encountered fine sand, slightly silty fine sand, and silty fine sand (Strata 1, 2 and 3) to the termination depths. Exceptions were noted in borings TB-1, TB-2 and TB-3 where relatively minor amounts of slightly clayey to clayey fine sand (Stratum 4) were found at various depths. Refer to the boring profiles on **Figure 3** for a more complete description of the subsoils found.

SPT N-values were generally less than ten (10) in the upper ten (10) feet of each boring. Below ten (10) feet, the N-values were generally greater than 15 and in most cases greater than 20. An exception was noted between the depths of 140 and 150 feet in boring TB-4 where N-values of four (4) and five (5) were recorded. Drilling fluid circulation losses were not noted during drilling. However, a greater than normal use of fluid was noted in boring TB-2 between the depths of 100 and 150 feet.

### **Evaluation**

As discussed above, the geology of the area where the subject site is located is conducive to the development of sinkholes. Solution features within the limestone that underlies the area can collapse or can allow the downward movement of overlying soils to produce depressions at the surface which are typically circular in shape. The depressions on the subject site and on adjacent properties are believed to have formed by these processes. The depressional features are relatively old as evidenced by the presence of mature trees (where clearing has not occurred) and

the presence of stable slopes. The stability of the depressions and the potential for future suitable activity can be evaluated by analysis of the SPT boring results and the geologic and hydrogeologic conditions in the area.

Sinkholes in the Central Florida area normally develop by subsidence or collapse of unconsolidated soils that overlie the limestone into openings and very loose zones in the limestone. Conditions that favor sinkhole development include the following:

- The presence of openings and very loose (ravelled) zones in the limestone.
- Easily erodible soils above the limestone.
- The presence of a significant hydraulic head between a shallow and a deep water table which promotes a downward erosion process.

Limestone was not found in the borings performed for this study to a depth of 150 feet and limestone was found in only one (1) boring performed at the adjacent properties. However, it is well documented that limestone underlies the area and that the surface of the limestone has been subjected to chemical erosion, creating openings and very loose zones. The sandy soils that were found in the borings are easily erodible if present in a loose condition. However, the relatively high SPT N-values recorded in the borings indicate that the sands are not loose, except in the near surface deposits, which is a typical condition in most of Central Florida. Lastly, the presence of low permeability soils (sandy clay and clay) found near the bottom of some of the borings, indicate a presence of a semi-eroded Hawthorn Formation above the limestone, that will provide confinement between the water table aquifer and the underlying limestone aquifer.

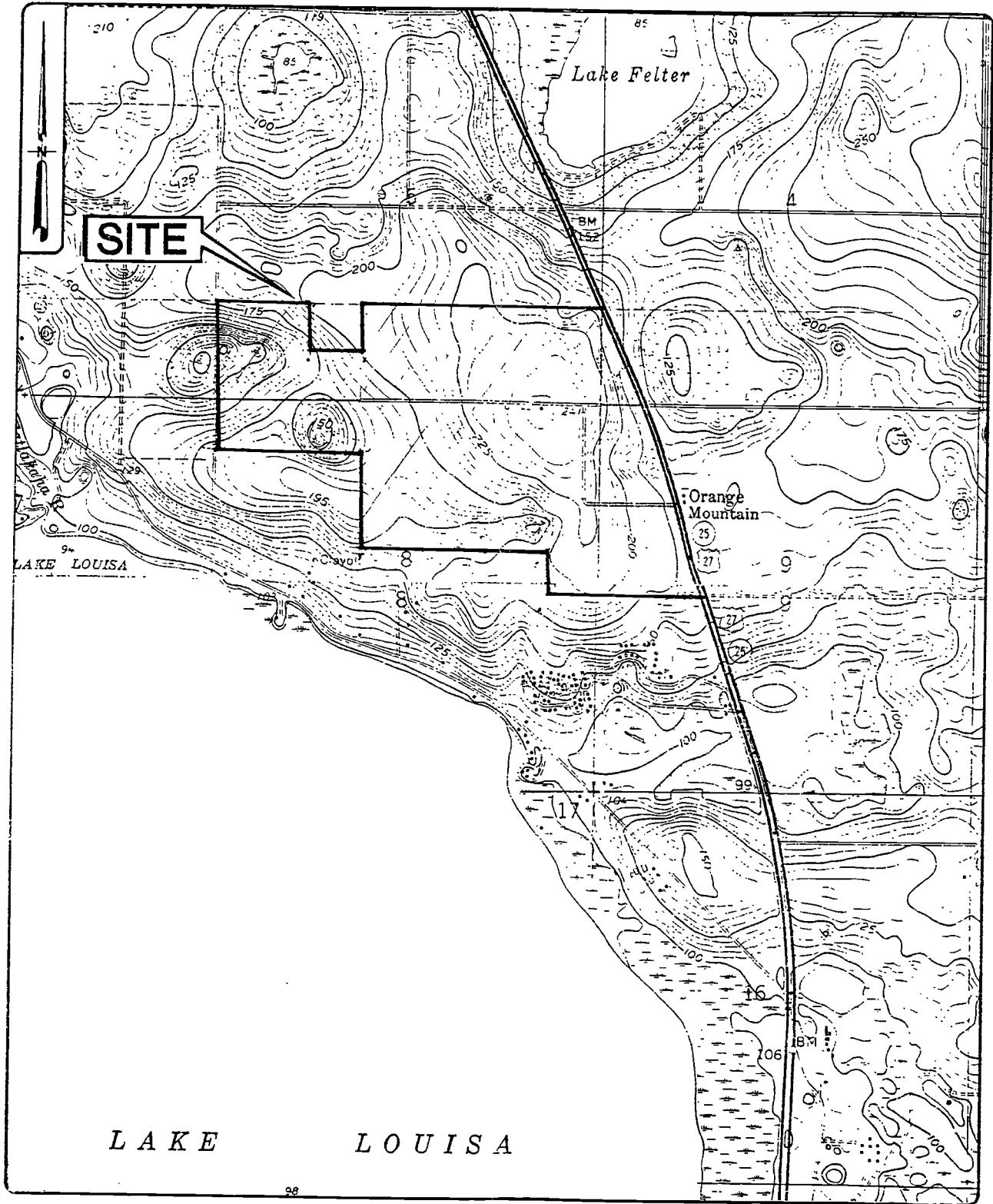
The conditions prior to depression development more than likely included loose sands and thin or leaky Hawthorn deposits. The present conditions at the boring locations indicate relatively dense soils through out the soil profile. The potential for future sinkhole development at the subject site in its present conditions is low relative the other sites in Central Florida. However, alteration of the site can increase the potential for further subsidence. To minimize the potential for future subsidence the development shall implement design and construction techniques to minimize increasing of hydraulic heads and overburdened loads in the depressional areas.

### **Recommendations**

Induced sinkholes, or those caused by man's activities, result from ponding of water, groundwater level declines caused by pumping from the limestone, and significant removal of overburden above the limestone. At the subject site, it is recommended that structures be located at least 200 feet from the edge of proposed surface water bodies and areas where surface water accumulates, such as lakes, drainage retention areas and depressions. In addition, on-site wells should be installed with cased depths of a minimum of 50 feet into the limestone. Due to the thickness of soils over the limestone at the site, significant removal of overburden is not anticipated.

Futher site specific investigations and construction recommendations should be made for all depressional areas during the final design and construction activity on this project.

**FIGURES**



REFERENCE:  
 U.S.G.S. CLERMONT EAST, FLA.  
 QUADRANGLE MAP  
 DATED 1962  
 PHOTOREVISED 1980  
 SECTION 4  
 TOWNSHIP 23 SOUTH  
 RANGE 26 EAST



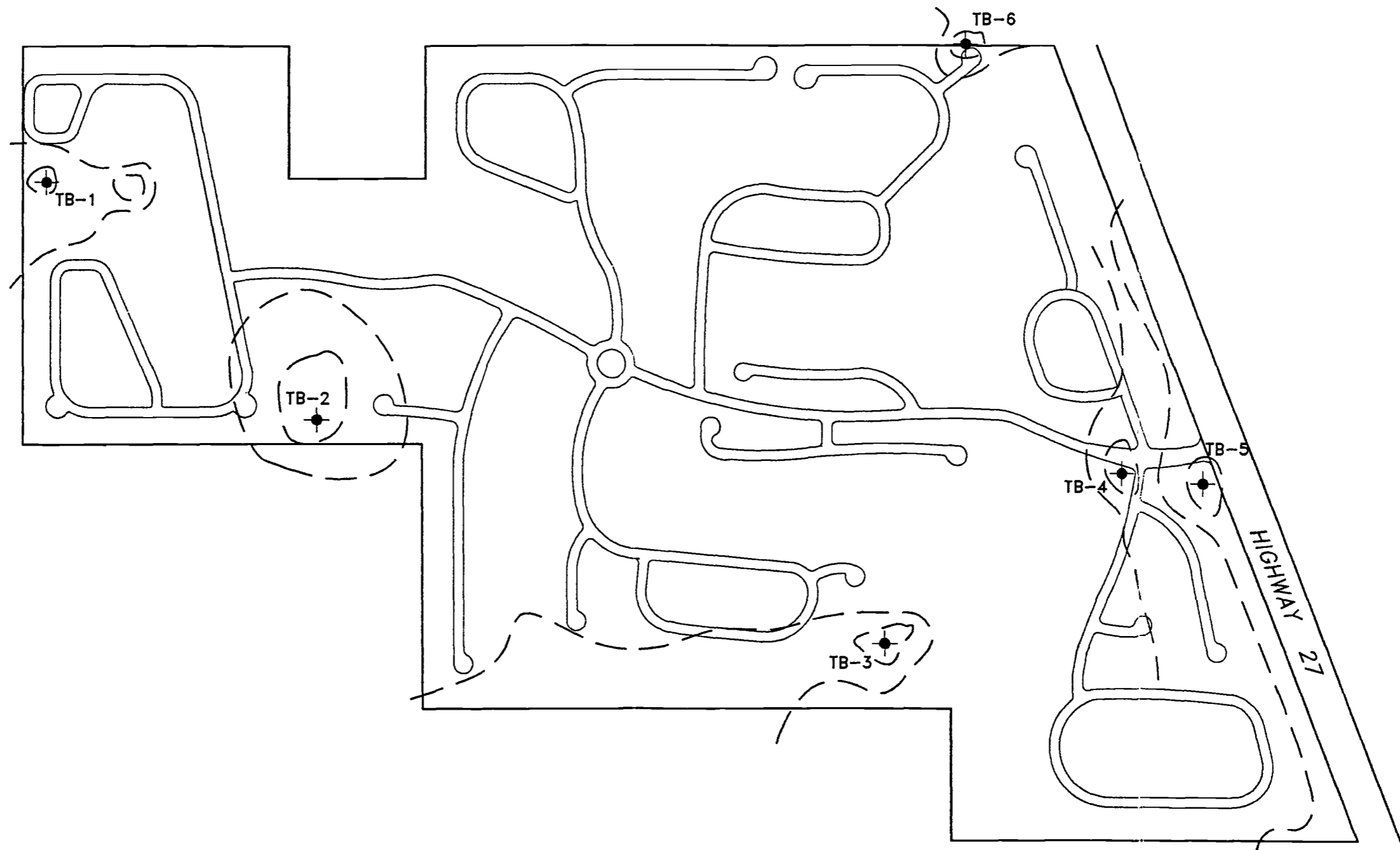
**Andreyev  
 Engineering,  
 Inc.**

GEOTECHNICAL INVESTIGATION  
 LAKE LOUISA CLUB  
 LAKE COUNTY, FLORIDA

DATE: 11-15-96	SCALE: 1"=2000'
ENGINEER: SC	PN: PGT-96-165


VICINITY MAP

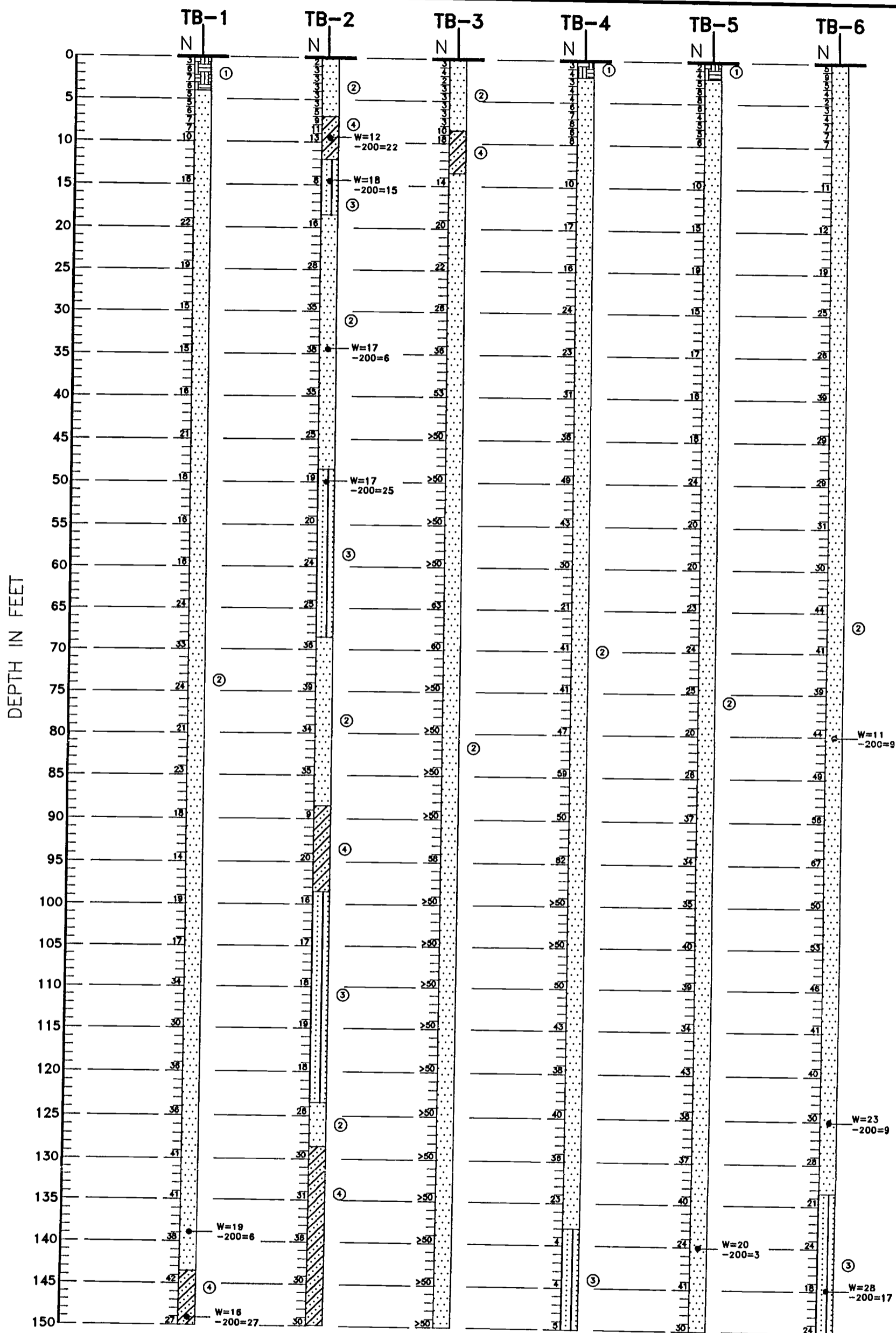
FIGURE 1



**LEGEND**


 APPROXIMATE LOCATION  
 OF SPT BORING


 <b>Andreyev Engineering, Inc.</b>	GEOTECHNICAL INVESTIGATION <b>LAKE LOUISA CLUB</b> LAKE COUNTY, FLORIDA	
	DATE: 11/13/96 ENGINEER: SC	SCALE: 1"=600' PN: PGT-96-165



**LEGEND**

- ① GRAYISH BROWN FINE SAND WITH SMALL ROOTS (TOPSOIL) (SP)
  - ② BROWN TO LIGHT BROWN TO ORANGISH BROWN SLIGHTLY SILTY FINE SAND (SP) (SP/SM)
  - ③ LIGHT GRAY TO LIGHT BROWN TO ORANGISH BROWN SLIGHTLY SILTY TO SILTY FINE SAND (SP/SM) (SM)
  - ④ LIGHT BROWN TO ORANGISH BROWN SLIGHTLY CLAYEY TO CLAYEY FINE SAND (SP/SC) (SC)
- (SP) UNIFIED SOIL CLASSIFICATION GROUP SYMBOL  
W NATURAL MOISTURE CONTENT IN PERCENT  
-200 PERCENT OF FINES PASSING THE U.S. No. 200 SIEVE  
N STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT

NOTE: GREATER THAN NOMINAL USE OF DRILLING FLUID NOTED IN BORING TB-2 FROM 100 TO 150 FEET.

 <p><b>Andreyev Engineering, Inc.</b></p>	GEOTECHNICAL INVESTIGATION <b>LAKE LOUISA CLUB</b> LAKE COUNTY, FLORIDA	
	<b>SOIL PROFILES</b> FIGURE 3	
DATE: 11-15-96 ENGINEER: SC	SCALE: 1"=12' PN: PGT-96-165	



Geotechnical Engineering Study,  
Proposed Stormwater  
Management Area  
**PHASE I**  
**LAKE LOUISA CLUB**  
Lake County, Florida



**Andreyev  
Engineering,  
Inc.**

▼ 4500 Orange Blvd.  
Sanford, Florida 32771  
TEL (407) 330-7763  
FAX (407) 330-7765

April 14, 1997  
Project No: PGT-96-165

**TO:** Lennar Homes  
7600 Nob Hill Road  
Tamarac, Florida 33321

**Attention:** Mr. Robert Ahrens

**SUBJECT:** Geotechnical Engineering Study of Proposed Stormwater Management Areas,  
Phase I, Lake Louisa Club, Lake County, Florida

---

Dear Mr. Ahrens:

As requested, Andreyev Engineering, Inc. (AEI) has completed a geotechnical engineering study for the subject project. The work was performed in general accordance with AEI Proposal No. DJR-97-006, dated April 3, 1997 with written authorization to proceed received on April 8, 1997.

The attached report presents the findings of the study and engineering analyses and recommendations to guide design and construction of the stormwater management areas. AEI appreciates the opportunity to participate in this project and trusts that the information herein is sufficient for your immediate needs. If you have any questions or comments concerning the contents of this report, or if we may be of further service, please do not hesitate to contact the undersigned.

Sincerely,

**ANDREYEV ENGINEERING, INC.**

David J. Rathbun, P.E.  
Senior Project Manager  
Florida Registration No. 40494

Nicolas E. Andreyev, P.E.  
President  
Florida Registration No. 35459

xc: Farner, Barley and Associates, Inc.

## 1.0 SITE AND PROJECT DESCRIPTION

The proposed Lake Louisa Club development is located on the west side of U.S. Highway 27 approximately four (4) miles southeast of Clermont, Florida. The property encompasses about 400 acres of land in portions of Sections 4, 5, 8 and 9 of Township 23 South, Range 26 East, Lake County, Florida. The subject site is approximately 1,500 feet north of Lake Louisa. Refer to **Figure 1** for a Vicinity Map. The site topography consists of hills and depressions with an estimated elevation change on the order of 150 feet. At the time of AEI's field exploration, the property was undeveloped except for a few abandoned structures. Most of the site had been cleared except for some of the depressions which contained mature trees. It appears that the subject site was formerly a citrus grove.

It is understood that the proposed development will include single family residences, paved streets, a golf course, drainage retention areas (DRA) and lake/conservation areas. The residential lot sizes will range from approximately 0.19 to 0.24 acre. Phase I consists of the eastern approximately 100 acres of the site. Ten (10) DRA's are planned in Phase I. The proposed DRA locations are shown on **Figure 2**. Four (4) of the DRA's will be adjacent to the U.S. 27 right-of-way. Final grades have not been determined but it appears that berms will be required between the DRA's and U.S. 27. The DRA's are expected to be on the order of 10 feet deep. Dry ponds are planned except for the DRA between golf holes 1 and 10 which will be lined to create a lake. Boring AB-10 was drilled near the edge of the proposed DRA above the top of the proposed liner. Due to the rolling terrain at the site, cut and fill is planned in roadway and lot areas. A proposed deep cut on the order of 10 feet is planned west of golf hole 18. Boring AB-3 was drilled in this area to assess subsurface conditions up to and below the cut elevation.

## 2.0 PURPOSE AND SCOPE OF SERVICES

The purpose of the study was to explore subsurface conditions at proposed DRA sites and in the proposed roadway cut area and provide the following:

- Soil and groundwater conditions encountered.
- Normal seasonal high groundwater level estimates.
- Permeability test results.
- Slope stability analyses for the berms DRA's.
- Recommendations for berm seepage control adjacent to U.S. Highway 27.
- Recommendations for the roadway cut area, including suitability of soils for use as fill and subgrade.

The field work was performed on April 9 and 10, 1997 and consisted of 10 auger borings to a depth of 25 feet below existing ground surface. Nine (9) of the borings were drilled at proposed DRA locations and 1 boring (AB-3) was drilled in the roadway cut area. In addition, 4 Standard Penetration Test (SPT) borings were previously drilled in or near the DRA sites by AEI. The scope of services for the subject study also included a field permeability test in each of the 10 DRA locations.

Samples were recovered from each boring and returned to AEI's laboratory for visual classification. Moisture content and No. 200 sieve tests were performed on selected samples. Approximate boring locations are shown on **Figure 2** and results of the borings in profile form are presented on **Figure 3**. The upper 25 feet of the previously performed SPT borings (TB-3 through TB-6) are also

shown on Figure 3. Results of the field permeability and laboratory tests are shown adjacent to the profiles. On the profiles, horizontal lines designating the interface between differing materials represent approximate boundaries. The transition between layers is typically gradual.

### 3.0 FINDINGS

#### 3.1 Subsurface Conditions

Fine sand to fine sand with silt (Stratum 1) was the predominant soil type found in the borings. Stratum 1 extended from the ground surface to the termination depth (25 feet) in borings AB-1, AB-3, AB-4, AB-7, AB-10, and TB-4 through TB-6. In borings AB-5, AB-6, and AB-8, Stratum 1 was underlain by fine to medium sand (Stratum 3) at depths ranging from about 18 ½ to 22 feet. In boring AB-9, Stratum 1 extended to a depth of approximately 9 feet where it was underlain by clayey fine sand (Stratum 4) and sandy clay (Stratum 5). Strata 4 and 5 extended to a depth of 22 feet in boring AB-9 where Stratum 1 was encountered to the boring termination depth. The groundwater table was not found in the borings.

The previously performed SPT borings were drilled to a depth of 150 feet below existing ground surface. Below the 25 foot depth shown on Figure 3, the SPT borings encountered fine sand to sand with silt (Stratum 1) for their entire depth.

#### 3.2 S.C.S. Soil Survey

The "Soil Survey Report, Maps and Interpretations, Lake County Area, Florida" published by the U.S. Department of Agriculture Soil Conservation Service (S.C.S.) was reviewed. The shallow soil types within the subject property boundaries consist of Candler and Lake sands. These soils are deep, excessively well drained soils with a seasonal high groundwater table greater than six (6) feet below ground surface.

#### 3.3 Permeability Test Results

The field permeability tests were conducted in temporary PVC slotted casings installed in the boreholes. The slotted PVC casings were installed to create open-hole permeability method. The tests were performed by applying a continuous flow of water to the open-holes to maintain a constant water level. The volume of water used was measured and the permeability was calculated per procedures recommended by the U.S. Bureau of Reclamation (Earth Manual, E-19). Results are as follows:

<u>Location</u>	<u>Tested Depth Interval Below Existing Ground Surface (feet)</u>	<u>Coefficient of Horizontal Permeability (feet per day)</u>
AB-1	5 ½ - 12	28
AB-2	5 ½ - 11 ½	27
AB-4	7 - 12	23
AB-5	7 ½ - 11 ½	29
AB-6	4 - 12	26
AB-7	7 - 12	38
AB-8	4 - 12	25
AB-9	5 - 10	81
AB-10	7 - 12	25
TB-5	7 - 12	19

## **4.0 EVALUATION AND RECOMMENDATIONS**

### **4.1 Drainage Retention Area Design Parameters**

The soils found in each DRA boring except AB-9 and TB-3 consisted of the Stratum 1, 2 and 3 sands. These sands are moderately to highly permeable and will be suitable for exfiltration of stormwater. The Strata 4 and 5 soils found in borings AB-9 and TB-3 have a relatively high fines content and therefore will have a very low permeability. Strata 4 and 5 should be considered as confining layers for purposes of infiltration analysis.

The normal seasonal high groundwater table is estimated to be below the depth of the borings (more than 25 feet below ground surface). However, water will temporarily perch on the Strata 4 and 5 soils after periods of heavy or prolonged rainfall.

### **4.2 Slope Stability**

Pond slopes of 3:1 (H:V) or flatter are expected to be stable. The stability of a 3:1 slope 12 feet high was analyzed using the computer program PCSTABL. The analysis was performed assuming that the pond was full of water and the soils below the water level were saturated. The resulting factor of safety was 1.9. Results are included in **Appendix A**. After final grades have been determined, additional slope stability analyses should be performed based on the actual pond geometry if higher or steeper slopes are planned.

### **4.3 Berm Seepage Control**

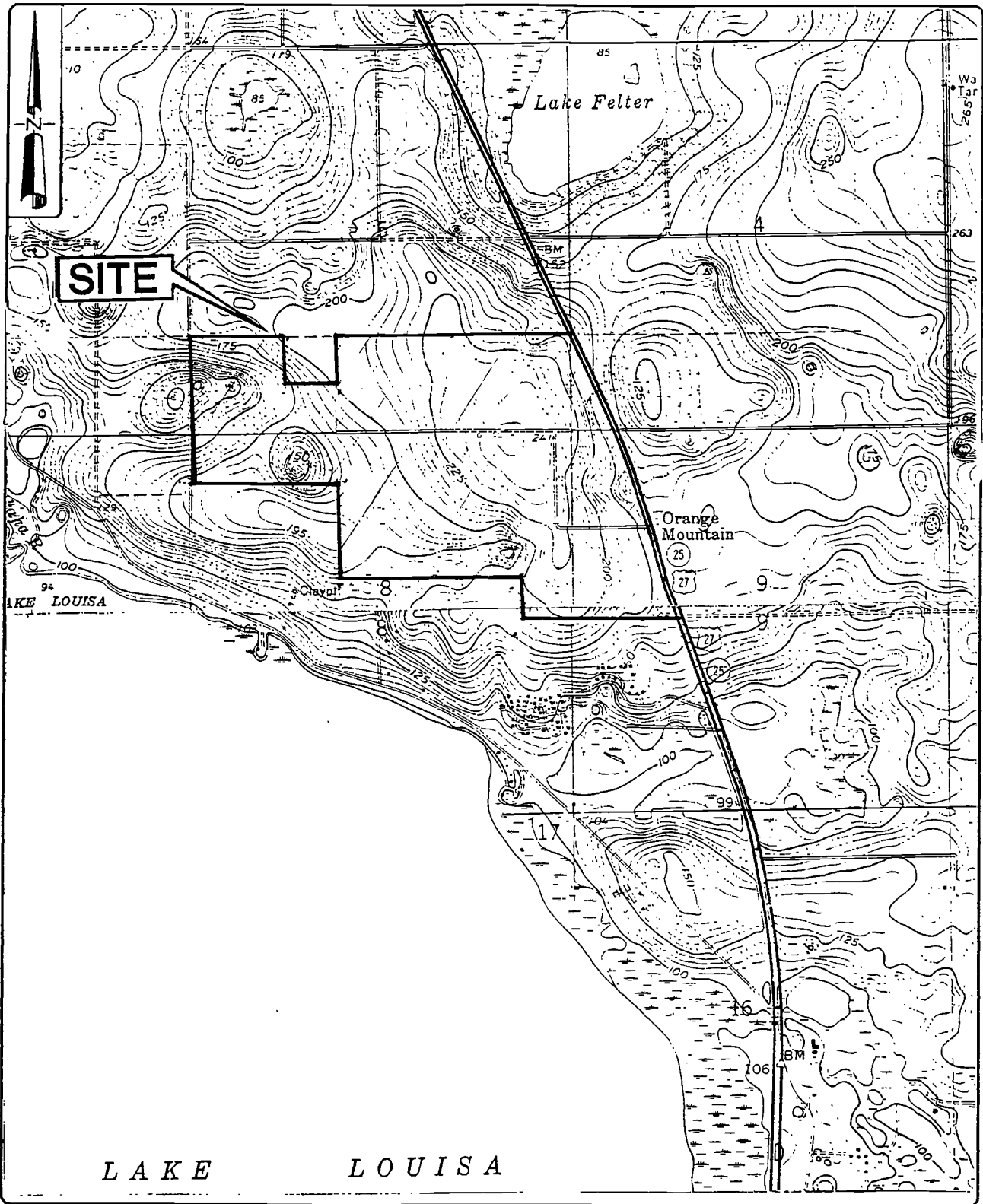
Depending on final grades, berms may be required for the DRA's adjacent to the U.S. 27 right-of-way. Water seepage through the berms can be controlled with a clay core. The core should be at least 2 feet wide, located in the center of the berms, and extend at least 3 feet below the surface elevation of the adjacent right-of-way. The core material should consist of clayey sand or sandy clay having at least 30 percent by weight passing the No. 200 sieve, a liquid limit between 30 and 50, and a plasticity index between 15 and 30. The core material should be placed in maximum 8 inch thick loose lifts and each lift should be compacted to at least 95 percent of the modified Proctor (ASTM D1557) maximum dry density of the soil. A moisture content between 1 percent below and 3 percent above the ASTM D1557 optimum moisture content is recommended during compaction. After plans have been prepared, additional recommendations can be provided regarding the horizontal and vertical extent of the clay core.

### **4.4 Roadway Cut Area**

Stratum 1 sands were found the entire depth of boring AB-3 which was performed in the proposed cut area. These sands are suitable for roadway support and for fill below pavement and structures.

The Stratum 2 and 3 soils found in some of the borings will also be suitable for roadway support and fill. However, the Stratum 4 and 5 clayey soils will not be suitable for roadway or structure support. Stratum 4 and 5 can be used in lower portions of fills but not within 4 feet of pavements and structures.

**FIGURES**



LAKE LOUISA

**REFERENCE:**

U.S.G.S. CLERMONT EAST, FLA.  
 QUADRANGLE MAP  
 DATED 1962  
 PHOTOREVISED 1980  
 SECTION 4  
 TOWNSHIP 23 SOUTH  
 RANGE 26 EAST



**Andreyev  
 Engineering,  
 Inc.**

DATE: 4-11-97

SCALE: 1"=2000'

ENGINEER: DJR

PN: PGT-96-165

GEOTECHNICAL INVESTIGATION

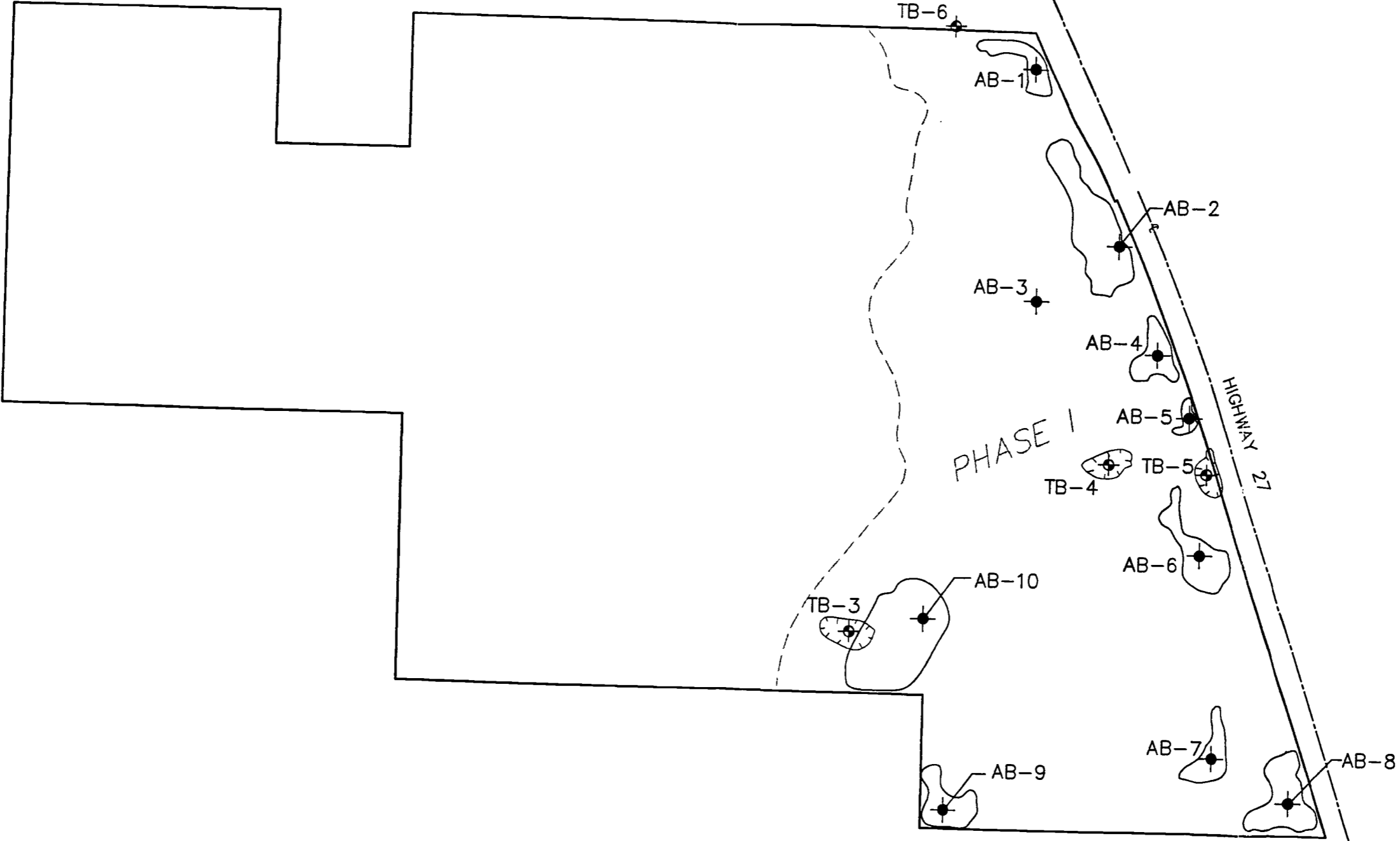
LAKE LOUISA CLUB

LAKE COUNTY, FLORIDA

VICINITY MAP


FIGURE 1

LAKEFT

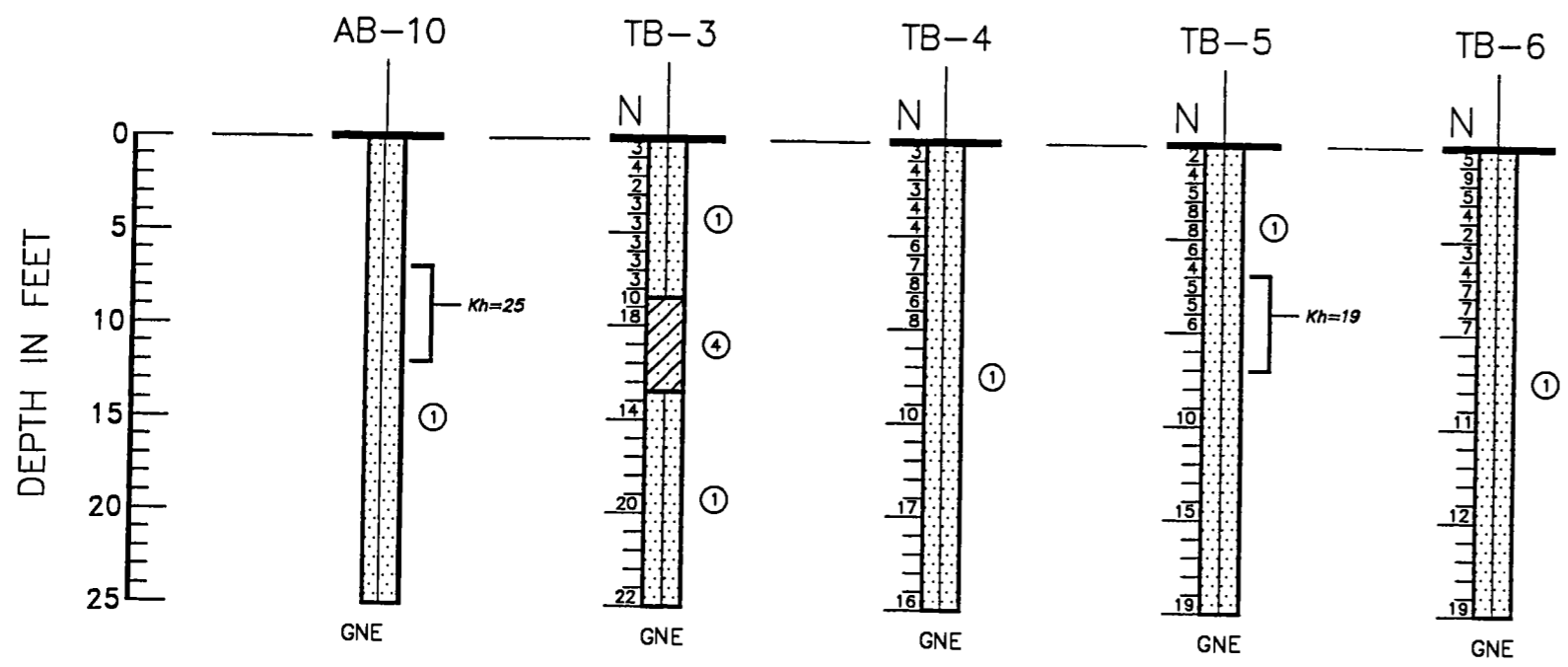
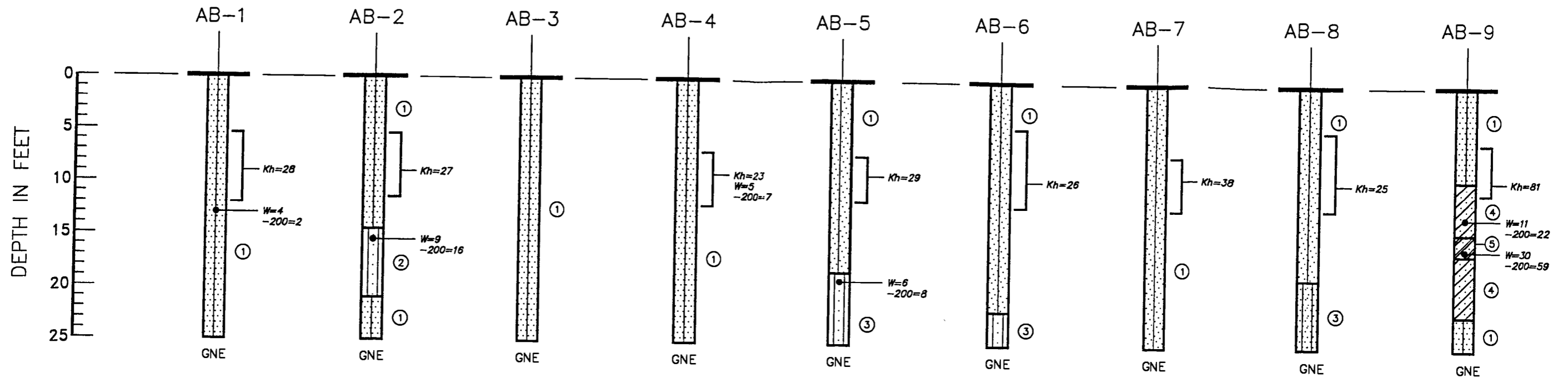


**LEGEND**

- LOCATION OF AUGER BORING
- ⊕ LOCATION OF SPT BORING (DRILLED 11/96)


 <b>Andreyev Engineering, Inc.</b>	GEOTECHNICAL INVESTIGATION LAKE LOUISA CLUB LAKE COUNTY, FLORIDA	
	LOCATION PLAN FIGURE 2	
DATE: 4-11-97 ENGINEER: DJR	SCALE: 1"=600' PN: PGT-96-165	





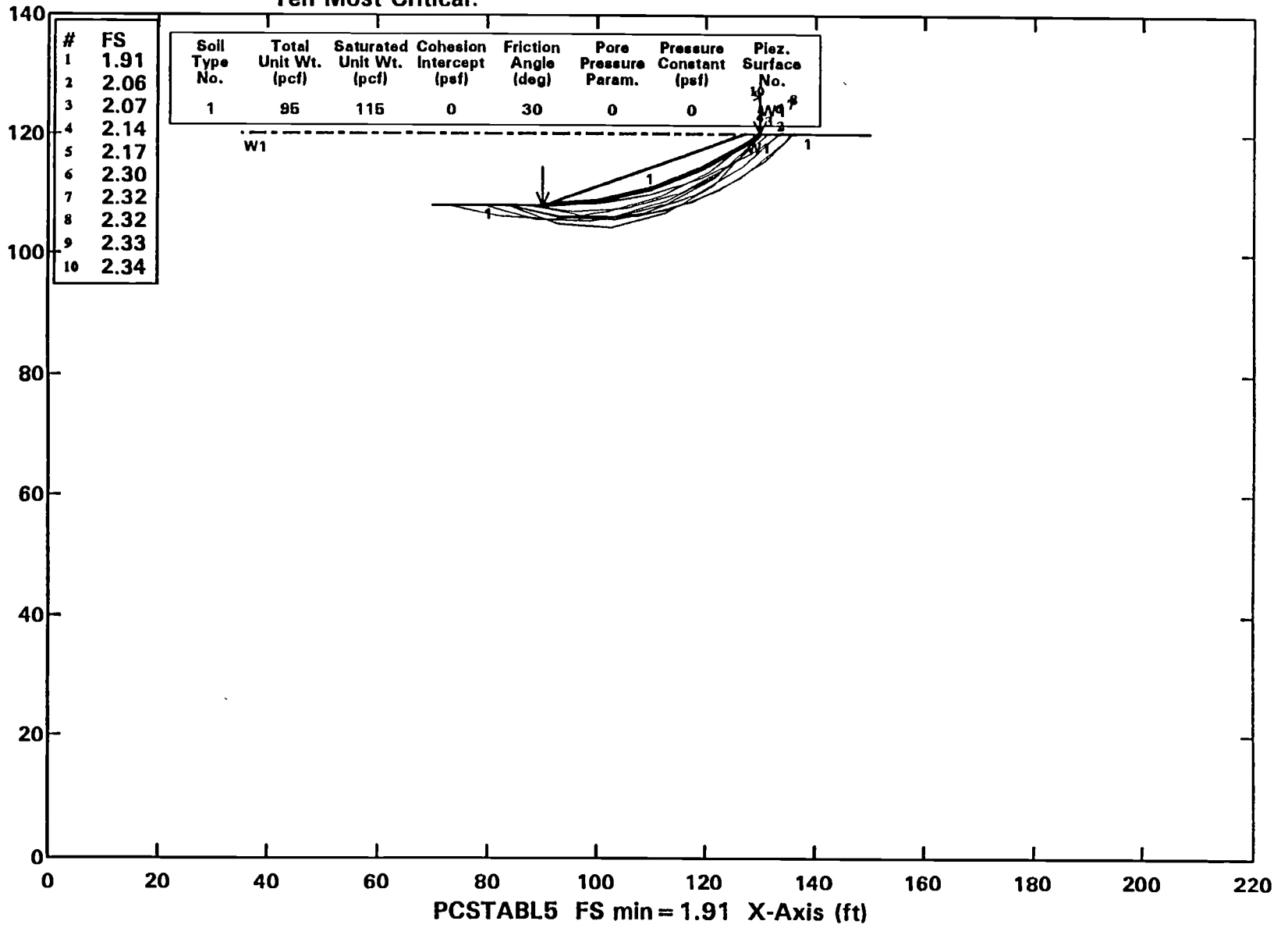
**LEGEND**

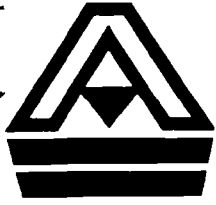
- ① BROWN TO REDDISH BROWN FINE SAND TO FINE SAND WITH SILT (SP) (SP-SM)
- ② REDDISH BROWN SILTY FINE SAND (SM)
- ③ LIGHT BROWN TO REDDISH BROWN FINE TO MEDIUM SAND (SP)
- ④ REDDISH BROWN TO GRAY CLAYEY FINE SAND (SC)
- ⑤ GRAY SANDY CLAY (CH)
- (SP) UNIFIED SOIL CLASSIFICATION GROUP SYMBOL
- N STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT
- W NATURAL MOISTURE CONTENT, IN PERCENT
- 200 PERCENT OF FINES PASSING THE U.S. No. 200 SIEVE
- Kh HORIZONTAL COEFFICIENT OF PERMEABILITY, IN FEET PER DAY
- GNE GROUNDWATER LEVEL NOT ENCOUNTERED TO MAXIMUM DEPTH OF BORING

 <b>Andreyev Engineering, Inc.</b>	GEOTECHNICAL INVESTIGATION LAKE LOUISA CLUB LAKE COUNTY, FLORIDA	
	SOIL PROFILES FIGURE 3	
DATE: 4-11-97 ENGINEER: DJR	SCALE: 1"=10' PN: PGT-96-165	

**APPENDIX A**

Ten Most Critical.





# Andreyev Engineering, Inc.

TAVARES OFFICE  
107 W. Main St., Suite B  
Tavares, Florida 32778  
352-742-9622  
Fax: 352-742-9623  
Email: ANDENGI@AOL.COM

▼ Groundwater ▼ Environmental ▼ Geotechnical ▼ Construction Materials Testing

July 28, 1998

Mr. Duane Booth  
FARNER-BARLEY & ASSOCIATES  
350 North Sinclair Ave.  
Tavares, FL 32778

Re: Legends Subdivision, Clermont, Lake County, FL

Dear Duane,

Per our conversation, the bottom of aquifer for Boring AB-19 without excavation of Stratum 3 should be set at 6 feet below ground surface.

It is understood that the pond bottom will be set at 8 feet below the existing ground surface. Due to the low permeability Stratum 3 soils encountered, we recommend over-excavating the clayey material to a depth of 11 feet below ground surface and replacing it with clean fine sand. This should provide adequate buffer between the pond bottom and the Stratum 3 soils.

Further, our field permeability test was conducted from ground surface to a depth of 9.5 feet and the horizontal hydraulic conductivity measured 19 feet per day.

If you have any questions or if I may be of any further assistance, please do not hesitate to call.

Sincerely,

ANDREYEV ENGINEERING, INC.

  
Ray Jones, E. I.  
Project Manager

RJ/mls

**BEST MANAGEMENT PRACTICES PLAN**

## BEST MANAGEMENT PRACTICES PLAN

Prepared For:  
Lake Louisa Club

An integrated pest management (IPM) program involves six basic areas:

1. **GOLF COURSE CONSTRUCTION:**

Soils will be selected to provide adequate drainage and root growth to assure strong healthy turf. Contour plans will be designed to provide a proper balance between surface drainage and surface water retention to protect contiguous wetlands and other water bodies from nutrient and pesticide runoff. Soil surveys will be used to establish soil leach ratings and solid runoff ratings. It should be noted that it is typical in golf course construction to either use excavated materials from on-site or to bring materials in. Therefore, the soils profile on the golf course may vary from the existing soil on site and accurate ratings may not be developed until completion of grading.

2. **IRRIGATION**

Consumptive use will vary depending on soil characteristics, stage of growth (established turf or newly planted) and stress factors (humidity, temperature, light intensity, etc.). The irrigation system will be computerized and will include a weather station to allow adjustments in the quantity of water applied. The system will be designed to convert to re-use water when and if it becomes available.

3. **PLANT SELECTION:**

The turf used will be selected to best match industry standards, soil ratings and usage. Wetlands plants to be used in mitigation and upgrading wetlands will be indigenous species and selected based on wildlife habitats and nutrient uptake properties. Tree planting will be done in open areas. Many of the trees may be transplanted from construction areas on-site.

4. **PLANT NUTRITION:**

Based on the soil analysis conducted, lime and fertilizer may be applied before planting to correct any imbalances which may exist. It is our intent to maintain a pH between 6.0 and 6.5 for maximum utilization of the secondary elements and to produce turf better able to withstand disease and pest attacks. Rates of application and fertilizer mixes will be adjusted based on manual soil surveys, growth rates, visual and playing conditions, etc.

5. **PESTICIDE SELECTION:**

Pesticides will be selected and applied based on soil surveys and consistent with guidelines issued by the Environmental Protection Agency, Soil Conservation Service, Florida Institute of Food and Agricultural Sciences and other appropriate agencies. Outside consultants will be used to assist in the selection process. As previously discussed, the construction of a golf course involves cutting existing grades, building up others, excavating lakes and filling other areas, etc. As a result, specific pesticide selections for each area of the course are not possible until completion of grading. A detailed plan will, however, be prepared before the application of any pesticides begins. Pesticides used in the program will be reviewed regularly and replaced as preferred alternatives become available. Organic materials and biological control agents will be used as they are developed.

6. **OPERATION AND MAINTENANCE:**

Only licensed operators will be permitted to apply pesticides and a minimum of two trained operators will be employed. Spray mixtures will be prepared only as per the written instructions of the golf course superintendent. A computerized spray unit will be used to apply pesticides. The unit must be programmed by the superintendent and will be capable of measuring the amounts remaining, etc. The unit will also automatically recalibrate itself to adjust the amount of chemicals being applied based on changes in ground speed, engine speed, terrain, etc. "Driplet" nozzles will be used to eliminate spray drift. A daily log of spray applications will be maintained listing date, area treated, weather conditions, reason for treatment, materials and rate applied, and operator's name. Chemicals and fertilizers will be stored and mixed in a maintenance area remote from water bodies and wells. Closed systems will be used to transfer, mix and load pesticides. The storage and handling area will be under the control of the superintendent.

**LAKE LOUISA CLUB  
GOLF COURSE GROUNDS**

**INTEGRATED PESTICIDE/NUTRIENT MANAGEMENT PLAN**

This plan has been designed to fulfill the three (3) principal objectives itemized below:

- 1) Maintain a balanced and healthy turf to maximize its natural resistance to disease:
- 2) Control turfgrass infestations below levels which necessitate widespread chemical treatments:
- 3) Progressively reduce dependence on chemicals through an ongoing turf monitoring and management program.

Beginning with golf course construction and continuing through project build-out, Lake Louisa's IPM Plan focuses primarily on the six basic and essential elements that follow. Each of these has been discussed more fully in subsequent sections.

**GOLF COURSE DEVELOPMENT:**

Follow construction strategies that take into account and provide for soil selectivity and conditioning, site shaping and contouring, erosion control, turfgrass suitability, opportunities for a variety of environmental enhancements.

**CULTURAL AND WILDLIFE PRACTICES:**

Use the most current management procedures to maintain a healthy and luxuriant turf over golf areas, and in other lawn acreage throughout Lake Louisa Club. Lake Louisa Club for water conservation and maximize its natural filtering capabilities.

**BIOLOGICAL PRACTICES:**

Minimize fairway play acreage; while establishing the most disease resistant turfgrasses; and utilize to the greatest possible extent native vegetation and roughs.

**CHEMICALS:**

Apply chemical treatment only on an as-needed basis, and select the most effective, non-persistent products that are formulated for local soils. Applications instructions will be strictly followed, and care will be taken to avoid highly toxic pesticides and those that produce allergenic or otherwise objectionable aerosols.

**RECORDS:**

Keep a daily log(s) to record all maintenance and improvement activity associated with the golf course and other grounds within the Lake Louisa Club community. This would include repairs, modifications, and new construction; mowing and irrigation schedules; and particulars on fertilizers, conditioners, and pesticide applications (personnel, compound, purpose, date and time, ambient weather, amount, precautions or procedures). Also, comply with the sampling, submittal, and record-keeping requirements of permitting and regulatory agencies.



## UPGRADING

The overall purpose of the IPM Plan is to provide a framework for effective and efficient ongoing operations, together with the review and evaluation features needed to make measurable improvements in the plan as experience and technology may dictate. In this regards, Lake Louisa Club has retained the services of an impressive consultation staff, and has established a relationship with turf, soil, and pesticide specialists at the University of Florida, the U.S Soil Conservation Service, and the EPA.

Soil reserves at Lake Louisa Club property are sufficient to provide most of the materials needed to grade-out all golf areas. Tees and greens will be built-up at least three feet above existing grades, since their spaces normally receive heavier chemical applications than other playing areas. At the completion of final grading, surveys will be conducted to determine soil fertility and other properties essential for successful seeding and germination. We expect there will be some requirements for lime, fertilizers, and perhaps other soil conditioners. Until a grass cover is established erosion will be controlled through the use of filter fabric, mulches, and hay bales and in some cases sodding with Bermuda grass or Bahia.

The irrigation system will be totally automated.

## CULTURAL PRACTICES

Cultural practices involve all the various procedures directed toward the maintenance of healthy turf grasses and associated landscaping. The key to healthy turf is intensive, daily care. This includes cutting with sharp and accurately adjusted mowers, together with a comprehensive inspection for incipient problems. Grass that is infrequently cut, cut too short, or cut by dull blades becomes weakened and susceptible to disease and weeds.

Such techniques as verti-cutting, thatching, aeration, topdressing, frequent soil testing, timely fertilization, and many other positive practices all help keep a high quality turf without the excessive use of toxic chemicals.

The Importance of a sound irrigation system cannot be overemphasized in good turf and landscape management practices. Lake Louisa Club's configuration has been designed around automated controls that can be operated on the basis of on-site weather data, as well as specific requirements associates with a variety of tasks such as fertilization, overseeding, and the like. This system includes a frequent and rigid inspection and maintenance program to avoid mechanical failures, and to insure adequate coverage's at calculated flow rates.. The precautions should essentially eliminate flooding from 'blowouts', nutrient losses by leaching or puddling or "burn-outs" from lack of water.

## BIOLOGICAL PRACTICES

Biologically, the first and most important Best Management Practice (BMP) is the selection of appropriate, site specific grasses and landscaping vegetation. Turf grasses will vary by golf course areas depending on their characteristics relative to play requirements on tees, fairways, roughs, collars, fringes, and greens. At present, plans call for the use of three (varieties of Bermuda grass on fairways (T-419), Tees (T-328), and greens (Tifdwarf). For the most part, on-site trees and shrubs will be transplanted where there are plans to create landscaping and vegetative focal points. Elsewhere the landscape will be selected from lists of hardy xeriscaped listings and attractive species that are beneficial to both resident and migratory wildlife.

Also, biological agents will be used, as they become available, to counteract turf and landscaping problems that would otherwise require control by chemical means. To the extent possible, this type of control can be achieved to some degree by nurturing the beneficial insects and microbes that normally occur under conditions conducive to plant growth. One area of recent research on biological pest control involves the use of nematodes to keep mole crickets in check. Findings from 33 golf courses in Florida suggest that the use of these worms alone can significantly reduce the incidences of serious mole cricket infestations.

### CHEMICALS

In spite of every effort to adhere to BMP's we recognize that all categories of pests may have to be controlled by chemicals at one time or another. Our rationale in the use of chemical controls is to apply minimal amounts, as necessary, to prevent chemical treatment. In this regard, our general guidelines for pesticide usage have been summarized below.

- The only pesticides used will be those having a half-life of 70 days, or less. Also, considerations will be given to their N-octanol/water partition coefficients, lethal dose coefficients, and their solubility properties. As noted above, current soil analyses will be used to determine soil-pesticide interaction ratings as issued by both the USDA and the Institute for Food and Agricultural Sciences (IFAS) at the University of Florida. In each fiscal year listings of chemicals, and application rates and schedules will be prepared and submitted to regulatory agencies upon request.
- In the case of each pest, threshold tolerance levels will be recorded and updated. Naturally, this number will vary on the type of infestation, turf condition, and course location. For example, healthy turf is more likely than poor turf to withstand a moderate infestation by the white grub. And Similarly, more pest damage can be accepted in fairways and roughs than on tees and greens.
- The timing of pesticide applications is a critical factor in reducing the overall need for chemical use. Even though our objective will be to maintain effective control by the use of spot-treatments and good course conditioning, there will be times when the broad application of particular pesticide is required. One such occasion, for example, might be in early summer, when dosing the entire course for mole cricket larvae could alleviate the need for frequent and stronger applications throughout the warm-weather season when they are much longer and harder to kill. Through this type of understanding, the principal goal of Rock Springs Ridges' chemical program is to maximize pest control while minimizing the use of toxic substance.
- Qualified supervision and conscientious oversight are key to the success of our chemical usage program. Therefore, a very careful selection will be made to fill the position of superintendent for the golf course and grounds. This person must be well schooled in horticulture and turf sciences, and must be state licensed to handle and distribute pesticides. Experience will be another very important consideration in this choice, since together with effective redemption. The particulars concerning pesticide storage and anticipated use are described in the attached exhibit.

### RECORDS

Record keeping is ultimately the most important and a valuable component of our IPM Program. In this way, daily log entries will provide a long-term data base regarding chemical treatments. Over time, this information will become critically important in the documentation, development, and justification of effective pest control methodologies at Lake Louisa Club. Furthermore, this database will provide essential information for accounting and inventory control, water quality monitoring tasks, and for reviews by local, state and federal regulatory agencies.

## UPGRADING

In the recent past, turf management, horticulture, and integrated pest management have become academic disciplines based on a growing foundation of scientific inquiry. In the construction of Lake Louisa Club, we intend at the outset, to benefit from all applicable information that is now available in these areas. Thereafter, over the long-term, every effort will be made to continuously upgrade our own experience and implementations, and through our respective professional affiliations.

## RECORD KEEPING

Record-keeping is the ingredient tying the IPM Program together and maximizing its efficiency. There are two aspects to record-keeping.

- History of pest problems, including when and where, probable cause, treatment tried, results, and any other factor (such as weather) which may be relevant.
- Daily record of pesticides/fertilizers applied, including concentrations, methods of application, operator, reason (cyclical, preventative, problem area, etc.) Weather conditions, and total quantities applied.

The forms used to record the information can be tailored to the golf course superintendent's preference; however, it should be remembered that they will be important for a number of different applications, including:

- The superintendent will be using them for solving, scheduling and purchasing and inventory control.
- The internal and external accountants will be using them for financial statement preparation and inventory control.
- The external auditor responsible for monitoring water quality will be using them for determining testing parameters and analyzing test results.
- Local state and federal officials will be using them to monitor adherence to overall governmental standards as well as compliance with specific development order or other permitting requirements.

## STORAGE

- All chemicals will be stored separate from fertilizer or fuel's.
- The storage building will be self contained to prevent contamination of the ground and ground water in the case of container failure. It will have ventilation, all proper caution signs, and a locked door at all times.
- With the increasing number of golf courses, this area is experiencing many more suppliers. Therefore, it is not necessary to stock large quantities of chemicals. It is anticipated this building will be in the range of 100-150 sq. Ft. and the products will be used or returned to the supplier by the end of each season.

**LAKE LOUISA CLUB**

**GENERAL COMMENTS:**

The following is a generalized guideline that has been proven to supply quality playing characteristics on Florida Golf Courses. Careful evaluation shall be given individual turf and soil conditions prior to implementing any changes to the below outlined program.

Careful attention shall be given to the fertilizer and chemical application rates and overspray. The adjacent environmentally sensitive areas shall not be adversely influenced by the golf course fertilizer and chemical maintenance programs.

The below Fertilizer Program shall be adjusted for available nutrients provided by the effluent re-use water.

**FERTILIZATION PROGRAM**

	WHEN	LBS. N	P	K
GREENS:	March-June	1.5 lb.	1/4 lb.	3/4 lb per 1000 Sq. Ft. every 2 weeks
	July-Sept.	1.0 lb.	1/4 lb.	3/4 lb per 1000 Sq. Ft. every 3 weeks
	Oct-Nov	1.5 lb.	1/4 lb.	3/4 lb per 1000 Sq. Ft. once per month
	Dec-Feb	1.5 lb.	1/2 lb.	0 lb per 1000 Sq. Ft. every 3 weeks

Milorganite

Dec-Feb				1 lb per 1000 Sq. Ft. every 6 weeks
---------	--	--	--	-------------------------------------

Sulfate Potash

TEES: Same as above except July-Sept. Only once per month.

FAIRWAYS:	October	Balanced Mixture to supply 1.5 lbs. N per 1000 Sq. Ft.		
	March	1.5 lbs.	0 lbs.	1.5 lbs per 100 Sq. Ft.
	*June	Same as October		

NOTE: If the IFAS Approved Biological Control "Nematode Program" (which is in various research states at the present time) is proven successful, the need for this control will be eliminated.

ROUGHES: Follow Fairway Guide

COMMENTS: Modify as the soil samples indicate.

MIXTURES: This will vary depending on soil analysis, but in general will be as follows:  
The balanced mixture to have a ratio of 4-1-3 with Nitrogen, Phosphorous and Potash.

NITROGEN: 35% Water Soluble - Such as Nitroform, I.B.D.U., or equal  
05% Natural Organic - Such as Milorganite or equal  
50% Ammonoical - Such as Sulfate of Ammonia

PHOSPHOROUS: Super Phosphate or Ammoniated Super Phosphate

POTASSIUM: 50% Sulfate of Potash Magnesium  
50% Sulfate of Potash

MINOR ELEMENTS: Will be added in trace amounts as indicated by the soil analysis

### HERBICIDE PROGRAM

This is a "Guideline Program Only" to be used only after identification of pest problem is evident.

PRE-EMERGENT: Greens and all overseeded surfaces (Tees, Collars, Etc.)  
Use: Scott's Goosegrass Crabgrass Control @ Label Rate, apply 3rd week in February  
then @ 60 day intervals  
Not to exceed 3 applications.  
Fairways & Other areas  
Use: Ronstar @ label rate in late February  
Repeat @ 90 day intervals.

NOTE: Each application is to be at rates designed to keep Bermuda Turf vigorous and healthy.

POST-EMERGENT As needed only.

BROADLEAF: Trimec at label rates.

CROWFOOT: We are recommending following the new guidelines as presented by the Manufacturer of Illozan. This product is now being introduced to golf courses and has been approved by the EPA as needed only.

### INSECTICIDES PROGRAM

Mole Crickets - Spot Control with Orthene @ 4 lbs. Per acre.

NOTE:

- 1) If "IFAS" Biological Control "Nematode Program" is proven successful, this will be used.
- 2) We will attempt cultural practices to try to co-exist with Parasitic Nematodes.

Worms: As needed apply Turcam or Sevin at label rates.

**FUNGICIDE PROGRAM**

Other - As needed after identification of problem.

Mowing Schedule and All Service Work - Please have Superintendent read and sign off on our Operational Manual.

**SOIL ANALYSIS**

Test all Greens First Year and Six (6) Representative Tees and Fairways.

Second Year tees Six (6) Representative Greens, Tees and Fairways.

**NEMATICIDES**

We will attempt cultural practices to try to co-exist with Parasitic Nematodes.

Please find below, our recommendations for pesticide usage at Lake Louisa Club. This is to be updated on a regular basis of once every six months or once per year to meet new requirements and introduce possible new products which may be more effective in treatment and control. Again, we would like to stress that our operational manuals and pre-operation training is geared to educate owners and employees in all plausible uses of non-chemical or cultural control options. Our program on all projects is to create a solid management program which controls targeted pests while leaving our 'Biological Friends' in existence to help fight the battle.

TABLE I - List of Insecticides for Use

PRODUCT TRADE NAME	USE	METHOD	TARGET
Sevin	Turf	Spray & Use	Mole Crickets, Worms
Amdro	Turf	Granular	Ants
Orthene	Turf	Spray	Mole Crickets, Worms, Grub
Triumph	Turf	Spray	Mole Crickets
Turcam	Turf	Spray	Worms, Mole Crickets
Crusade	Turf	Granular	Mole Crickets
Nemacur	Turf	Granular	Nematodes
Mocap	Turf	Granular	Nematodes

TABLE II - List of Fungicides

PRODUCT TRADE NAME	USE	METHOD	TARGET
Alliette	Turf	Spray	Pythium
Subdue	Turf	Spray	Pythium
Fore	Turf	Spray	Helminthosporum
Daconil	Turf	Spray	Rizortonia
Chipeo 26019	Turf	Spray	Helminthosporum
Banner	Turf	Spray	Fusarium

These products are used for specific disease and are alternated to avoid build-up of metals and disease resistance. Again, we recommend lighter than recommended rates with consistent application formats.

TABLE III - List of Herbicides

PRODUCT TRADE NAME	USE	METHOD	TARGET
Scott's Pre-Em	Turf	Spray	Crowfoot
Scott's Crabgrass	Turf	Granular	Crowfoot
Illoxan	Turf	Spray	Crowfoot
Basagran	Turf	Spray	Sedges
M.S.M.A.	Turf	Spray	Crabgrass, Sedges
Trimec	Turf	Spray	Broadleaf
Ronstar	Turf	Granular	Crabgrass, Goosegrass
Primo	Turf	Spray	Growth Regulator
Round-up	Turf	Spray	Non-Selective
Barricade	Turf	Spray	Pre-Emerge
Finale	Turf	Spray	Non-Selective

NOTE: These products are not to be used in excess of the Manufacturer's recommendation for the year.

RECEIVED

AUG 17 1998

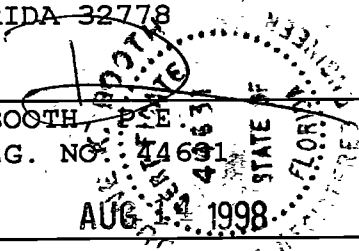
4-069-035 TAEER  
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ORLANDO  
SJR WMD

19451-1

LEGENDS @ KINGS RIDGE  
STORMWATER CALCULATIONS  
FBA NO. 961504.001

FARNER, BARLEY & ASSOCIATES, INC.  
350 NORTH SINCLAIR AVENUE  
TAVARES, FLORIDA 32778

BY: \_\_\_\_\_  
DUANE K. BOOTH, PSE.  
FLORIDA REG. NO. 44691  
DATE: \_\_\_\_\_ AUG 14 1998





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**LEGENDS  
(F/K/A LAKE LOUISA CLUB)**

**STORMWATER DESIGN SUMMARY**

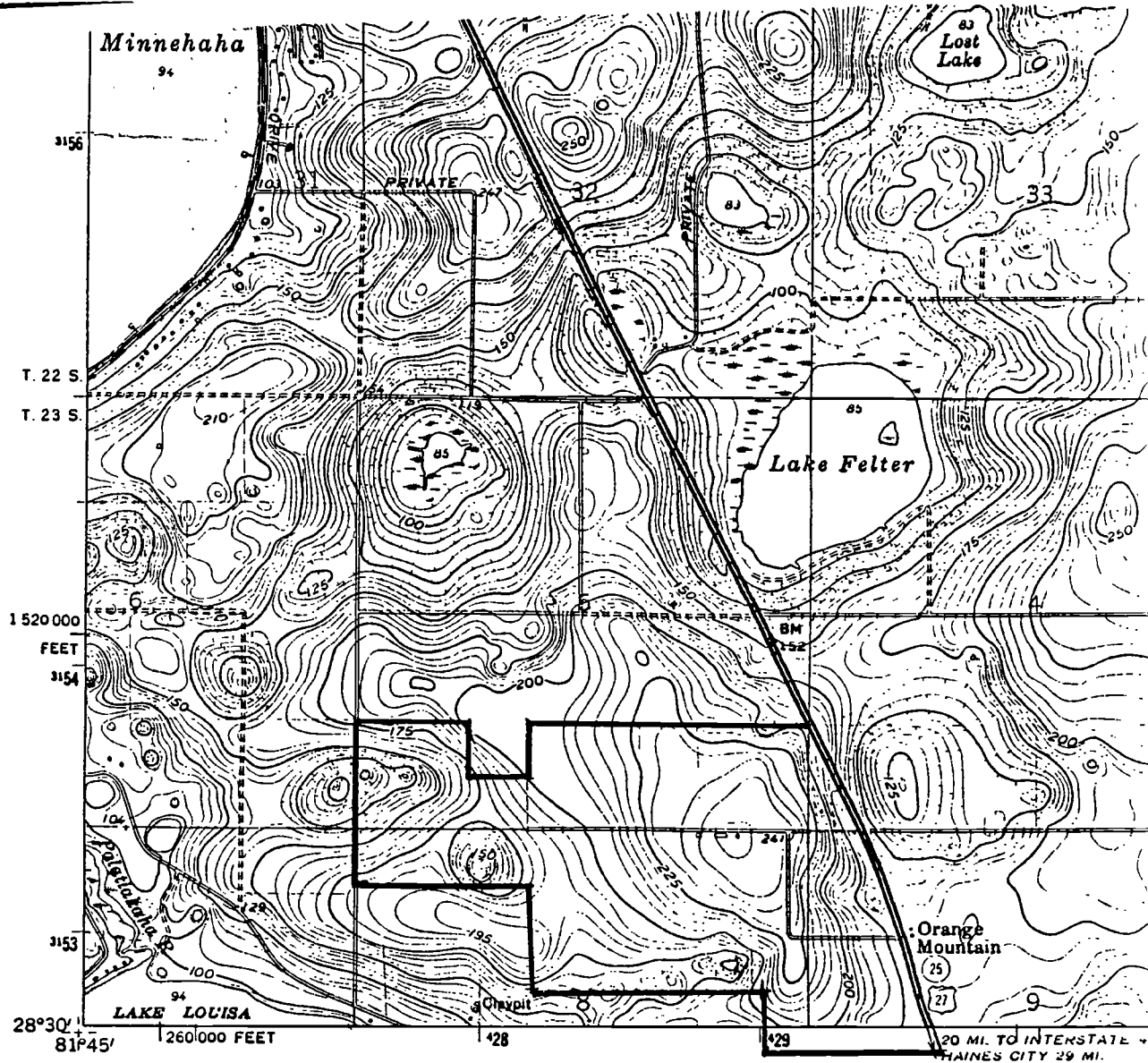
Legends is located in Sections 4, 5, 8, and 9 of Township 23S, Range 26E on U.S. Highway 27 South of Clermont consisting of approximately 403 acres. The property as existing today is mostly burned out orange grove and an abandoned farm house and sheds with a paved drive from U.S. Highway 27 to the farm house. The grove has been replanted with small pine trees.

Since the subject property does not have a positive outfall, the stormwater management system is designed to retain the total runoff from the 25 year-96 hour storm event. Therefore, the pre-develop site conditions were not modeled for pre vs. post comparison.

All ponds have been modeled through "ICPR" with infiltration calculated through "ponds". Pond 9 has been omitted in "ponds" because it is a lined pond and used for irrigation as discussed in the pre-application meeting. Ponds 18, 20, 22, and 24 shall be over excavated and filled with clean sand to provide adequate depth between pond bottom and confining layer as suggested in soil report. The plans and calculations depict the appropriate elevation of excavation. Basins 5, 13, and 17 do not exist and are not referred to in this submittal. These basins were used in preliminary design and were eventually omitted from final design.

See ICPR Max Node conditions for comparison of peak stage versus pond max elevation and ponds Recovery analysis for stormwater treatment volume calculation and recovery analysis.

MAPS



(LAKE NELLIE)  
4640 IV NE

Mapped, edited, and published by the Geological Survey

Control by USGS and USC&GS

Planimetry by photogrammetric methods from aerial photographs taken 1952. Topography by planetable surveys 1962

Polyconic projection

10,000-foot grid based on Florida coordinate system, east zone

1000-meter Universal Transverse Mercator grid ticks, zone 17, shown in blue. 1927 North American Datum

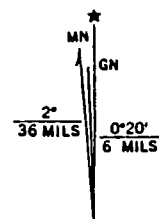
To place on the predicted North American Datum 1983

move the projection lines 27 meters south and

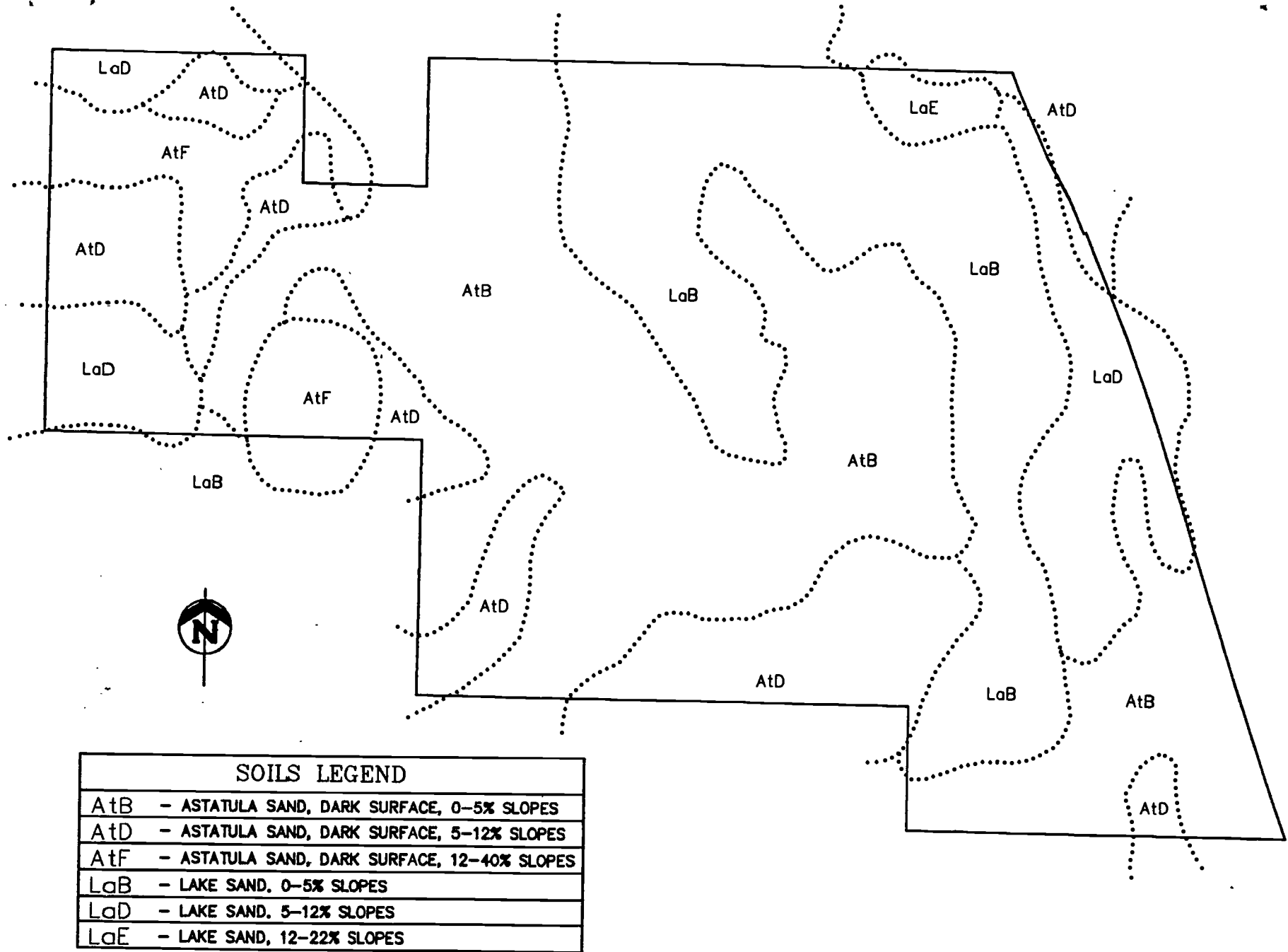
18 meters west as shown by dashed corner ticks

Fine red dashed lines indicate selected fence and field lines where generally visible on aerial photographs. This information is unchecked

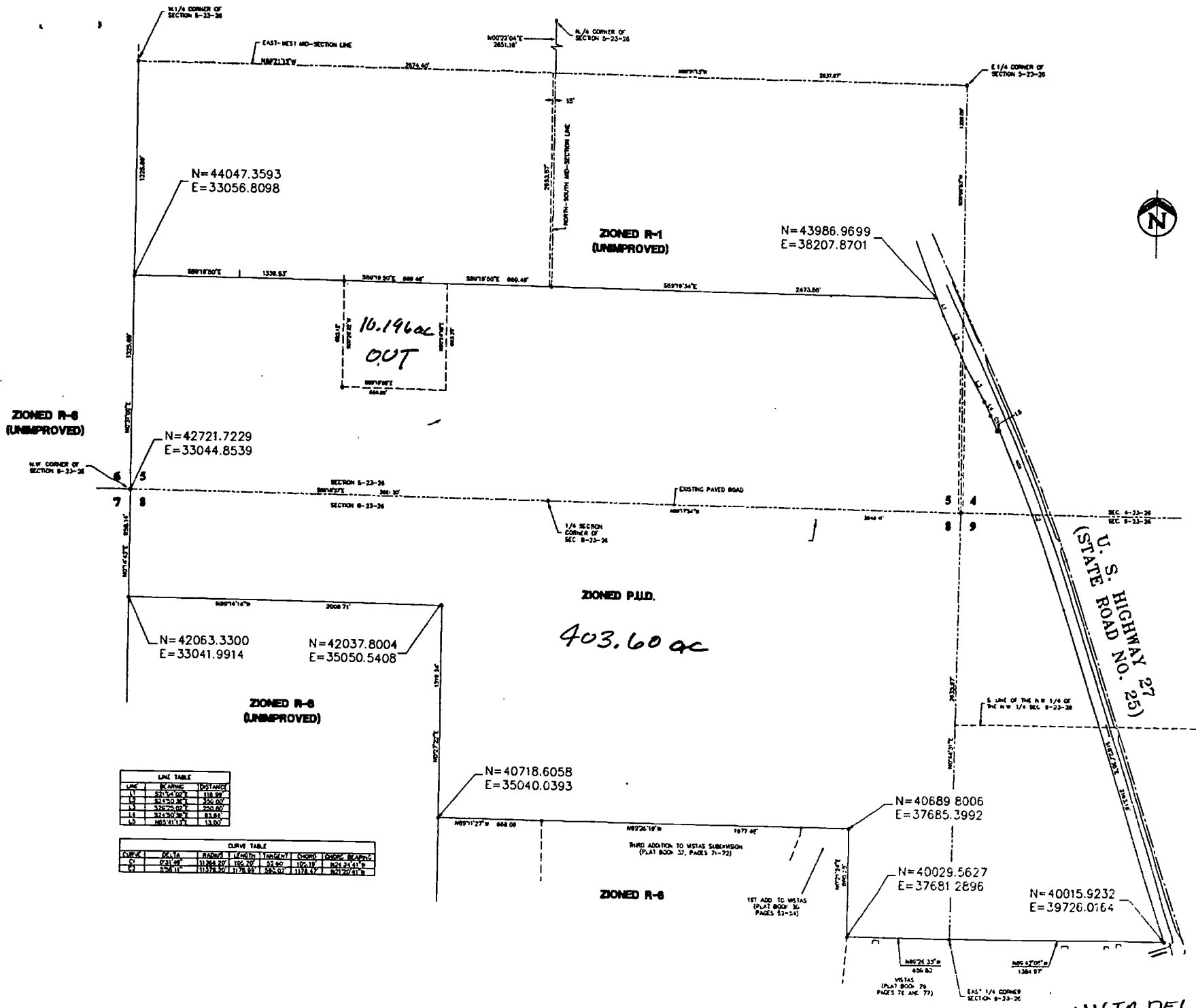
Revisions shown in purple compiled from aerial photographs taken 1977 and other source data. This information not field checked. Map edited 1980



UTM GRID AND 1980 MAGNETIC NORTH DECLINATION AT CENTER OF SHEET



NOTE: SOIL INFORMATION OBTAINED FROM U.S.D.A.  
SOIL CONSERVATION SERVICE.



N=44047.3593  
E=33056.8098

ZONED R-1  
(UNIMPROVED)

N=43986.9699  
E=38207.8701

10.196 ac  
OUT

ZONED R-6  
(UNIMPROVED)

N=42721.7229  
E=33044.8539

ZONED P.L.D.

403.60 ac

ZONED R-6  
(UNIMPROVED)

N=42063.3300  
E=33041.9914

N=42037.8004  
E=35050.5408

N=40718.6058  
E=35040.0393

ZONED R-6

N=40689.8006  
E=37685.3992

N=40029.5627  
E=37681.2896

N=40015.9232  
E=39726.0164

LINC TABLE

LINE	BEARING	DISTANCE
L1	S21°45'00"E	118.89'
L2	S11°10'00"E	255.00'
L3	S28°20'00"E	255.00'
L4	S73°50'00"E	83.85'
L5	N82°11'00"E	13.00'

CURVE TABLE

CURVE	P.C.	P.T.	RADIUS	LENGTH	CHORD	CHORD BEARING
C1	023.49'	11385.22'	105.70'	21.40'	102.19'	N21°21'41"E
C2	028.11'	11378.20'	1178.82'	285.02'	1178.47'	S21°20'41"E

STATE HIGHWAY NO. 27

VISTA DEL RIO PLUD

**DEVELOPED BASIN SUMMARY  
AND CURVE NUMBER CALCULATION**

LOT SIZE	SITE IMPERVIOUS ANBA
65' X 115'	3750 SF
80' X 115'	4725 SF

BASIN NUMBER	AREA (ON SITE) (acres)	AREA (OFF SITE) (acres)	TOTAL AREA (acres)	IMPERVIOUS AREA (acres)	PERVIOUS AREA (acres)	CN
B1	7.84	—	7.84			50
B2a	8.64	—	8.64			55
B2b	18.74	—	18.74			54
B2c	14.84	—	14.84			49
B3	27.66	—	27.66			62
B4	18.39	—	18.39			48
B6	10.47	—	10.47			39
B7	25.19	—	25.19			51
B8	6.92	—	6.92			45
B9	7.81	—	7.81			60
B10	13.60	—	13.60			53
B11	11.52	—	11.52			52




BASIN NUMBER	AREA (ON SITE) (acres)	AREA (OFF SITE) (acres)	TOTAL AREA (acres)	IMPERVIOUS AREA (acres)	PERVIOUS AREA (acres)	CN
B12	14.39	—	14.39			53
B14	4.79	—	4.79			54
B15	16.02	—	16.02			51
B16	17.16	—	17.16			54
B18	23.37	0.64	24.03			54
B19	11.26	—	11.26			51
B20	8.70	—	8.70			51
B21	23.79	—	23.79			57
B22	11.72	3.13	16.56			48



# STORM RUNOFF WORKSHEET

PROJECT #: 961504.001 PROJECT: LEGANOS DATE: 6/2/98  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 1 TOTAL AREA 7.84 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS - GOOD	6.40		39	82	3198
RES	14 X 3750 = 1.21					
PUMT	24 X 414 = 0.23					
	<u>1.44</u>		1.44	98	18	1764
TOTALS						4962

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 50

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. (2) TOTAL AREA \_\_\_\_\_ STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS - GOOD	38.10		39	85	
RES	44 X 3750 = 165,000					
PUMT	24 X 1655 = 39,720					
	BLVD 82,860					
	<u>287,580</u>		6.60	98	15	
TOTALS						

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = \_\_\_\_\_

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: LEGENDS DATE: 6/15/98  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. B2a TOTAL AREA 8.64 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	6.31		39	73	2847	
RES		21 X 3750 = 78,750						
PVMT		24 X 947 = 22,728						
		<u>101,478</u>		2.33	98	27	2644	
TOTALS								5493

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 55$

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. B2b TOTAL AREA 18.74 STORM: 25 YEAR 94 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	13.82		39	74	2886	
RES		21 X 3750 = 78,750						
CLUB SITE		85% IMP = 50,816						
PVMT		= 74,800						
		<u>204,366</u>		4.92	98	24	2548	
TOTALS								5434

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 54$

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: LEGENDS DATE: 6/24/99  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. B2c TOTAL AREA 14.84 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<u>A</u>		<u>12.35</u>		<u>39</u>	<u>83</u>	<u>3237</u>
<u>RES</u>		<u>3 X 4725 = 14,175</u>					
		<u>2 X 3750 = 7,500</u>					
<u>PUMPT</u>		<u>28 X 964 = 26,992</u>					
		<u>48,667</u>		<u>1.12</u>	<u>98</u>	<u>8</u>	<u>784</u>
<u>POND (WET)</u>		<u>EL. 163.00</u>	<u>59,806</u>		<u>1.37</u>	<u>98</u>	<u>882</u>
TOTALS							<u>4903</u>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
<u>A</u>					
<u>B</u>					
<u>C</u>					
<u>D</u>					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 49

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. \_\_\_\_\_ TOTAL AREA \_\_\_\_\_ STORM: \_\_\_\_\_ YEAR \_\_\_\_\_ HOUR \_\_\_\_\_

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
TOTALS							

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
<u>A</u>					
<u>B</u>					
<u>C</u>					
<u>D</u>					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = \_\_\_\_\_

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = 11.6 in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 3 TOTAL AREA 23.59 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	14.49		39	61	23.79
Res		30 x 4725 = 3.25					
PVMT		24 x 1876 = 1.03					
85% PAV/SHOP		5.78 ac. x 0.85 = 4.91					
		9.19		9.19	98	37	3822
TOTALS							6204

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 62

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 4 TOTAL AREA 18.39 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	15.41		39	84	3274
RES		20 x 4725 = 2.17					
PVMT		0.81					
		2.98		2.98	98	16	1568
TOTALS							4844

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 48

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. <b>5</b>		TOTAL AREA <b>2.77</b>			STORM: <b>25</b> YEAR <b>24</b> HOUR		
SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
<b>A</b>	<b>GREEN GRASS - GOOD</b>	<b>2.77</b>	<b>0</b>	<b>39</b>	<b>100</b>	<b>3400</b>	
				<b>98</b>	<b>0</b>	<b>0</b>	
TOTALS						<b>3100</b>	

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = **39**

$S = \frac{1000}{CN} - 10$

$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.

RUNOFF R = \_\_\_\_\_ in.

\_\_\_\_\_ ac.ft.

\_\_\_\_\_ cu.ft.

BASIN NO. <b>6</b>		TOTAL AREA <b>10.47</b>			STORM: <b>25</b> YEAR <b>24</b> HOUR		
SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
<b>A</b>	<b>GREEN GRASS - GOOD</b>	<b>10.47</b>	<b>0</b>	<b>39</b>	<b>100</b>	<b>3400</b>	
				<b>98</b>	<b>0</b>	<b>0</b>	
TOTALS						<b>3400</b>	

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = **39**

$S = \frac{1000}{CN} - 10$

$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$

Q = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.

RUNOFF R = \_\_\_\_\_ in.

\_\_\_\_\_ ac.ft.

\_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 7 TOTAL AREA 32.65 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS-GOOD	25.89		39	79	3081
	RES	11 X 4725 = 1.19					
	PUM'T	24 X 957 = 0.53					
	85% Rec SITE	6.15 ac. 0.85 = 5.23					
		<u>6.95</u>		6.76	98	21	2058
TOTALS						100	5139

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 51

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 8 TOTAL AREA 6.92 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS-GOOD	6.25		39	90	3510
	RES	6 X 3750 = 0.52					
	PUM'T	<u>0.15</u>					
		<u>0.67</u>		0.67	98	10	980
TOTALS							4490

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 45

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.



# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. <b>9</b>		TOTAL AREA <b>7.81</b>			STORM: <b>25</b> YEAR <b>96</b> HOUR		
SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<b>A</b>	<b>GREEN GRASS - GOOD</b>	<b>5.02</b>		<b>39</b>	<b>64</b>	<b>2496</b>
	<i>Res</i>	<i>9 X 3750 = 0.77</i>					
	<i>PUM'T</i>	<i>24 X 536 = 0.30</i>					
		<i>1.07</i>		<b>1.07</b>	<b>98</b>	<b>14</b>	<b>1372</b>
	<b>POND (WET)</b>			<b>1.72</b>	<b>98</b>	<b>22</b>	<b>2156</b>
TOTALS						<b>6024</b>	<b>6024</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\overline{CN}$  = **60**

$$S = \frac{1000}{CN} - 10$$

$$R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

R = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. <b>10</b>		TOTAL AREA <b>13.60</b>			STORM: <b>25</b> YEAR <b>96</b> HOUR		
SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	<b>A</b>	<b>GREEN GRASS - GOOD</b>	<b>10.29</b>		<b>39</b>	<b>74</b>	<b>2464</b>
	<i>Res</i>	<i>32 X 3750 = 2.75</i>					
	<i>PUM'T</i>	<i>0.27 + 0.29 = 0.54</i>					
		<i>3.31</i>		<b>3.31</b>	<b>98</b>	<b>24</b>	<b>2352</b>
TOTALS							<b>5316</b>

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\overline{CN}$  = **53**

$$S = \frac{1000}{CN} - 10$$

$$Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$$

Q = runoff (in.)  
P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 11 TOTAL AREA 11.52 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS - GOOD	8.97		39	78	3042
RES	21 X 3750 = 1.81					
PUM'T	24 X 1336 = 0.74					
	<u>2.55</u>		2.55	98	22	2154
TOTALS						5198

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 52

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 12 TOTAL AREA 14.34 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS - GOOD	10.99		39	76	2964
RES	27 X 3750 = 2.32					
PUM'T	24 X 2127 = 1.17					
	<u>3.49</u>		3.49	98	24	2352
TOTALS						5316

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 53

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.



# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_

PRE-DEVELOPMENT  
 POST-DEVELOPMENT

BASIN NO. 15 TOTAL AREA 16.02 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	12.74		39	80	3120
		20 x 4725 = 94,500					
		24 x 2021 = 48,504					
		<u>143,004</u>		3.28	98	20	1960
TOTALS							5080

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 51$

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 16 TOTAL AREA 17.16 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	12.29		39	72	2808
		33 x 4725 = 155,925					
		24 x 2353 = 56,472					
		<u>212,397</u>		4.87	98	28	2744
TOTALS							5552

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN} = 54$

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 17 TOTAL AREA 0.42 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
A	GREEN GRASS-GOOD	0.42		39	100	3900
TOTALS						3900

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 39

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 18 ON SITE + OFF SITE TOTAL AREA 24.03 STORM: 25 YEAR 96 HOUR

SOIL GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	23.37 ON SITE					
A	GREEN GRASS-GOOD	18.11		39	75	2925
	24 x 2479 = 59,496					
	42 x 4725 = 198,450					
	<u>257,946</u>		5.92	98	25	2450
TOTALS						5375

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 54

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT #: \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. 19 TOTAL AREA 11.26 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	8.91		39	79	3081
PUMT		24 X 1315 = 3,156					
RES		21 X 4725 = 99,225					
		102,381		2.35	98	21	2058
TOTALS							5139

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 51

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 20 TOTAL AREA 8.70 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	6.95		39	80	3120
RES		13 X 3750 = 48,750					
PUMT		24 X 1142 = 27,408					
		76,158		1.75	98	20	1960
TOTALS							5080

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = 51

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 Q = runoff (in.)  
 P = rainfall (in.)  
 RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_

PRE-DEVELOPMENT  
 POST-DEVELOPMENT

BASIN NO. 21 TOTAL AREA 23.79 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	16.50		39	69	2691	
		RES	65 X 3750 = 243,750					
		PUMPT	24 X 3077 = 73,848					
			<u>317,598</u>	7.29	98	31	3038	
TOTALS								5729

PRODUCT COVERAGE =  $\overline{CN}$  = 57

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. 22 <sup>ONSITE + OFFSITE</sup> TOTAL AREA ~~16.56~~ 14.35 STORM: 25 YEAR 96 HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA	
	A	GREEN GRASS - GOOD	12.12		39	84	3274	
		RES	23 X 3750 = 86,250					
		PUMPT	24 X 450 = 10,800					
			<u>2.23</u>	2.23	98	16	1568	
TOTALS								4844

PRODUCT COVERAGE =  $\overline{CN}$  = 48

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.8S)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ / cu.ft.

# STORM RUNOFF WORKSHEET

PROJECT # \_\_\_\_\_ PROJECT: \_\_\_\_\_ DATE: \_\_\_\_\_  PRE-DEVELOPMENT  POST-DEVELOPMENT

BASIN NO. **23** *ON SITE + OFF SITE* TOTAL AREA **50.90** STORM: **25** YEAR **96** HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	41.75		39	82	3198
RES		65 X 4725 = 274,625					
PUMT		24 X 5166 = 123,984					
		<u>398,609</u>		9.15	98	18	1764
TOTALS							4962

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = **50**

$S = \frac{1000}{CN} - 10$   
 $R = \frac{(P - 0.2S)^2}{(P + 0.85)}$   
 R = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.

BASIN NO. **24** *ON SITE + OFF SITE* TOTAL AREA **83.94** STORM: **25** YEAR **96** HOUR

SOIL	GROUP	LAND USE	AREA Pervious (acres)	AREA Imperv. (acres)	CN	AREA (%)	PRODUCT CN x AREA
	A	GREEN GRASS - GOOD	72.75		39	84	3276
PUMT		24 X 5750 = 13.17					
RES (65')		78 X 3750 = 6.11					
RES (80')		38 X 4725 = 4.12					
		<u>13.40</u>		13.40	98	16	1368
TOTALS							4844

GROUP	AREA Pervious	%	AREA Imperv.	%	TOTAL AREA
A					
B					
C					
D					
TOTALS					

PRODUCT COVERAGE =  $\bar{CN}$  = **48**

$S = \frac{1000}{CN} - 10$   
 $Q = \frac{(P - 0.2S)^2}{(P + 0.85)}$   
 Q = runoff (in.)  
 P = rainfall (in.)

RAINFALL (P) = \_\_\_\_\_ in.  
 RUNOFF R = \_\_\_\_\_ in.  
 \_\_\_\_\_ ac.ft.  
 \_\_\_\_\_ cu.ft.



ICPR INPUT DATA

Advanced Interconnected Channel & Pond Routing (ICPR Ver 2.01) [9]  
- Copyright 1995, Streamline Technologies, Inc.

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Simulation-----

C:\ICPR2\DATA\LEGENDS

Execution: Hydraulics

Header: LEGENDS OF CLERMONT 25YR96HR STORM EVENT

-----HYDRAULICS-----HYDROLOGY-----

Max Delta Z (ft): 1

Delta Z Factor: 0.05

Override Defaults: No

Time Step Optimizer: 10

Drop Structure Optimizer: 10

Sim Start Time(hrs): 0

Sim End Time(hrs): 96

Min Calc Time(sec): 60

Max Calc Time(sec): 300

To Hour: PInc(min):

96 60

To Hour: PInc(min):

96 60

-----GROUP SELECTIONS-----

+ BASE [07/28/98]

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 1           Base Flow(cfs): 0           Init Stage(ft): 200  
Group: BASE        Length(ft): 0           Warn Stage(ft): 205  
Comment:

Stage(ft)	Area(ac)
200	0.257
201	0.345
202	0.444
203	0.551
204	0.676
205	0.807

-----Class: Node-----

Name: 10           Base Flow(cfs): 0           Init Stage(ft): 210  
Group: BASE        Length(ft): 0           Warn Stage(ft): 219  
Comment:

Stage(ft)	Area(ac)
210	0.093
211	0.178
212	0.37
213	0.706
214	1.089
215	1.268
216	1.412
217	1.558
218	1.727
219	1.934

-----Class: Node-----

Name: 11           Base Flow(cfs): 0           Init Stage(ft): 211  
Group: BASE        Length(ft): 0           Warn Stage(ft): 218  
Comment:

Stage(ft)	Area(ac)
211	0.418
212	0.475
213	0.533
214	0.593
215	0.654
216	0.717
217	0.78
218	0.845

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 2B           Base Flow(cfs): 0           Init Stage(ft): 180  
Group: BASE           Length(ft): 0           Warn Stage(ft): 185  
Comment:

Stage(ft)	Area(ac)
180	1.11
181	1.232
182	1.354
183	1.479
184	1.604
185	1.73

-----Class: Node-----

Name: 2C           Base Flow(cfs): 0           Init Stage(ft): 163  
Group: BASE           Length(ft): 0           Warn Stage(ft): 167  
Comment:

Stage(ft)	Area(ac)
163	0.605
164	0.693
165	0.782
166	1.05
167	1.357

-----Class: Node-----

Name: 3           Base Flow(cfs): 0           Init Stage(ft): 165  
Group: BASE           Length(ft): 0           Warn Stage(ft): 175  
Comment:

Stage(ft)	Area(ac)
165	0.595
166	0.685
167	0.779
168	0.879
169	0.987
170	1.102
171	1.226
172	1.354
173	1.489
174	1.824
175	1.987

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----  
Name: 4           Base Flow(cfs): 0           Init Stage(ft): 177  
Group: BASE       Length(ft): 0           Warn Stage(ft): 185  
Comment:

Stage(ft)	Area(ac)
177	0.729
178	0.846
179	0.971
180	1.102
181	1.231
182	1.363
183	1.614
184	2.041
185	2.704

-----Class: Node-----  
Name: 6           Base Flow(cfs): 0           Init Stage(ft): 199  
Group: BASE       Length(ft): 0           Warn Stage(ft): 204  
Comment:

Stage(ft)	Area(ac)
199	0.999
200	1.077
201	1.156
202	1.237
203	1.318
204	1.401

-----Class: Node-----  
Name: 7           Base Flow(cfs): 0           Init Stage(ft): 149  
Group: BASE       Length(ft): 0           Warn Stage(ft): 170  
Comment:

Stage(ft)	Area(ac)
149	0.057
150	0.115
155	0.557
160	1.064
165	1.689
170	3.575

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 8           Base Flow(cfs): 0           Init Stage(ft): 235  
Group: BASE       Length(ft): 0           Warn Stage(ft): 240  
Comment:

Stage(ft)	Area(ac)
235	0.292
236	0.391
237	0.488
238	0.697
239	1.192
240	2.442

-----Class: Node-----

Name: 9           Base Flow(cfs): 0           Init Stage(ft): 236  
Group: BASE       Length(ft): 0           Warn Stage(ft): 240  
Comment:

Stage(ft)	Area(ac)
236	1.719
237	1.886
238	2.059
239	2.236
240	3.255

-----Class: Node-----

Name: 999         Base Flow(cfs): 0           Init Stage(ft): 195  
Group: BASE       Length(ft): 0           Warn Stage(ft): 200  
Comment:

Time(hrs)	Stage(ft)
30	196
60	197
96	198

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 12      Base Flow(cfs): 0      Init Stage(ft): 205  
Group: BASE      Length(ft): 0      Warn Stage(ft): 216  
Comment:

Stage(ft)	Area(ac)
205	0.089
206	0.115
207	0.143
208	0.174
209	0.206
210	0.239
211	0.278
212	0.32
213	0.379
214	0.439
215	0.5
216	0.562

-----Class: Node-----

Name: 14      Base Flow(cfs): 0      Init Stage(ft): 230  
Group: BASE      Length(ft): 0      Warn Stage(ft): 238  
Comment:

Stage(ft)	Area(ac)
230	0.184
231	0.215
232	0.248
233	0.282
234	0.318
235	0.355
236	0.393
237	0.432
238	0.473

-----Class: Node-----

Name: 15      Base Flow(cfs): 0      - Init Stage(ft): 194  
Group: BASE      Length(ft): 0      Warn Stage(ft): 201  
Comment:

Stage(ft)	Area(ac)
194	0.366
195	0.458
196	0.615
197	0.746
198	0.886
199	1.071
200	1.236
201	1.406

LEGENDS OF CLERNONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----  
Name: 16           Base Flow(cfs): 0           Init Stage(ft): 159  
Group: BASE           Length(ft): 0           Warn Stage(ft): 169  
Comment:

Stage(ft)	Area(ac)
159	0.573
160	0.661
161	0.751
162	0.845
163	1.112
164	1.231
165	1.52
166	1.659
167	2.016
168	2.194
169	2.387

-----Class: Node-----  
Name: 18           Base Flow(cfs): 0           Init Stage(ft): 165  
Group: BASE           Length(ft): 0           Warn Stage(ft): 171  
Comment:

Stage(ft)	Area(ac)
165	1.261
166	1.466
167	1.714
168	1.975
169	2.351
170	2.705
171	3.31

-----Class: Node-----  
Name: 19           Base Flow(cfs): 0           Init Stage(ft): 178  
Group: BASE           Length(ft): 0           Warn Stage(ft): 183  
Comment:

Stage(ft)	Area(ac)
178	0.726
179	0.798
180	0.873
181	0.949
182	1.028
183	1.11



LEGENDS OF CLERNONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 20      Base Flow(cfs): 0      Init Stage(ft): 191  
Group: BASE      Length(ft): 0      Warn Stage(ft): 196  
Comment:

Stage(ft)	Area(ac)
191	0.41
192	0.492
193	0.626
194	0.787
195	0.954
196	1.156

-----Class: Node-----

Name: 21      Base Flow(cfs): 0      Init Stage(ft): 185  
Group: BASE      Length(ft): 0      Warn Stage(ft): 196  
Comment:

Stage(ft)	Area(ac)
185	0.227
186	0.275
187	0.326
188	0.379
189	0.434
190	0.492
191	0.803
192	1.115
193	1.374
194	1.642
195	1.872
196	2.138

-----Class: Node-----

Name: 22      Base Flow(cfs): 0      Init Stage(ft): 169  
Group: BASE      Length(ft): 0      Warn Stage(ft): 176  
Comment:

Stage(ft)	Area(ac)
169	0.262
170	0.338
171	0.42
172	0.505
173	0.641
174	0.811
175	1.181
176	1.581

LEGENDS OF CLERMONT

\*\*\*\*\* Input Report \*\*\*\*\*

-----Class: Node-----

Name: 23           Base Flow(cfs): 0           Init Stage(ft): 130  
Group: BASE           Length(ft): 0           Warn Stage(ft): 150

Comment:

Stage(ft)	Area(ac)
130	0.033
135	0.33
140	0.825
145	1.521
150	2.406

-----Class: Node-----

Name: 24           Base Flow(cfs): 0           Init Stage(ft): 112  
Group: BASE           Length(ft): 0           Warn Stage(ft): 119

Comment:

Stage(ft)	Area(ac)
112	1.9
113	2.1
114	2.33
115	2.82
116	3.002
117	3.504
118	3.998
119	4.31

-----Class: Node-----

Name: 2A           Base Flow(cfs): 0           Init Stage(ft): 190  
Group: BASE           Length(ft): 0           Warn Stage(ft): 198

Comment:

Stage(ft)	Area(ac)
190	0.196
191	0.229
192	0.264
193	0.3
194	0.337
195	0.375
196	0.415
197	0.456
198	0.498

**ICPR BASIN  
AND  
DEVELOPED HYDROGRAPH SUMMARY  
25 YEAR-96 HOUR STORM**

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Basin Summary - LEGENDS \*\*\*\*\*

-----

\*\*\*

Basin Name:	1	2A	2B	2C	3
Group Name:	BASE	BASE	BASE	BASE	BASE
Node Name:	1	2A	2B	2C	3
Hydrograph Type:	SB	SB	SB	SB	SB
Spec Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Comp Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Rainfall File:	SJRWND96	SJRWND96	SJRWND96	SJRWND96	SJRWND96
Rainfall Amount (in):	11.20	11.20	11.20	11.20	11.20
Storm Duration (hr):	96.00	96.00	96.00	96.00	96.00
Status:	ONSITE	ONSITE	ONSITE	ONSITE	ONSITE
Time of Conc. (min):	15.00	15.00	15.00	15.00	15.00
Lag Time (hr):	0.00	0.00	0.00	0.00	0.00
Area (acres):	7.84	8.64	18.74	14.84	23.59
Curve Number:	50.00	55.00	54.00	49.00	62.00
DCIA (%):	0.00	0.00	0.00	0.00	0.00
Time Max (hrs):	59.75	59.75	59.75	59.75	59.75
Flow Max (cfs):	17.56	22.91	48.18	31.95	75.25
Runoff Volume (in):	4.41	5.15	5.01	4.26	6.18
Runoff Volume (cf):	125474	161595	340530	229315	529004

\*\*\*

Basin Name:	4	5	6	7	8
Group Name:	BASE	BASE	BASE	BASE	BASE
Node Name:	4	5	6	7	8
Hydrograph Type:	SB	SB	SB	SB	SB
Spec Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Comp Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Rainfall File:	SJRWND96	SJRWND96	SJRWND96	SJRWND96	SJRWND96
Rainfall Amount (in):	11.20	11.20	11.20	11.20	11.20
Storm Duration (hr):	96.00	96.00	96.00	96.00	96.00
Status:	ONSITE	ONSITE	ONSITE	ONSITE	ONSITE
Time of Conc. (min):	15.00	15.00	15.00	15.00	15.00
Lag Time (hr):	0.00	0.00	0.00	0.00	0.00
Area (acres):	18.39	2.77	10.47	32.65	6.92
Curve Number:	48.00	39.00	39.00	51.00	45.00
DCIA (%):	0.00	0.00	0.00	0.00	0.00
Time Max (hrs):	59.75	59.75	59.75	59.75	59.75
Flow Max (cfs):	38.02	3.49	13.20	75.84	12.49
Runoff Volume (in):	4.11	2.75	2.75	4.56	3.65
Runoff Volume (cf):	274150	27578	104466	540164	91795

\*\*\*

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Basin Summary - LEGENDS \*\*\*\*\*

Group Name:	BASE	BASE	BASE	BASE	BASE
Node Name:	9	10	11	12	14
Hydrograph Type:	SB	SB	SB	SB	SB
Spec Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Comp Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Rainfall File:	SJRWND96	SJRWND96	SJRWND96	SJRWND96	SJRWND96
Rainfall Amount (in):	11.20	11.20	11.20	11.20	11.20
Storm Duration (hr):	96.00	96.00	96.00	96.00	96.00
Status:	ONSITE	ONSITE	ONSITE	ONSITE	ONSITE
Time of Conc. (min):	15.00	15.00	15.00	15.00	15.00
Lag Time (hr):	0.00	0.00	0.00	0.00	0.00
Area (acres):	7.81	13.60	11.52	14.39	4.45
Curve Number:	60.00	53.00	52.00	53.00	56.00
DCIA (%):	0.00	0.00	0.00	0.00	0.00
Time Max (hrs):	59.75	59.75	59.75	59.75	59.75
Flow Max (cfs):	23.74	33.86	27.71	35.82	12.16
Runoff Volume (in):	5.89	4.86	4.71	4.86	5.30
Runoff Volume (cf):	166846	239820	196788	253713	85646

\*\*\*

Basin Name:	15	16	17	18	19
Group Name:	BASE	BASE	BASE	BASE	BASE
Node Name:	15	16	17	18	19
Hydrograph Type:	SB	SB	SB	SB	SB
Spec Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Comp Time Inc (sec):	15.00	15.00	15.00	15.00	15.00
Rainfall File:	SJRWND96	SJRWND96	SJRWND96	SJRWND96	SJRWND96
Rainfall Amount (in):	11.20	11.20	11.20	11.20	11.20
Storm Duration (hr):	96.00	96.00	96.00	96.00	96.00
Status:	ONSITE	ONSITE	ONSITE	ONSITE	ONSITE
Time of Conc. (min):	15.00	15.00	15.00	15.00	15.00
Lag Time (hr):	0.00	0.00	0.00	0.00	0.00
Area (acres):	16.37	17.16	0.42	23.37	11.26
Curve Number:	51.00	56.00	39.00	54.00	51.00
DCIA (%):	0.00	0.00	0.00	0.00	0.00
Time Max (hrs):	59.75	59.75	59.75	59.75	59.75
Flow Max (cfs):	38.03	46.87	0.53	60.09	26.15
Runoff Volume (in):	4.56	5.30	2.75	5.01	4.56
Runoff Volume (cf):	270835	330209	4189	424644	186265

\*\*\*

Basin Name:	20	21	22	23	24
-------------	----	----	----	----	----

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Basin Summary - LEGENDS \*\*\*\*\*

```

-----
Hydrograph Type:      SB      SB      SB      SB      SB
NODE NAME:           20      21      22      23      24
Spec Time Inc (sec):  15.00  15.00  15.00  15.00  15.00
Comp Time Inc (sec):  15.00  15.00  15.00  15.00  15.00
Rainfall File:       SJRWMD96 SJRWMD96 SJRWMD96 SJRWMD96 SJRWMD96
Rainfall Amount (in): 11.20  11.20  11.20  11.20  11.20
Storm Duration (hr):  96.00  96.00  96.00  96.00  96.00
Status:              ONSITE  ONSITE  ONSITE  ONSITE  ONSITE
Time of Conc. (min):  15.00  15.00  15.00  15.00  15.00
Lag Time (hr):       0.00   0.00   0.00   0.00   0.00
Area (acres):        8.70   23.79  14.35  50.90  86.15
Curve Number:        51.00  57.00  48.00  50.00  48.00
DCIA (%):            0.00   0.00   0.00   0.00   0.00
  
```

```

Time Max (hrs):      59.75  59.75  59.75  59.75  59.75
Flow Max (cfs):      20.21  66.87  29.67  113.96 178.14
Runoff Volume (in):  4.56   5.45   4.11   4.41   4.11
Runoff Volume (cf):  143939 470593 213958 814515 1284497
  
```

```

***
Basin Name:          999
Group Name:          BASE
Node Name:           999
Hydrograph Type:    SB
  
```

```

Spec Time Inc (sec): 30.00
Comp Time Inc (sec): 30.00
Rainfall File:       SJRWMD96
Rainfall Amount (in): 11.20
Storm Duration (hr): 96.00
Status:              ONSITE
Time of Conc. (min): 999.00
Lag Time (hr):       0.00
Area (acres):        2.00
Curve Number:        40.00
DCIA (%):            0.00
  
```

```

Time Max (hrs):      64.00
Flow Max (cfs):      0.17
Runoff Volume (in):  2.90
Runoff Volume (cf):  21041
  
```

**ICPR NODE MAX CONDITIONS  
(STORMWATER ROUTING SUMMARY)  
25 YEAR-96 HOUR STORM**

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Maximum Conditions - LEGENDS \*\*\*\*\*

(Time units - hours)

Node Name	Group Name	Max Time Conditions	Max Stage (ft)	Warning Stage (ft)	Max Delta Stage (ft)	Max Surface Area (sf)	Max Time Inflow	Max Inflow (cfs)	Max Time Outflow	Max Outflow (cfs)
1	BASE	60.87	202.53	205.00	0.0431	21803.90	60.01	12.42	0.00	0.00
10	BASE	60.84	214.19	219.00	0.0513	48930.60	60.01	24.97	0.00	0.00
11	BASE	61.27	214.53	218.00	0.0567	27246.87	60.01	21.75	0.00	0.00
12	BASE	61.27	215.17	216.00	0.1268	22245.07	60.01	29.50	0.00	0.00
14	BASE	61.82	233.67	238.00	0.0549	13339.54	60.01	9.88	0.00	0.00
15	BASE	60.99	198.07	201.00	0.0609	39126.55	60.01	29.99	0.00	0.00
16	BASE	60.97	162.85	169.00	0.0638	46671.63	60.01	35.67	0.00	0.00
18	BASE	60.86	166.99	171.00	0.0366	74586.89	60.01	39.72	0.00	0.00
19	BASE	61.01	180.02	183.00	0.0338	38081.62	60.01	19.70	0.00	0.00
20	BASE	60.97	193.36	196.00	0.0393	29794.57	60.01	15.33	0.00	0.00
21	BASE	61.91	193.52	196.00	0.1230	65924.40	60.01	55.42	0.00	0.00
22	BASE	61.47	173.68	176.00	0.0695	32948.25	60.01	24.87	0.00	0.00
23	BASE	62.47	145.31	150.00	0.1397	68683.30	60.01	98.66	0.00	0.00
24	BASE	61.37	116.83	119.00	0.0745	148969.49	60.01	144.61	0.00	0.00
2A	BASE	61.46	195.57	198.00	0.0830	17329.01	60.01	18.53	0.00	0.00
2B	BASE	60.96	182.23	185.00	0.0382	60255.04	60.01	34.86	0.00	0.00
2C	BASE	62.55	166.66	167.00	-0.0491	54557.99	60.01	28.16	0.00	0.00
3	BASE	61.66	171.12	175.00	0.0882	54073.75	60.01	60.27	0.00	0.00
4	BASE	60.91	179.38	185.00	0.0420	44466.78	60.01	27.02	0.00	0.00
6	BASE	60.71	199.32	204.00	-0.0124	44589.67	60.01	5.63	0.00	0.00
7	BASE	60.52	155.62	170.00	0.0809	26995.99	60.01	29.56	0.00	0.00
8	BASE	60.99	237.05	240.00	0.0334	21692.22	60.01	9.83	0.00	0.00
9	BASE	95.98	238.14	240.00	0.0154	90804.09	60.01	20.74	0.00	0.00
999	BASE	95.98	198.00	200.00	1.0000	0.00	64.00	0.17	0.00	0.00



**ICPR ROUTED HYDROGRAPH  
BY BASIN  
WITH INFILTRATION INPUTED FROM "PONDS"**

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
*** Group: BASE		Node: 1						
0.000	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
1.050	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
2.019	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
3.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
4.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
5.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
6.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
7.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
8.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
9.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
10.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
11.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
12.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
13.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
14.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
15.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
16.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
17.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
18.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
19.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
20.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
21.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
22.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
23.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
24.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
25.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
26.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
27.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
28.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
29.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
30.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
31.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
32.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
33.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
34.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
35.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
36.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
37.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
38.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
39.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
40.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
41.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
42.014	200.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
43.014	200.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
44.014	200.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00

45.014 200.00 0.00 0.00 0.00 -0.00 0.00 0.00 0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
46.014	200.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
47.003	200.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
48.035	200.00	0.00	0.00	0.02	-0.03	0.00	0.00	0.00	
49.022	200.00	0.26	0.00	0.04	-0.04	0.00	0.00	0.00	
50.017	200.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
51.031	200.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
52.025	200.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00	
53.030	200.00	0.00	0.00	0.13	-0.13	0.00	0.00	0.00	
54.008	200.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
55.018	200.00	0.00	0.00	0.21	-0.22	0.00	0.00	0.00	
56.061	200.00	0.00	0.00	0.29	-0.31	0.00	0.00	0.00	
57.014	200.00	0.00	0.00	0.43	-0.44	0.00	0.00	0.00	
58.044	200.00	0.00	0.00	0.64	-0.79	0.00	0.00	0.00	
59.002	199.99	0.00	0.00	1.32	-1.84	0.00	0.00	0.00	
60.006	201.54	0.40	0.00	15.87	-3.46	0.00	0.00	0.00	
61.006	202.51	0.50	0.00	2.80	-4.71	0.00	0.00	0.00	
62.006	202.05	0.45	0.00	1.65	-4.93	0.00	0.00	0.00	
63.016	201.42	0.39	0.00	1.20	-4.28	0.00	0.00	0.00	
64.032	200.77	0.32	0.00	1.04	-3.41	0.00	0.00	0.00	
65.025	200.31	0.28	0.00	0.74	-1.82	0.00	0.00	0.00	
66.012	200.15	0.27	0.00	0.74	-0.74	0.00	0.00	0.00	
67.029	200.15	0.27	0.00	0.75	-0.73	0.00	0.00	0.00	
68.046	200.16	0.27	0.00	0.66	-0.64	0.00	0.00	0.00	
69.038	200.16	0.27	0.00	0.51	-0.55	0.00	0.00	0.00	
70.055	200.15	0.27	0.00	0.51	-0.51	0.00	0.00	0.00	
71.009	200.15	0.27	0.00	0.51	-0.49	0.00	0.00	0.00	
72.010	200.16	0.27	0.00	0.43	-0.41	0.00	0.00	0.00	
73.043	200.16	0.27	0.00	0.27	-0.31	0.00	0.00	0.00	
74.076	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
75.030	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
76.063	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
77.017	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
78.050	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
79.004	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
80.037	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
81.070	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
82.024	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
83.057	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
84.011	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
85.044	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
86.005	200.15	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
87.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
88.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
89.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
90.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	

91.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00
92.005	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
93.055	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
94.015	200.15	0.27	0.00	0.28	-0.28	0.00	0.00	0.00	
95.018	200.16	0.27	0.00	0.28	-0.25	0.00	0.00	0.00	
96.031	200.19	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	200.19	0.27	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 10

0.000	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
1.050	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
2.019	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
3.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
4.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
5.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
6.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
7.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
8.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
9.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
10.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
11.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
12.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
13.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
14.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
15.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
16.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
17.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
18.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
19.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
20.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
21.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
22.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
23.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
24.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
25.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
26.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
27.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
28.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
29.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
30.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
31.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
32.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
33.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
34.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
35.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
36.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
37.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00

38.014	210.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	0.00
39.014	210.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
40.014	210.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
41.014	210.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
42.014	210.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
43.014	210.00	0.09	0.00	0.02	-0.02	0.00	0.00	0.00	
44.014	210.00	0.09	0.00	0.04	-0.03	0.00	0.00	0.00	
45.014	210.00	0.09	0.00	0.05	-0.05	0.00	0.00	0.00	
46.014	210.00	0.09	0.00	0.06	-0.06	0.00	0.00	0.00	
47.003	210.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
48.035	210.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00	
49.022	210.00	0.09	0.00	0.13	-0.13	0.00	0.00	0.00	
50.017	210.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
51.031	210.00	0.00	0.00	0.20	-0.20	0.00	0.00	0.00	
52.025	210.00	0.00	0.00	0.24	-0.25	0.00	0.00	0.00	
53.030	210.00	0.09	0.00	0.31	-0.31	0.00	0.00	0.00	
54.008	210.00	0.00	0.00	0.38	-0.39	0.00	0.00	0.00	
55.018	210.00	0.00	0.00	0.49	-0.50	0.00	0.00	0.00	
56.061	210.00	0.00	0.00	0.65	-0.68	0.00	0.00	0.00	
57.014	210.02	0.09	0.00	0.92	-0.86	0.00	0.00	0.00	
58.044	210.18	0.11	0.00	1.35	-1.01	0.00	0.00	0.00	
59.002	210.69	0.15	0.00	2.70	-1.32	0.00	0.00	0.00	
60.006	213.33	0.83	0.00	30.23	-5.29	0.00	0.00	0.00	
61.006	214.16	1.12	0.00	5.23	-10.14	0.00	0.00	0.00	
62.006	213.68	0.97	0.00	3.07	-10.42	0.00	0.00	0.00	
63.016	213.02	0.71	0.00	2.21	-8.16	0.00	0.00	0.00	
64.032	212.35	0.49	0.00	1.92	-5.61	0.00	0.00	0.00	
65.025	211.72	0.32	0.00	1.37	-3.65	0.00	0.00	0.00	
66.012	211.23	0.22	0.00	1.37	-2.37	0.00	0.00	0.00	
67.029	210.94	0.17	0.00	1.37	-1.74	0.00	0.00	0.00	
68.046	210.76	0.16	0.00	1.22	-1.54	0.00	0.00	0.00	
69.038	210.55	0.14	0.00	0.93	-1.36	0.00	0.00	0.00	
70.055	210.34	0.12	0.00	0.93	-1.15	0.00	0.00	0.00	
71.009	210.25	0.11	0.00	0.93	-0.98	0.00	0.00	0.00	
72.010	210.24	0.11	0.00	0.79	-0.77	0.00	0.00	0.00	
73.043	210.22	0.11	0.00	0.49	-0.56	0.00	0.00	0.00	
74.076	210.19	0.11	0.00	0.49	-0.49	0.00	0.00	0.00	
75.030	210.19	0.11	0.00	0.49	-0.49	0.00	0.00	0.00	
76.063	210.19	0.11	0.00	0.49	-0.49	0.00	0.00	0.00	
77.017	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
78.050	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
79.004	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
80.037	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
81.070	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
82.024	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
83.057	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
84.011	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	



85.044	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00
86.005	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
87.005	210.19	0.11	0.00	0.50	-0.50	0.00	0.00	0.00	
88.005	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
89.005	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
90.005	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
91.005	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
92.005	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
93.055	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
94.015	210.19	0.11	0.00	0.51	-0.51	0.00	0.00	0.00	
95.018	210.21	0.11	0.00	0.51	-0.46	0.00	0.00	0.00	
96.031	210.34	0.12	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	210.34	0.12	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 11

0.000	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
1.050	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
2.019	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
3.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
4.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
5.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
6.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
7.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
8.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
9.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
10.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
11.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
12.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
13.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
14.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
15.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
16.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
17.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
18.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
19.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
20.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
21.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
22.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
23.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
24.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
25.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
26.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
27.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
28.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
29.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
30.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
31.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
34.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
35.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
36.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
37.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
38.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
39.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
40.014	211.00	0.42	0.00	0.00	0.00	0.00	0.00	0.00
41.014	211.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
42.014	211.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
43.014	211.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00
44.014	211.00	0.42	0.00	0.02	-0.02	0.00	0.00	0.00
45.014	211.00	0.42	0.00	0.03	-0.03	0.00	0.00	0.00
46.014	211.00	0.42	0.00	0.04	-0.04	0.00	0.00	0.00
47.003	211.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00
48.035	211.00	0.00	0.00	0.06	-0.07	0.00	0.00	0.00
49.022	211.00	0.42	0.00	0.09	-0.09	0.00	0.00	0.00
50.017	211.00	0.00	0.00	0.11	-0.12	0.00	0.00	0.00
51.031	211.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00
52.025	211.00	0.00	0.00	0.18	-0.19	0.00	0.00	0.00
53.030	211.00	0.42	0.00	0.24	-0.24	0.00	0.00	0.00
54.008	211.00	0.00	0.00	0.29	-0.30	0.00	0.00	0.00
55.018	211.00	0.00	0.00	0.38	-0.39	0.00	0.00	0.00
56.061	211.00	0.00	0.00	0.51	-0.54	0.00	0.00	0.00
57.014	211.00	0.00	0.00	0.73	-0.75	0.00	0.00	0.00
58.044	211.00	0.00	0.00	1.08	-1.27	0.00	0.00	0.00
59.002	211.00	0.00	0.00	2.17	-2.16	0.00	0.00	0.00
60.006	212.93	0.53	0.00	24.84	-3.10	0.00	0.00	0.00
61.006	214.52	0.62	0.00	4.33	-3.77	0.00	0.00	0.00
62.006	214.46	0.62	0.00	2.54	-4.07	0.00	0.00	0.00
63.016	214.21	0.61	0.00	1.84	-4.00	0.00	0.00	0.00
64.032	213.89	0.59	0.00	1.60	-3.89	0.00	0.00	0.00
65.025	213.54	0.57	0.00	1.14	-3.76	0.00	0.00	0.00
66.012	213.17	0.54	0.00	1.14	-3.61	0.00	0.00	0.00
67.029	212.79	0.52	0.00	1.14	-3.46	0.00	0.00	0.00
68.046	212.41	0.50	0.00	1.01	-3.32	0.00	0.00	0.00
69.038	212.01	0.48	0.00	0.78	-3.18	0.00	0.00	0.00
70.055	211.56	0.45	0.00	0.78	-3.31	0.00	0.00	0.00
71.009	211.20	0.43	0.00	0.78	-2.17	0.00	0.00	0.00
72.010	211.07	0.42	0.00	0.65	-0.62	0.00	0.00	0.00
73.043	211.07	0.42	0.00	0.41	-0.47	0.00	0.00	0.00
74.076	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00
75.030	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00
76.063	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00
77.017	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00
78.050	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00

79.004	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00
80.037	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
81.070	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00	
82.024	211.06	0.42	0.00	0.41	-0.41	0.00	0.00	0.00	
83.057	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
84.011	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
85.044	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
86.005	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
87.005	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
88.005	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
89.005	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
90.005	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
91.005	211.06	0.42	0.00	0.43	-0.43	0.00	0.00	0.00	
92.005	211.06	0.42	0.00	0.43	-0.42	0.00	0.00	0.00	
93.055	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
94.015	211.06	0.42	0.00	0.42	-0.42	0.00	0.00	0.00	
95.018	211.07	0.42	0.00	0.42	-0.38	0.00	0.00	0.00	
96.031	211.10	0.42	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	211.10	0.42	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 12

0.000	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
1.050	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
2.019	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
3.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
4.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
5.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
6.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
7.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
8.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
9.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
10.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
11.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
12.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
13.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
14.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
15.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
16.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
17.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
18.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
19.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
20.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
21.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
22.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
23.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
24.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00
25.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
28.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	205.00	0.09	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	205.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	205.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
41.014	205.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
42.014	205.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
43.014	205.00	0.09	0.00	0.02	-0.02	0.00	0.00	0.00	
44.014	205.00	0.09	0.00	0.04	-0.04	0.00	0.00	0.00	
45.014	205.00	0.09	0.00	0.05	-0.05	0.00	0.00	0.00	
46.014	205.00	0.09	0.00	0.06	-0.06	0.00	0.00	0.00	
47.003	205.00	0.00	0.00	0.07	-0.08	0.00	0.00	0.00	
48.035	205.00	0.00	0.00	0.10	-0.10	0.00	0.00	0.00	
49.022	205.00	0.09	0.00	0.14	-0.13	0.00	0.00	0.00	
50.017	205.00	0.00	0.00	0.17	-0.17	0.00	0.00	0.00	
51.031	205.00	0.00	0.00	0.21	-0.21	0.00	0.00	0.00	
52.025	205.00	0.00	0.00	0.26	-0.26	0.00	0.00	0.00	
53.030	205.00	0.09	0.00	0.33	-0.33	0.00	0.00	0.00	
54.008	205.00	0.00	0.00	0.40	-0.41	0.00	0.00	0.00	
55.018	205.00	0.00	0.00	0.51	-0.52	0.00	0.00	0.00	
56.061	205.00	0.00	0.00	0.69	-0.72	0.00	0.00	0.00	
57.014	205.02	0.09	0.00	0.97	-0.90	0.00	0.00	0.00	
58.044	205.22	0.09	0.00	1.43	-1.02	0.00	0.00	0.00	
59.002	206.01	0.12	0.00	2.86	-1.16	0.00	0.00	0.00	
60.006	212.17	0.33	0.00	31.99	-2.51	0.00	0.00	0.00	
61.006	215.16	0.51	0.00	5.53	-4.70	0.00	0.00	0.00	
62.006	215.06	0.50	0.00	3.25	-5.24	0.00	0.00	0.00	
63.016	214.81	0.49	0.00	2.34	-3.28	0.00	0.00	0.00	
64.032	214.77	0.49	0.00	2.04	-1.57	0.00	0.00	0.00	
65.025	214.83	0.49	0.00	1.45	-1.27	0.00	0.00	0.00	
66.012	214.87	0.49	0.00	1.45	-1.12	0.00	0.00	0.00	
67.029	214.94	0.50	0.00	1.45	-1.02	0.00	0.00	0.00	
68.046	215.00	0.50	0.00	1.29	-0.94	0.00	0.00	0.00	
69.038	215.04	0.50	0.00	0.99	-0.88	0.00	0.00	0.00	
70.055	215.06	0.50	0.00	0.99	-0.83	0.00	0.00	0.00	
71.009	215.09	0.51	0.00	0.99	-0.79	0.00	0.00	0.00	
72.010	215.11	0.51	0.00	0.83	-0.75	0.00	0.00	0.00	



73.043	215.10	0.51	0.00	0.52	-0.71	0.00	0.00	0.00
74.076	215.07	0.50	0.00	0.52	-0.68	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
75.030	215.05	0.50	0.00	0.52	-0.65	0.00	0.00	0.00	
76.063	215.03	0.50	0.00	0.52	-0.63	0.00	0.00	0.00	
77.017	215.01	0.50	0.00	0.53	-0.61	0.00	0.00	0.00	
78.050	215.00	0.50	0.00	0.53	-0.60	0.00	0.00	0.00	
79.004	214.99	0.50	0.00	0.53	-0.58	0.00	0.00	0.00	
80.037	214.98	0.50	0.00	0.53	-0.57	0.00	0.00	0.00	
81.070	214.97	0.50	0.00	0.53	-0.56	0.00	0.00	0.00	
82.024	214.97	0.50	0.00	0.53	-0.55	0.00	0.00	0.00	
83.057	214.97	0.50	0.00	0.53	-0.53	0.00	0.00	0.00	
84.011	214.97	0.50	0.00	0.53	-0.53	0.00	0.00	0.00	
85.044	214.97	0.50	0.00	0.53	-0.52	0.00	0.00	0.00	
86.005	214.97	0.50	0.00	0.53	-0.51	0.00	0.00	0.00	
87.005	214.98	0.50	0.00	0.53	-0.50	0.00	0.00	0.00	
88.005	214.98	0.50	0.00	0.53	-0.50	0.00	0.00	0.00	
89.005	214.99	0.50	0.00	0.54	-0.49	0.00	0.00	0.00	
90.005	215.00	0.50	0.00	0.54	-0.49	0.00	0.00	0.00	
91.005	215.00	0.50	0.00	0.54	-0.48	0.00	0.00	0.00	
92.005	215.01	0.50	0.00	0.54	-0.48	0.00	0.00	0.00	
93.055	215.03	0.50	0.00	0.54	-0.47	0.00	0.00	0.00	
94.015	215.04	0.50	0.00	0.54	-0.47	0.00	0.00	0.00	
95.018	215.05	0.50	0.00	0.54	-0.45	0.00	0.00	0.00	
96.031	215.08	0.51	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	215.08	0.51	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 14

0.000	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
1.050	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
2.019	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
3.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
4.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
5.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
6.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
7.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
8.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
9.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
10.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
11.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
12.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
13.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
14.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
15.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
16.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
17.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
18.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00
19.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
22.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	230.00	0.18	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	230.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
37.014	230.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
38.014	230.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	230.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	230.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
41.014	230.00	0.18	0.00	0.01	-0.01	0.00	0.00	0.00	
42.014	230.00	0.18	0.00	0.02	-0.02	0.00	0.00	0.00	
43.014	230.00	0.18	0.00	0.02	-0.02	0.00	0.00	0.00	
44.014	230.00	0.18	0.00	0.03	-0.03	0.00	0.00	0.00	
45.014	230.00	0.18	0.00	0.03	-0.03	0.00	0.00	0.00	
46.014	230.00	0.18	0.00	0.03	-0.03	0.00	0.00	0.00	
47.003	230.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
48.035	230.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
49.022	230.00	0.18	0.00	0.06	-0.06	0.00	0.00	0.00	
50.017	230.00	0.18	0.00	0.07	-0.07	0.00	0.00	0.00	
51.031	230.00	0.00	0.00	0.09	-0.09	0.00	0.00	0.00	
52.025	230.00	0.00	0.00	0.11	-0.11	0.00	0.00	0.00	
53.030	230.00	0.18	0.00	0.13	-0.13	0.00	0.00	0.00	
54.008	230.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
55.018	230.00	0.00	0.00	0.20	-0.20	0.00	0.00	0.00	
56.061	230.00	0.00	0.00	0.26	-0.27	0.00	0.00	0.00	
57.014	230.00	0.00	0.00	0.36	-0.37	0.00	0.00	0.00	
58.044	230.00	0.00	0.00	0.52	-0.59	0.00	0.00	0.00	
59.002	230.04	0.19	0.00	1.02	-0.74	0.00	0.00	0.00	
60.006	232.01	0.25	0.00	10.74	-0.87	0.00	0.00	0.00	
61.006	233.59	0.30	0.00	1.82	-1.11	0.00	0.00	0.00	
62.006	233.67	0.31	0.00	1.06	-1.23	0.00	0.00	0.00	
63.016	233.58	0.30	0.00	0.77	-1.22	0.00	0.00	0.00	
64.032	233.44	0.30	0.00	0.67	-1.21	0.00	0.00	0.00	
65.025	233.27	0.29	0.00	0.47	-1.19	0.00	0.00	0.00	
66.012	233.04	0.28	0.00	0.47	-1.37	0.00	0.00	0.00	

67.029	232.81	0.28	0.00	0.47	-1.06	0.00	0.00	0.00
68.046	232.71	0.27	0.00	0.42	-0.50	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
69.038	232.69	0.27	0.00	0.32	-0.39	0.00	0.00	0.00	
70.055	232.68	0.27	0.00	0.32	-0.33	0.00	0.00	0.00	
71.009	232.68	0.27	0.00	0.32	-0.30	0.00	0.00	0.00	
72.010	232.68	0.27	0.00	0.27	-0.27	0.00	0.00	0.00	
73.043	232.67	0.27	0.00	0.17	-0.25	0.00	0.00	0.00	
74.076	232.65	0.27	0.00	0.17	-0.23	0.00	0.00	0.00	
75.030	232.63	0.27	0.00	0.17	-0.22	0.00	0.00	0.00	
76.063	232.62	0.27	0.00	0.17	-0.20	0.00	0.00	0.00	
77.017	232.61	0.27	0.00	0.17	-0.20	0.00	0.00	0.00	
78.050	232.60	0.27	0.00	0.17	-0.19	0.00	0.00	0.00	
79.004	232.60	0.27	0.00	0.17	-0.18	0.00	0.00	0.00	
80.037	232.60	0.27	0.00	0.17	-0.18	0.00	0.00	0.00	
81.070	232.60	0.27	0.00	0.17	-0.17	0.00	0.00	0.00	
82.024	232.60	0.27	0.00	0.17	-0.17	0.00	0.00	0.00	
83.057	232.60	0.27	0.00	0.17	-0.16	0.00	0.00	0.00	
84.011	232.60	0.27	0.00	0.17	-0.16	0.00	0.00	0.00	
85.044	232.61	0.27	0.00	0.17	-0.15	0.00	0.00	0.00	
86.005	232.61	0.27	0.00	0.17	-0.15	0.00	0.00	0.00	
87.005	232.62	0.27	0.00	0.17	-0.15	0.00	0.00	0.00	
88.005	232.63	0.27	0.00	0.17	-0.15	0.00	0.00	0.00	
89.005	232.64	0.27	0.00	0.17	-0.14	0.00	0.00	0.00	
90.005	232.65	0.27	0.00	0.17	-0.14	0.00	0.00	0.00	
91.005	232.66	0.27	0.00	0.17	-0.14	0.00	0.00	0.00	
92.005	232.67	0.27	0.00	0.17	-0.14	0.00	0.00	0.00	
93.055	232.68	0.27	0.00	0.17	-0.14	0.00	0.00	0.00	
94.015	232.69	0.27	0.00	0.17	-0.14	0.00	0.00	0.00	
95.018	232.70	0.27	0.00	0.17	-0.13	0.00	0.00	0.00	
96.031	232.73	0.27	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	232.73	0.27	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 15

0.000	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
1.050	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
2.019	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
3.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
4.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
5.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
6.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
7.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
8.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
9.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
10.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
11.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
12.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
13.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00

14.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00
15.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
16.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	194.00	0.37	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	194.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
43.014	194.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
44.014	194.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
45.014	194.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	
46.014	194.00	0.37	0.00	0.03	-0.03	0.00	0.00	0.00	
47.003	194.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
48.035	194.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
49.022	194.00	0.37	0.00	0.10	-0.10	0.00	0.00	0.00	
50.017	194.00	0.00	0.00	0.14	-0.14	0.00	0.00	0.00	
51.031	194.00	0.00	0.00	0.18	-0.18	0.00	0.00	0.00	
52.025	194.00	0.00	0.00	0.23	-0.23	0.00	0.00	0.00	
53.030	194.00	0.37	0.00	0.30	-0.30	0.00	0.00	0.00	
54.008	194.00	0.00	0.00	0.37	-0.38	0.00	0.00	0.00	
55.018	194.00	0.00	0.00	0.49	-0.50	0.00	0.00	0.00	
56.061	194.00	0.00	0.00	0.67	-0.70	0.00	0.00	0.00	
57.014	194.00	0.00	0.00	0.96	-0.99	0.00	0.00	0.00	
58.044	193.99	0.00	0.00	1.44	-1.68	0.00	0.00	0.00	
59.002	194.02	0.37	0.00	2.93	-2.54	0.00	0.00	0.00	
60.006	196.52	0.68	0.00	34.22	-4.25	0.00	0.00	0.00	



61.006	198.07	0.90	0.00	6.00	-6.39	0.00	0.00	0.00
62.006	197.88	0.87	0.00	3.53	-7.10	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	Inflow					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
63.016	197.56	0.82	0.00	2.56	-5.39	0.00	0.00	0.00	
64.032	197.40	0.80	0.00	2.22	-2.55	0.00	0.00	0.00	
65.025	197.41	0.80	0.00	1.58	-1.14	0.00	0.00	0.00	
66.012	197.47	0.81	0.00	1.59	-0.92	0.00	0.00	0.00	
67.029	197.54	0.82	0.00	1.59	-0.81	0.00	0.00	0.00	
68.046	197.61	0.83	0.00	1.41	-0.74	0.00	0.00	0.00	
69.038	197.67	0.84	0.00	1.08	-0.68	0.00	0.00	0.00	
70.055	197.71	0.85	0.00	1.08	-0.64	0.00	0.00	0.00	
71.009	197.75	0.85	0.00	1.08	-0.61	0.00	0.00	0.00	
72.010	197.79	0.86	0.00	0.91	-0.57	0.00	0.00	0.00	
73.043	197.81	0.86	0.00	0.57	-0.54	0.00	0.00	0.00	
74.076	197.81	0.86	0.00	0.57	-0.51	0.00	0.00	0.00	
75.030	197.82	0.86	0.00	0.57	-0.49	0.00	0.00	0.00	
76.063	197.83	0.86	0.00	0.57	-0.47	0.00	0.00	0.00	
77.017	197.84	0.86	0.00	0.58	-0.46	0.00	0.00	0.00	
78.050	197.85	0.87	0.00	0.58	-0.44	0.00	0.00	0.00	
79.004	197.86	0.87	0.00	0.58	-0.43	0.00	0.00	0.00	
80.037	197.88	0.87	0.00	0.58	-0.42	0.00	0.00	0.00	
81.070	197.90	0.87	0.00	0.58	-0.42	0.00	0.00	0.00	
82.024	197.91	0.87	0.00	0.58	-0.41	0.00	0.00	0.00	
83.057	197.93	0.88	0.00	0.58	-0.40	0.00	0.00	0.00	
84.011	197.94	0.88	0.00	0.58	-0.39	0.00	0.00	0.00	
85.044	197.96	0.88	0.00	0.58	-0.39	0.00	0.00	0.00	
86.005	197.98	0.88	0.00	0.58	-0.38	0.00	0.00	0.00	
87.005	198.00	0.89	0.00	0.59	-0.38	0.00	0.00	0.00	
88.005	198.02	0.89	0.00	0.59	-0.37	0.00	0.00	0.00	
89.005	198.04	0.89	0.00	0.59	-0.37	0.00	0.00	0.00	
90.005	198.06	0.90	0.00	0.59	-0.37	0.00	0.00	0.00	
91.005	198.08	0.90	0.00	0.59	-0.36	0.00	0.00	0.00	
92.005	198.10	0.90	0.00	0.59	-0.36	0.00	0.00	0.00	
93.055	198.12	0.91	0.00	0.59	-0.36	0.00	0.00	0.00	
94.015	198.14	0.91	0.00	0.59	-0.36	0.00	0.00	0.00	
95.018	198.17	0.92	0.00	0.59	-0.35	0.00	0.00	0.00	
96.031	198.19	0.92	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	198.19	0.92	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 16

0.000	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
1.050	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
2.019	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
3.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
4.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
5.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
6.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
7.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00

8.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00
9.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
10.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	159.00	0.57	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	159.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
37.014	159.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
38.014	159.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	159.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
40.014	159.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
41.014	159.00	0.57	0.00	0.05	-0.05	0.00	0.00	0.00	
42.014	159.00	0.57	0.00	0.07	-0.07	0.00	0.00	0.00	
43.014	159.00	0.57	0.00	0.09	-0.09	0.00	0.00	0.00	
44.014	159.00	0.57	0.00	0.10	-0.10	0.00	0.00	0.00	
45.014	159.00	0.57	0.00	0.12	-0.12	0.00	0.00	0.00	
46.014	159.00	0.57	0.00	0.13	-0.13	0.00	0.00	0.00	
47.003	159.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	
48.035	159.00	0.00	0.00	0.18	-0.19	0.00	0.00	0.00	
49.022	159.00	0.57	0.00	0.24	-0.24	0.00	0.00	0.00	
50.017	159.00	0.57	0.00	0.28	-0.29	0.00	0.00	0.00	
51.031	159.00	0.00	0.00	0.34	-0.35	0.00	0.00	0.00	
52.025	159.00	0.00	0.00	0.41	-0.42	0.00	0.00	0.00	
53.030	159.00	0.57	0.00	0.51	-0.51	0.00	0.00	0.00	
54.008	159.00	0.00	0.00	0.60	-0.62	0.00	0.00	0.00	

55.018	159.00	0.00	0.00	0.76	-0.78	0.00	0.00	0.00
56.061	159.00	0.00	0.00	1.00	-1.05	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	{<-----Inflow----->}					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
57.014	159.00	0.00	0.00	1.39	-1.43	0.00	0.00	0.00	
58.044	158.99	0.00	0.00	2.00	-2.34	0.00	0.00	0.00	
59.002	159.00	0.00	0.00	3.92	-3.90	0.00	0.00	0.00	
60.006	161.23	0.77	0.00	41.42	-5.76	0.00	0.00	0.00	
61.006	162.85	1.07	0.00	7.03	-7.90	0.00	0.00	0.00	
62.006	162.62	1.01	0.00	4.10	-8.86	0.00	0.00	0.00	
63.016	162.19	0.90	0.00	2.95	-8.02	0.00	0.00	0.00	
64.032	161.71	0.82	0.00	2.56	-7.23	0.00	0.00	0.00	
65.025	161.22	0.77	0.00	1.82	-6.75	0.00	0.00	0.00	
66.012	160.70	0.72	0.00	1.82	-6.35	0.00	0.00	0.00	
67.029	160.18	0.68	0.00	1.83	-5.94	0.00	0.00	0.00	
68.046	159.67	0.63	0.00	1.62	-5.46	0.00	0.00	0.00	
69.038	159.26	0.60	0.00	1.24	-3.44	0.00	0.00	0.00	
70.055	159.10	0.58	0.00	1.24	-1.44	0.00	0.00	0.00	
71.009	159.09	0.58	0.00	1.24	-1.19	0.00	0.00	0.00	
72.010	159.10	0.58	0.00	1.04	-0.99	0.00	0.00	0.00	
73.043	159.09	0.58	0.00	0.65	-0.75	0.00	0.00	0.00	
74.076	159.09	0.58	0.00	0.65	-0.65	0.00	0.00	0.00	
75.030	159.09	0.58	0.00	0.65	-0.65	0.00	0.00	0.00	
76.063	159.09	0.58	0.00	0.65	-0.65	0.00	0.00	0.00	
77.017	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
78.050	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
79.004	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
80.037	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
81.070	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
82.024	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
83.057	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
84.011	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
85.044	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
86.005	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
87.005	159.09	0.58	0.00	0.66	-0.66	0.00	0.00	0.00	
88.005	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
89.005	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
90.005	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
91.005	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
92.005	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
93.055	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
94.015	159.09	0.58	0.00	0.67	-0.67	0.00	0.00	0.00	
95.018	159.09	0.58	0.00	0.67	-0.60	0.00	0.00	0.00	
96.031	159.12	0.58	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	159.12	0.58	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 18  
 0.000 165.00 1.26 0.00 0.00 0.00 0.00 0.00 0.00  
 1.050 165.00 1.26 0.00 0.00 0.00 0.00 0.00 0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	'<-----Inflow----->'					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
4.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	165.00	1.26	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
41.014	165.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	
42.014	165.00	1.26	0.00	0.04	-0.04	0.00	0.00	0.00	
43.014	165.00	1.26	0.00	0.07	-0.06	0.00	0.00	0.00	
44.014	165.00	1.26	0.00	0.09	-0.09	0.00	0.00	0.00	
45.014	165.00	1.26	0.00	0.11	-0.11	0.00	0.00	0.00	
46.014	165.00	1.26	0.00	0.13	-0.13	0.00	0.00	0.00	
47.003	165.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	
48.035	165.00	0.00	0.00	0.19	-0.19	0.00	0.00	0.00	



49.022	165.00	1.26	0.00	0.26	-0.25	0.00	0.00	0.00
50.017	165.00	1.26	0.00	0.31	-0.31	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
51.031	165.00	0.00	0.00	0.38	-0.38	0.00	0.00	0.00	
52.025	165.00	0.00	0.00	0.46	-0.47	0.00	0.00	0.00	
53.030	165.00	1.26	0.00	0.59	-0.59	0.00	0.00	0.00	
54.008	165.00	0.00	0.00	0.70	-0.72	0.00	0.00	0.00	
55.018	165.00	0.00	0.00	0.90	-0.92	0.00	0.00	0.00	
56.061	165.00	0.00	0.00	1.20	-1.26	0.00	0.00	0.00	
57.014	165.00	0.00	0.00	1.68	-1.73	0.00	0.00	0.00	
58.044	165.00	0.00	0.00	2.46	-3.03	0.00	0.00	0.00	
59.002	164.99	0.00	0.00	4.88	-8.15	0.00	0.00	0.00	
60.006	166.12	1.50	0.00	53.46	-13.76	0.00	0.00	0.00	
61.006	166.97	1.71	0.00	9.18	-15.88	0.00	0.00	0.00	
62.006	166.53	1.60	0.00	5.38	-16.35	0.00	0.00	0.00	
63.016	165.92	1.45	0.00	3.88	-14.93	0.00	0.00	0.00	
64.032	165.41	1.34	0.00	3.37	-9.30	0.00	0.00	0.00	
65.025	165.19	1.30	0.00	2.39	-3.51	0.00	0.00	0.00	
66.012	165.16	1.29	0.00	2.40	-2.40	0.00	0.00	0.00	
67.029	165.16	1.29	0.00	2.41	-2.34	0.00	0.00	0.00	
68.046	165.17	1.30	0.00	2.13	-2.07	0.00	0.00	0.00	
69.038	165.16	1.29	0.00	1.63	-1.76	0.00	0.00	0.00	
70.055	165.16	1.29	0.00	1.63	-1.63	0.00	0.00	0.00	
71.009	165.16	1.29	0.00	1.63	-1.57	0.00	0.00	0.00	
72.010	165.17	1.29	0.00	1.37	-1.31	0.00	0.00	0.00	
73.043	165.16	1.29	0.00	0.86	-0.98	0.00	0.00	0.00	
74.076	165.16	1.29	0.00	0.86	-0.86	0.00	0.00	0.00	
75.030	165.16	1.29	0.00	0.86	-0.86	0.00	0.00	0.00	
76.063	165.16	1.29	0.00	0.86	-0.86	0.00	0.00	0.00	
77.017	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
78.050	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
79.004	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
80.037	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
81.070	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
82.024	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
83.057	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
84.011	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
85.044	165.16	1.29	0.00	0.87	-0.87	0.00	0.00	0.00	
86.005	165.16	1.29	0.00	0.88	-0.88	0.00	0.00	0.00	
87.005	165.16	1.29	0.00	0.88	-0.88	0.00	0.00	0.00	
88.005	165.16	1.29	0.00	0.88	-0.88	0.00	0.00	0.00	
89.005	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
90.005	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
91.005	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
92.005	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
93.055	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
94.015	165.16	1.29	0.00	0.89	-0.89	0.00	0.00	0.00	
95.018	165.16	1.29	0.00	0.88	-0.80	0.00	0.00	0.00	



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)	
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)			
*** Group: BASE		Node: 19								
0.000	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
1.050	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
2.019	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
4.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	178.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	178.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	
43.014	178.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	0.00	

44.014	178.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00
45.014	178.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	{<-----Inflow----->}					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
46.014	178.00	0.73	0.00	0.02	-0.02	0.00	0.00	0.00	
47.003	178.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
48.035	178.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
49.022	178.00	0.73	0.00	0.07	-0.07	0.00	0.00	0.00	
50.017	178.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00	
51.031	178.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
52.025	178.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
53.030	178.00	0.73	0.00	0.21	-0.21	0.00	0.00	0.00	
54.008	178.00	0.00	0.00	0.26	-0.26	0.00	0.00	0.00	
55.018	178.00	0.00	0.00	0.34	-0.34	0.00	0.00	0.00	
56.061	178.00	0.00	0.00	0.46	-0.48	0.00	0.00	0.00	
57.014	178.00	0.00	0.00	0.66	-0.68	0.00	0.00	0.00	
58.044	178.00	0.00	0.00	0.99	-1.19	0.00	0.00	0.00	
59.002	178.00	0.00	0.00	2.01	-2.56	0.00	0.00	0.00	
60.006	179.05	0.80	0.00	23.54	-3.84	0.00	0.00	0.00	
61.006	180.02	0.87	0.00	4.13	-4.21	0.00	0.00	0.00	
62.006	179.92	0.87	0.00	2.43	-4.37	0.00	0.00	0.00	
63.016	179.70	0.85	0.00	1.76	-4.31	0.00	0.00	0.00	
64.032	179.44	0.83	0.00	1.53	-4.22	0.00	0.00	0.00	
65.025	179.15	0.81	0.00	1.09	-4.11	0.00	0.00	0.00	
66.012	178.85	0.79	0.00	1.09	-4.00	0.00	0.00	0.00	
67.029	178.54	0.77	0.00	1.09	-3.87	0.00	0.00	0.00	
68.046	178.27	0.75	0.00	0.97	-3.07	0.00	0.00	0.00	
69.038	178.11	0.73	0.00	0.74	-1.56	0.00	0.00	0.00	
70.055	178.07	0.73	0.00	0.74	-0.74	0.00	0.00	0.00	
71.009	178.07	0.73	0.00	0.75	-0.72	0.00	0.00	0.00	
72.010	178.07	0.73	0.00	0.63	-0.60	0.00	0.00	0.00	
73.043	178.07	0.73	0.00	0.39	-0.45	0.00	0.00	0.00	
74.076	178.07	0.73	0.00	0.39	-0.39	0.00	0.00	0.00	
75.030	178.07	0.73	0.00	0.39	-0.39	0.00	0.00	0.00	
76.063	178.06	0.73	0.00	0.39	-0.39	0.00	0.00	0.00	
77.017	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
78.050	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
79.004	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
80.037	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
81.070	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
82.024	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
83.057	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
84.011	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
85.044	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
86.005	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
87.005	178.07	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
88.005	178.06	0.73	0.00	0.40	-0.40	0.00	0.00	0.00	
89.005	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	
90.005	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	

91.005	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00
92.005	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
93.055	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	
94.015	178.07	0.73	0.00	0.41	-0.41	0.00	0.00	0.00	
95.018	178.07	0.73	0.00	0.41	-0.37	0.00	0.00	0.00	
96.031	178.08	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	178.08	0.73	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 20

0.000	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
1.050	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
2.019	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
3.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
4.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
5.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
6.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
7.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
8.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
9.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
10.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
11.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
12.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
13.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
14.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
15.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
16.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
17.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
18.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
19.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
20.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
21.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
22.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
23.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
24.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
25.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
26.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
27.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
28.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
29.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
30.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
31.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
32.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
33.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
34.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
35.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
36.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
37.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00



38.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00
39.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
40.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	191.00	0.41	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	191.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
43.014	191.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
44.014	191.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
45.014	191.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
46.014	191.00	0.41	0.00	0.02	-0.02	0.00	0.00	0.00	
47.003	191.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00	
48.035	191.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
49.022	191.00	0.41	0.00	0.06	-0.06	0.00	0.00	0.00	
50.017	191.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
51.031	191.00	0.00	0.00	0.10	-0.10	0.00	0.00	0.00	
52.025	191.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
53.030	191.00	0.41	0.00	0.16	-0.16	0.00	0.00	0.00	
54.008	191.00	0.00	0.00	0.20	-0.20	0.00	0.00	0.00	
55.018	191.00	0.00	0.00	0.26	-0.27	0.00	0.00	0.00	
56.061	191.00	0.00	0.00	0.35	-0.37	0.00	0.00	0.00	
57.014	191.00	0.00	0.00	0.51	-0.53	0.00	0.00	0.00	
58.044	191.00	0.00	0.00	0.76	-0.91	0.00	0.00	0.00	
59.002	191.00	0.00	0.00	1.56	-1.81	0.00	0.00	0.00	
60.006	192.36	0.54	0.00	18.19	-2.86	0.00	0.00	0.00	
61.006	193.36	0.68	0.00	3.19	-3.68	0.00	0.00	0.00	
62.006	193.20	0.66	0.00	1.88	-4.02	0.00	0.00	0.00	
63.016	192.95	0.62	0.00	1.36	-3.02	0.00	0.00	0.00	
64.032	192.82	0.60	0.00	1.18	-1.37	0.00	0.00	0.00	
65.025	192.83	0.60	0.00	0.84	-0.56	0.00	0.00	0.00	
66.012	192.88	0.61	0.00	0.84	-0.45	0.00	0.00	0.00	
67.029	192.93	0.62	0.00	0.85	-0.40	0.00	0.00	0.00	
68.046	192.99	0.62	0.00	0.75	-0.36	0.00	0.00	0.00	
69.038	193.03	0.63	0.00	0.57	-0.33	0.00	0.00	0.00	
70.055	193.06	0.64	0.00	0.58	-0.31	0.00	0.00	0.00	
71.009	193.10	0.64	0.00	0.58	-0.30	0.00	0.00	0.00	
72.010	193.13	0.65	0.00	0.48	-0.28	0.00	0.00	0.00	
73.043	193.14	0.65	0.00	0.30	-0.27	0.00	0.00	0.00	
74.076	193.15	0.65	0.00	0.30	-0.25	0.00	0.00	0.00	
75.030	193.16	0.65	0.00	0.30	-0.24	0.00	0.00	0.00	
76.063	193.17	0.65	0.00	0.30	-0.23	0.00	0.00	0.00	
77.017	193.18	0.65	0.00	0.31	-0.23	0.00	0.00	0.00	
78.050	193.19	0.66	0.00	0.31	-0.22	0.00	0.00	0.00	
79.004	193.20	0.66	0.00	0.31	-0.21	0.00	0.00	0.00	
80.037	193.21	0.66	0.00	0.31	-0.21	0.00	0.00	0.00	
81.070	193.22	0.66	0.00	0.31	-0.21	0.00	0.00	0.00	
82.024	193.24	0.66	0.00	0.31	-0.20	0.00	0.00	0.00	
83.057	193.25	0.67	0.00	0.31	-0.20	0.00	0.00	0.00	
84.011	193.26	0.67	0.00	0.31	-0.20	0.00	0.00	0.00	

85.044	193.28	0.67	0.00	0.31	-0.19	0.00	0.00	0.00
86.005	193.29	0.67	0.00	0.31	-0.19	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
87.005	193.31	0.68	0.00	0.31	-0.19	0.00	0.00	0.00	
88.005	193.32	0.68	0.00	0.31	-0.19	0.00	0.00	0.00	
89.005	193.34	0.68	0.00	0.31	-0.18	0.00	0.00	0.00	
90.005	193.35	0.68	0.00	0.32	-0.18	0.00	0.00	0.00	
91.005	193.37	0.69	0.00	0.32	-0.18	0.00	0.00	0.00	
92.005	193.39	0.69	0.00	0.32	-0.18	0.00	0.00	0.00	
93.055	193.40	0.69	0.00	0.31	-0.18	0.00	0.00	0.00	
94.015	193.42	0.69	0.00	0.32	-0.18	0.00	0.00	0.00	
95.018	193.44	0.70	0.00	0.31	-0.17	0.00	0.00	0.00	
96.031	193.46	0.70	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	193.46	0.70	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 21

0.000	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
1.050	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
2.019	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
3.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
4.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
5.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
6.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
7.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
8.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
9.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
10.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
11.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
12.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
13.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
14.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
15.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
16.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
17.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
18.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
19.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
20.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
21.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
22.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
23.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
24.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
25.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
26.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
27.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
28.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
29.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
30.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00
31.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
34.014	185.00	0.23	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	185.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
36.014	185.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
37.014	185.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00	
38.014	185.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	
39.014	185.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00	
40.014	185.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
41.014	185.00	0.23	0.00	0.10	-0.10	0.00	0.00	0.00	
42.014	185.00	0.23	0.00	0.12	-0.12	0.00	0.00	0.00	
43.014	185.00	0.23	0.00	0.15	-0.15	0.00	0.00	0.00	
44.014	185.00	0.23	0.00	0.17	-0.17	0.00	0.00	0.00	
45.014	185.00	0.23	0.00	0.19	-0.19	0.00	0.00	0.00	
46.014	185.00	0.23	0.00	0.21	-0.21	0.00	0.00	0.00	
47.003	185.00	0.00	0.00	0.23	-0.24	0.00	0.00	0.00	
48.035	185.00	0.00	0.00	0.28	-0.29	0.00	0.00	0.00	
49.022	185.00	0.23	0.00	0.37	-0.37	0.00	0.00	0.00	
50.017	185.00	0.23	0.00	0.43	-0.44	0.00	0.00	0.00	
51.031	185.00	0.00	0.00	0.52	-0.52	0.00	0.00	0.00	
52.025	185.00	0.00	0.00	0.61	-0.63	0.00	0.00	0.00	
53.030	185.00	0.23	0.00	0.77	-0.76	0.00	0.00	0.00	
54.008	185.00	0.00	0.00	0.90	-0.92	0.00	0.00	0.00	
55.018	185.00	0.00	0.00	1.13	-1.15	0.00	0.00	0.00	
56.061	185.00	0.00	0.00	1.47	-1.52	0.00	0.00	0.00	
57.014	185.04	0.23	0.00	2.04	-1.73	0.00	0.00	0.00	
58.044	185.29	0.24	0.00	2.91	-1.81	0.00	0.00	0.00	
59.002	186.00	0.28	0.00	5.67	-2.04	0.00	0.00	0.00	
60.006	191.37	0.92	0.00	58.90	-3.51	0.00	0.00	0.00	
61.006	193.41	1.48	0.00	9.93	-5.49	0.00	0.00	0.00	
62.006	193.52	1.51	0.00	5.79	-6.23	0.00	0.00	0.00	
63.016	193.45	1.49	0.00	4.17	-6.24	0.00	0.00	0.00	
64.032	193.32	1.46	0.00	3.62	-6.17	0.00	0.00	0.00	
65.025	193.14	1.41	0.00	2.56	-6.06	0.00	0.00	0.00	
66.012	192.94	1.36	0.00	2.57	-5.94	0.00	0.00	0.00	
67.029	192.73	1.31	0.00	2.57	-5.79	0.00	0.00	0.00	
68.046	192.52	1.25	0.00	2.27	-5.64	0.00	0.00	0.00	
69.038	192.28	1.19	0.00	1.74	-5.47	0.00	0.00	0.00	
70.055	192.02	1.12	0.00	1.74	-5.26	0.00	0.00	0.00	
71.009	191.78	1.05	0.00	1.74	-4.71	0.00	0.00	0.00	
72.010	191.59	0.99	0.00	1.46	-3.16	0.00	0.00	0.00	
73.043	191.48	0.95	0.00	0.92	-1.80	0.00	0.00	0.00	
74.076	191.42	0.93	0.00	0.91	-1.39	0.00	0.00	0.00	
75.030	191.38	0.92	0.00	0.91	-1.19	0.00	0.00	0.00	
76.063	191.36	0.92	0.00	0.92	-1.06	0.00	0.00	0.00	
77.017	191.36	0.91	0.00	0.93	-0.97	0.00	0.00	0.00	
78.050	191.36	0.91	0.00	0.93	-0.90	0.00	0.00	0.00	

79.004	191.36	0.92	0.00	0.93	-0.84	0.00	0.00	0.00
80.037	191.37	0.92	0.00	0.93	-0.80	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
81.070	191.38	0.92	0.00	0.92	-0.76	0.00	0.00	0.00
82.024	191.40	0.93	0.00	0.93	-0.73	0.00	0.00	0.00
83.057	191.42	0.93	0.00	0.93	-0.70	0.00	0.00	0.00
84.011	191.44	0.94	0.00	0.93	-0.68	0.00	0.00	0.00
85.044	191.46	0.95	0.00	0.93	-0.66	0.00	0.00	0.00
86.005	191.49	0.95	0.00	0.93	-0.64	0.00	0.00	0.00
87.005	191.51	0.96	0.00	0.93	-0.62	0.00	0.00	0.00
88.005	191.54	0.97	0.00	0.94	-0.61	0.00	0.00	0.00
89.005	191.57	0.98	0.00	0.94	-0.59	0.00	0.00	0.00
90.005	191.60	0.99	0.00	0.94	-0.58	0.00	0.00	0.00
91.005	191.63	1.00	0.00	0.95	-0.57	0.00	0.00	0.00
92.005	191.66	1.01	0.00	0.94	-0.56	0.00	0.00	0.00
93.055	191.69	1.02	0.00	0.94	-0.55	0.00	0.00	0.00
94.015	191.72	1.03	0.00	0.94	-0.55	0.00	0.00	0.00
95.018	191.76	1.04	0.00	0.94	-0.53	0.00	0.00	0.00
96.031	191.80	1.05	0.00	0.00	0.00	0.00	0.00	0.00
96.064	191.80	1.05	0.00	0.00	0.00	0.00	0.00	0.00

\*\*\* Group: BASE Node: 22

0.000	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
1.050	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
2.019	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
3.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
4.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
5.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
6.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
7.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
8.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
9.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
10.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
11.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
12.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
13.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
14.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
15.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
16.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
17.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
18.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
19.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
20.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
21.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
22.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
23.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
24.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
25.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
28.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
29.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
30.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
31.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
32.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
33.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
34.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
35.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
36.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
37.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
38.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
39.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
40.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
41.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
42.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
43.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
44.014	169.00	0.26	0.00	0.00	0.00	0.00	0.00	0.00
45.014	169.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
46.014	169.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
47.003	169.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
48.035	169.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00
49.022	169.00	0.00	0.00	0.03	-0.03	0.00	0.00	0.00
50.017	169.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00
51.031	169.00	0.00	0.00	0.08	-0.08	0.00	0.00	0.00
52.025	169.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00
53.030	169.00	0.00	0.00	0.17	-0.17	0.00	0.00	0.00
54.008	169.00	0.00	0.00	0.22	-0.23	0.00	0.00	0.00
55.018	169.00	0.00	0.00	0.31	-0.32	0.00	0.00	0.00
56.061	169.00	0.00	0.00	0.44	-0.46	0.00	0.00	0.00
57.014	169.00	0.00	0.00	0.65	-0.68	0.00	0.00	0.00
58.044	168.99	0.00	0.00	1.01	-1.18	0.00	0.00	0.00
59.002	169.07	0.27	0.00	2.14	-1.52	0.00	0.00	0.00
60.006	171.90	0.50	0.00	27.07	-2.21	0.00	0.00	0.00
61.006	173.65	0.75	0.00	4.86	-3.62	0.00	0.00	0.00
62.006	173.64	0.75	0.00	2.88	-4.34	0.00	0.00	0.00
63.016	173.43	0.71	0.00	2.09	-4.20	0.00	0.00	0.00
64.032	173.17	0.67	0.00	1.82	-3.97	0.00	0.00	0.00
65.025	172.88	0.62	0.00	1.30	-3.72	0.00	0.00	0.00
66.012	172.57	0.58	0.00	1.30	-3.47	0.00	0.00	0.00
67.029	172.27	0.54	0.00	1.31	-3.22	0.00	0.00	0.00
68.046	171.97	0.50	0.00	1.16	-3.00	0.00	0.00	0.00
69.038	171.63	0.47	0.00	0.89	-3.04	0.00	0.00	0.00
70.055	171.32	0.45	0.00	0.89	-2.10	0.00	0.00	0.00
71.009	171.21	0.44	0.00	0.89	-0.94	0.00	0.00	0.00
72.010	171.21	0.44	0.00	0.75	-0.73	0.00	0.00	0.00

73.043	171.20	0.44	0.00	0.47	-0.61	0.00	0.00	0.00
74.076	171.18	0.43	0.00	0.47	-0.54	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
75.030	171.17	0.43	0.00	0.47	-0.49	0.00	0.00	0.00	
76.063	171.17	0.43	0.00	0.47	-0.46	0.00	0.00	0.00	
77.017	171.17	0.43	0.00	0.48	-0.43	0.00	0.00	0.00	
78.050	171.18	0.44	0.00	0.48	-0.41	0.00	0.00	0.00	
79.004	171.20	0.44	0.00	0.48	-0.40	0.00	0.00	0.00	
80.037	171.21	0.44	0.00	0.48	-0.38	0.00	0.00	0.00	
81.070	171.23	0.44	0.00	0.48	-0.37	0.00	0.00	0.00	
82.024	171.25	0.44	0.00	0.48	-0.36	0.00	0.00	0.00	
83.057	171.28	0.44	0.00	0.48	-0.36	0.00	0.00	0.00	
84.011	171.30	0.45	0.00	0.48	-0.35	0.00	0.00	0.00	
85.044	171.33	0.45	0.00	0.48	-0.35	0.00	0.00	0.00	
86.005	171.35	0.45	0.00	0.48	-0.34	0.00	0.00	0.00	
87.005	171.38	0.45	0.00	0.49	-0.34	0.00	0.00	0.00	
88.005	171.40	0.45	0.00	0.49	-0.33	0.00	0.00	0.00	
89.005	171.43	0.46	0.00	0.49	-0.33	0.00	0.00	0.00	
90.005	171.46	0.46	0.00	0.49	-0.33	0.00	0.00	0.00	
91.005	171.49	0.46	0.00	0.49	-0.33	0.00	0.00	0.00	
92.005	171.52	0.46	0.00	0.49	-0.32	0.00	0.00	0.00	
93.055	171.55	0.47	0.00	0.49	-0.32	0.00	0.00	0.00	
94.015	171.58	0.47	0.00	0.49	-0.32	0.00	0.00	0.00	
95.018	171.61	0.47	0.00	0.49	-0.31	0.00	0.00	0.00	
96.031	171.66	0.48	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	171.66	0.48	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 23

0.000	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
1.050	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
2.019	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
3.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
4.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
5.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
6.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
7.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
8.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
9.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
10.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
11.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
12.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
13.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
14.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
15.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
16.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
17.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
18.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
19.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00

20.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00
21.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	<-----Inflow----->					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
22.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
23.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
24.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
25.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
26.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
27.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
28.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
29.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
30.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
31.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
32.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
33.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
34.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
35.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
36.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
37.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
38.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
39.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
40.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
41.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
42.014	130.00	0.03	0.00	0.00	0.00	0.00	0.00	0.00
43.014	130.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
44.014	130.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
45.014	130.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00
46.014	130.00	0.00	0.00	0.05	-0.05	0.00	0.00	0.00
47.003	130.00	0.00	0.00	0.09	-0.10	0.00	0.00	0.00
48.035	130.00	0.00	0.00	0.15	-0.16	0.00	0.00	0.00
49.022	130.04	0.04	0.00	0.25	-0.21	0.00	0.00	0.00
50.017	130.17	0.04	0.00	0.34	-0.26	0.00	0.00	0.00
51.031	130.36	0.05	0.00	0.47	-0.33	0.00	0.00	0.00
52.025	130.58	0.07	0.00	0.60	-0.41	0.00	0.00	0.00
53.030	130.85	0.08	0.00	0.82	-0.52	0.00	0.00	0.00
54.008	131.16	0.10	0.00	1.03	-0.63	0.00	0.00	0.00
55.018	131.53	0.12	0.00	1.38	-0.77	0.00	0.00	0.00
56.061	132.01	0.15	0.00	1.90	-0.95	0.00	0.00	0.00
57.014	132.60	0.19	0.00	2.76	-1.16	0.00	0.00	0.00
58.044	133.44	0.24	0.00	4.18	-1.46	0.00	0.00	0.00
59.002	134.77	0.32	0.00	8.60	-1.89	0.00	0.00	0.00
60.006	141.57	1.04	0.00	102.99	-4.67	0.00	0.00	0.00
61.006	145.03	1.53	0.00	18.20	-8.77	0.00	0.00	0.00
62.006	145.28	1.57	0.00	10.74	-10.54	0.00	0.00	0.00
63.016	145.21	1.56	0.00	7.77	-10.62	0.00	0.00	0.00
64.032	145.03	1.53	0.00	6.77	-10.47	0.00	0.00	0.00
65.025	144.78	1.49	0.00	4.81	-10.24	0.00	0.00	0.00
66.012	144.49	1.45	0.00	4.83	-9.98	0.00	0.00	0.00

67.029	144.20	1.41	0.00	4.85	-9.70	0.00	0.00	0.00
68.046	143.90	1.37	0.00	4.30	-9.42	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
69.038	143.56	1.32	0.00	3.30	-9.12	0.00	0.00	0.00	
70.055	143.19	1.27	0.00	3.30	-8.78	0.00	0.00	0.00	
71.009	142.86	1.22	0.00	3.31	-8.46	0.00	0.00	0.00	
72.010	142.50	1.17	0.00	2.78	-8.12	0.00	0.00	0.00	
73.043	142.07	1.11	0.00	1.75	-7.74	0.00	0.00	0.00	
74.076	141.62	1.05	0.00	1.74	-7.31	0.00	0.00	0.00	
75.030	141.20	0.99	0.00	1.74	-6.92	0.00	0.00	0.00	
76.063	140.76	0.93	0.00	1.75	-6.49	0.00	0.00	0.00	
77.017	140.37	0.88	0.00	1.76	-6.11	0.00	0.00	0.00	
78.050	139.95	0.82	0.00	1.77	-5.72	0.00	0.00	0.00	
79.004	139.58	0.78	0.00	1.77	-5.42	0.00	0.00	0.00	
80.037	139.18	0.74	0.00	1.77	-5.15	0.00	0.00	0.00	
81.070	138.80	0.71	0.00	1.77	-4.89	0.00	0.00	0.00	
82.024	138.46	0.67	0.00	1.77	-4.65	0.00	0.00	0.00	
83.057	138.10	0.64	0.00	1.77	-4.40	0.00	0.00	0.00	
84.011	137.78	0.61	0.00	1.78	-4.18	0.00	0.00	0.00	
85.044	137.45	0.57	0.00	1.78	-3.95	0.00	0.00	0.00	
86.005	137.15	0.54	0.00	1.78	-3.75	0.00	0.00	0.00	
87.005	136.86	0.51	0.00	1.79	-3.54	0.00	0.00	0.00	
88.005	136.59	0.49	0.00	1.80	-3.35	0.00	0.00	0.00	
89.005	136.34	0.46	0.00	1.81	-3.17	0.00	0.00	0.00	
90.005	136.11	0.44	0.00	1.81	-3.00	0.00	0.00	0.00	
91.005	135.89	0.42	0.00	1.82	-2.85	0.00	0.00	0.00	
92.005	135.70	0.40	0.00	1.82	-2.71	0.00	0.00	0.00	
93.055	135.52	0.38	0.00	1.81	-2.57	0.00	0.00	0.00	
94.015	135.37	0.37	0.00	1.81	-2.46	0.00	0.00	0.00	
95.018	135.23	0.35	0.00	1.81	-2.32	0.00	0.00	0.00	
96.031	135.31	0.36	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	135.31	0.36	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 24

0.000	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
1.050	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
2.019	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
3.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
4.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
5.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
6.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
7.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
8.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
9.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
10.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
11.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
12.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
13.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00



14.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00
15.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
16.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	112.00	1.90	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	112.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
46.014	112.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
47.003	112.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00	
48.035	112.00	0.00	0.00	0.06	-0.07	0.00	0.00	0.00	
49.022	112.00	0.00	0.00	0.18	-0.18	0.00	0.00	0.00	
50.017	112.00	0.00	0.00	0.31	-0.32	0.00	0.00	0.00	
51.031	112.00	0.00	0.00	0.49	-0.50	0.00	0.00	0.00	
52.025	112.00	0.00	0.00	0.70	-0.72	0.00	0.00	0.00	
53.030	112.00	0.00	0.00	1.01	-1.01	0.00	0.00	0.00	
54.008	112.00	0.00	0.00	1.32	-1.37	0.00	0.00	0.00	
55.018	112.00	0.00	0.00	1.84	-1.89	0.00	0.00	0.00	
56.061	112.00	0.00	0.00	2.62	-2.78	0.00	0.00	0.00	
57.014	112.00	0.00	0.00	3.92	-4.07	0.00	0.00	0.00	
58.044	111.99	0.00	0.00	6.08	-7.23	0.00	0.00	0.00	
59.002	112.00	1.90	0.00	12.83	-12.03	0.00	0.00	0.00	
60.006	114.76	2.70	0.00	162.49	-17.96	0.00	0.00	0.00	

61.006	116.81	3.41	0.00	29.18	-23.78	0.00	0.00	0.00
62.006	116.76	3.38	0.00	17.29	-26.36	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
63.016	116.59	3.30	0.00	12.53	-17.49	0.00	0.00	0.00	
64.032	116.58	3.29	0.00	10.93	-6.87	0.00	0.00	0.00	
65.025	116.67	3.34	0.00	7.78	-4.25	0.00	0.00	0.00	
66.012	116.77	3.39	0.00	7.81	-3.45	0.00	0.00	0.00	
67.029	116.88	3.44	0.00	7.85	-3.04	0.00	0.00	0.00	
68.046	116.99	3.50	0.00	6.97	-2.76	0.00	0.00	0.00	
69.038	117.07	3.54	0.00	5.34	-2.55	0.00	0.00	0.00	
70.055	117.14	3.57	0.00	5.35	-2.39	0.00	0.00	0.00	
71.009	117.21	3.61	0.00	5.37	-2.27	0.00	0.00	0.00	
72.010	117.27	3.64	0.00	4.52	-2.15	0.00	0.00	0.00	
73.043	117.31	3.65	0.00	2.84	-2.03	0.00	0.00	0.00	
74.076	117.32	3.66	0.00	2.82	-1.93	0.00	0.00	0.00	
75.030	117.34	3.67	0.00	2.83	-1.86	0.00	0.00	0.00	
76.063	117.37	3.69	0.00	2.85	-1.79	0.00	0.00	0.00	
77.017	117.39	3.70	0.00	2.87	-1.74	0.00	0.00	0.00	
78.050	117.42	3.71	0.00	2.88	-1.69	0.00	0.00	0.00	
79.004	117.44	3.72	0.00	2.88	-1.65	0.00	0.00	0.00	
80.037	117.47	3.74	0.00	2.88	-1.61	0.00	0.00	0.00	
81.070	117.50	3.75	0.00	2.87	-1.58	0.00	0.00	0.00	
82.024	117.53	3.77	0.00	2.88	-1.55	0.00	0.00	0.00	
83.057	117.56	3.78	0.00	2.89	-1.52	0.00	0.00	0.00	
84.011	117.59	3.79	0.00	2.89	-1.50	0.00	0.00	0.00	
85.044	117.62	3.81	0.00	2.90	-1.47	0.00	0.00	0.00	
86.005	117.65	3.83	0.00	2.91	-1.45	0.00	0.00	0.00	
87.005	117.68	3.84	0.00	2.91	-1.43	0.00	0.00	0.00	
88.005	117.71	3.86	0.00	2.93	-1.42	0.00	0.00	0.00	
89.005	117.75	3.87	0.00	2.95	-1.40	0.00	0.00	0.00	
90.005	117.78	3.89	0.00	2.96	-1.39	0.00	0.00	0.00	
91.005	117.81	3.91	0.00	2.96	-1.37	0.00	0.00	0.00	
92.005	117.85	3.92	0.00	2.96	-1.36	0.00	0.00	0.00	
93.055	117.88	3.94	0.00	2.95	-1.35	0.00	0.00	0.00	
94.015	117.91	3.96	0.00	2.96	-1.34	0.00	0.00	0.00	
95.018	117.95	3.97	0.00	2.95	-1.30	0.00	0.00	0.00	
96.031	117.99	3.99	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	117.99	3.99	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 2A

0.000	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
1.050	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
2.019	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
3.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
4.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
5.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
6.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00
7.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
10.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	190.00	0.20	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	190.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
38.014	190.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	190.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	190.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00	
41.014	190.00	0.20	0.00	0.02	-0.02	0.00	0.00	0.00	
42.014	190.00	0.20	0.00	0.03	-0.03	0.00	0.00	0.00	
43.014	190.00	0.20	0.00	0.03	-0.03	0.00	0.00	0.00	
44.014	190.00	0.20	0.00	0.04	-0.04	0.00	0.00	0.00	
45.014	190.00	0.20	0.00	0.05	-0.05	0.00	0.00	0.00	
46.014	190.00	0.20	0.00	0.05	-0.06	0.00	0.00	0.00	
47.003	190.00	0.00	0.00	0.06	-0.07	0.00	0.00	0.00	
48.035	190.00	0.00	0.00	0.08	-0.08	0.00	0.00	0.00	
49.022	190.00	0.20	0.00	0.11	-0.11	0.00	0.00	0.00	
50.017	190.00	0.20	0.00	0.13	-0.13	0.00	0.00	0.00	
51.031	190.00	0.00	0.00	0.16	-0.16	0.00	0.00	0.00	
52.025	190.00	0.00	0.00	0.19	-0.19	0.00	0.00	0.00	
53.030	190.00	0.20	0.00	0.24	-0.24	0.00	0.00	0.00	
54.008	190.00	0.00	0.00	0.28	-0.29	0.00	0.00	0.00	

55.018	190.00	0.00	0.00	0.36	-0.37	0.00	0.00	0.00
56.061	190.00	0.00	0.00	0.47	-0.50	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
57.014	190.00	0.00	0.00	0.66	-0.68	0.00	0.00	0.00	
58.044	189.99	0.00	0.00	0.96	-1.10	0.00	0.00	0.00	
59.002	190.07	0.20	0.00	1.89	-1.39	0.00	0.00	0.00	
60.006	193.24	0.31	0.00	20.31	-1.78	0.00	0.00	0.00	
61.006	195.52	0.40	0.00	3.47	-2.49	0.00	0.00	0.00	
62.006	195.50	0.40	0.00	2.03	-3.23	0.00	0.00	0.00	
63.016	195.24	0.38	0.00	1.46	-2.64	0.00	0.00	0.00	
64.032	195.10	0.38	0.00	1.27	-1.42	0.00	0.00	0.00	
65.025	195.06	0.38	0.00	0.90	-1.11	0.00	0.00	0.00	
66.012	195.04	0.38	0.00	0.90	-0.95	0.00	0.00	0.00	
67.029	195.04	0.38	0.00	0.90	-0.85	0.00	0.00	0.00	
68.046	195.05	0.38	0.00	0.80	-0.78	0.00	0.00	0.00	
69.038	195.04	0.38	0.00	0.61	-0.71	0.00	0.00	0.00	
70.055	195.02	0.38	0.00	0.61	-0.66	0.00	0.00	0.00	
71.009	195.01	0.38	0.00	0.61	-0.63	0.00	0.00	0.00	
72.010	195.00	0.38	0.00	0.52	-0.59	0.00	0.00	0.00	
73.043	194.97	0.37	0.00	0.32	-0.55	0.00	0.00	0.00	
74.076	194.92	0.37	0.00	0.32	-0.51	0.00	0.00	0.00	
75.030	194.88	0.37	0.00	0.32	-0.49	0.00	0.00	0.00	
76.063	194.85	0.37	0.00	0.32	-0.47	0.00	0.00	0.00	
77.017	194.82	0.37	0.00	0.33	-0.45	0.00	0.00	0.00	
78.050	194.79	0.37	0.00	0.33	-0.43	0.00	0.00	0.00	
79.004	194.77	0.37	0.00	0.33	-0.42	0.00	0.00	0.00	
80.037	194.75	0.37	0.00	0.33	-0.41	0.00	0.00	0.00	
81.070	194.73	0.36	0.00	0.33	-0.40	0.00	0.00	0.00	
82.024	194.72	0.36	0.00	0.33	-0.39	0.00	0.00	0.00	
83.057	194.70	0.36	0.00	0.33	-0.38	0.00	0.00	0.00	
84.011	194.69	0.36	0.00	0.33	-0.37	0.00	0.00	0.00	
85.044	194.68	0.36	0.00	0.33	-0.36	0.00	0.00	0.00	
86.005	194.68	0.36	0.00	0.33	-0.36	0.00	0.00	0.00	
87.005	194.67	0.36	0.00	0.33	-0.35	0.00	0.00	0.00	
88.005	194.67	0.36	0.00	0.33	-0.35	0.00	0.00	0.00	
89.005	194.66	0.36	0.00	0.33	-0.34	0.00	0.00	0.00	
90.005	194.66	0.36	0.00	0.33	-0.34	0.00	0.00	0.00	
91.005	194.66	0.36	0.00	0.33	-0.33	0.00	0.00	0.00	
92.005	194.66	0.36	0.00	0.33	-0.33	0.00	0.00	0.00	
93.055	194.66	0.36	0.00	0.33	-0.33	0.00	0.00	0.00	
94.015	194.67	0.36	0.00	0.33	-0.32	0.00	0.00	0.00	
95.018	194.67	0.36	0.00	0.33	-0.31	0.00	0.00	0.00	
96.031	194.70	0.36	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	194.70	0.36	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 2B  
 0.000 180.00 1.11 0.00 0.00 0.00 0.00 0.00 0.00  
 1.050 180.00 1.11 0.00 0.00 0.00 0.00 0.00 0.00





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
4.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
5.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
6.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
7.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
8.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
9.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
10.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	180.00	1.11	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	180.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
39.014	180.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
40.014	180.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
41.014	180.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
42.014	180.00	1.11	0.00	0.03	-0.03	0.00	0.00	0.00	
43.014	180.00	1.11	0.00	0.05	-0.05	0.00	0.00	0.00	
44.014	180.00	1.11	0.00	0.07	-0.07	0.00	0.00	0.00	
45.014	180.00	1.11	0.00	0.08	-0.09	0.00	0.00	0.00	
46.014	180.00	1.11	0.00	0.10	-0.10	0.00	0.00	0.00	
47.003	180.00	0.00	0.00	0.12	-0.12	0.00	0.00	0.00	
48.035	180.00	0.00	0.00	0.15	-0.16	0.00	0.00	0.00	

49.022	180.00	1.11	0.00	0.20	-0.20	0.00	0.00	0.00
50.017	180.00	1.11	0.00	0.25	-0.25	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
51.031	180.00	0.00	0.00	0.31	-0.31	0.00	0.00	0.00	
52.025	180.00	0.00	0.00	0.37	-0.38	0.00	0.00	0.00	
53.030	180.00	1.11	0.00	0.47	-0.47	0.00	0.00	0.00	
54.008	180.00	0.00	0.00	0.56	-0.58	0.00	0.00	0.00	
55.018	180.00	0.00	0.00	0.72	-0.74	0.00	0.00	0.00	
56.061	180.00	0.00	0.00	0.96	-1.01	0.00	0.00	0.00	
57.014	180.00	0.00	0.00	1.35	-1.39	0.00	0.00	0.00	
58.044	180.00	0.00	0.00	1.97	-2.37	0.00	0.00	0.00	
59.002	179.99	0.00	0.00	3.91	-5.21	0.00	0.00	0.00	
60.006	181.19	1.26	0.00	42.87	-8.02	0.00	0.00	0.00	
61.006	182.23	1.38	0.00	7.36	-8.92	0.00	0.00	0.00	
62.006	182.03	1.36	0.00	4.31	-9.27	0.00	0.00	0.00	
63.016	181.69	1.32	0.00	3.11	-9.04	0.00	0.00	0.00	
64.032	181.31	1.27	0.00	2.70	-8.73	0.00	0.00	0.00	
65.025	180.89	1.22	0.00	1.92	-8.38	0.00	0.00	0.00	
66.012	180.48	1.17	0.00	1.92	-7.61	0.00	0.00	0.00	
67.029	180.18	1.13	0.00	1.93	-4.37	0.00	0.00	0.00	
68.046	180.10	1.12	0.00	1.71	-1.66	0.00	0.00	0.00	
69.038	180.10	1.12	0.00	1.31	-1.41	0.00	0.00	0.00	
70.055	180.09	1.12	0.00	1.31	-1.31	0.00	0.00	0.00	
71.009	180.09	1.12	0.00	1.31	-1.26	0.00	0.00	0.00	
72.010	180.10	1.12	0.00	1.10	-1.05	0.00	0.00	0.00	
73.043	180.10	1.12	0.00	0.69	-0.79	0.00	0.00	0.00	
74.076	180.09	1.12	0.00	0.69	-0.69	0.00	0.00	0.00	
75.030	180.09	1.12	0.00	0.69	-0.69	0.00	0.00	0.00	
76.063	180.09	1.12	0.00	0.69	-0.69	0.00	0.00	0.00	
77.017	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
78.050	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
79.004	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
80.037	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
81.070	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
82.024	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
83.057	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
84.011	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
85.044	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
86.005	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
87.005	180.09	1.12	0.00	0.70	-0.70	0.00	0.00	0.00	
88.005	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
89.005	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
90.005	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
91.005	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
92.005	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
93.055	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
94.015	180.09	1.12	0.00	0.71	-0.71	0.00	0.00	0.00	
95.018	180.09	1.12	0.00	0.71	-0.64	0.00	0.00	0.00	



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
*** Group: BASE		Node: 2C						
0.000	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
1.050	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
2.019	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
3.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
4.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
5.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
6.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
7.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
8.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
9.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
10.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
11.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
12.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
13.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
14.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
15.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
16.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
17.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
18.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
19.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
20.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
21.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
22.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
23.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
24.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
25.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
26.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
27.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
28.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
29.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
30.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
31.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
32.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
33.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
34.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
35.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
36.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
37.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
38.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
39.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
40.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
41.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
42.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00
43.014	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00

44.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
45.014	163.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	{<-----Inflow----->}					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
46.014	163.00	0.61	0.00	0.00	-0.00	0.00	0.00	0.00	
47.003	163.00	0.61	0.00	0.01	-0.00	0.00	0.00	0.00	
48.035	163.00	0.61	0.00	0.03	-0.00	0.00	0.00	0.00	
49.022	163.01	0.61	0.00	0.05	-0.01	0.00	0.00	0.00	
50.017	163.02	0.61	0.00	0.08	-0.01	0.00	0.00	0.00	
51.031	163.03	0.61	0.00	0.11	-0.02	0.00	0.00	0.00	
52.025	163.04	0.61	0.00	0.15	-0.03	0.00	0.00	0.00	
53.030	163.06	0.61	0.00	0.21	-0.04	0.00	0.00	0.00	
54.008	163.09	0.61	0.00	0.26	-0.05	0.00	0.00	0.00	
55.018	163.12	0.62	0.00	0.36	-0.07	0.00	0.00	0.00	
56.061	163.17	0.62	0.00	0.50	-0.10	0.00	0.00	0.00	
57.014	163.23	0.63	0.00	0.74	-0.13	0.00	0.00	0.00	
58.044	163.33	0.63	0.00	1.13	-0.18	0.00	0.00	0.00	
59.002	163.52	0.65	0.00	2.36	-0.26	0.00	0.00	0.00	
60.006	165.26	0.85	0.00	29.01	-0.86	0.00	0.00	0.00	
61.006	166.52	1.21	0.00	5.17	-1.89	0.00	0.00	0.00	
62.006	166.65	1.25	0.00	3.05	-2.51	0.00	0.00	0.00	
63.016	166.65	1.25	0.00	2.21	-2.64	0.00	0.00	0.00	
64.032	166.62	1.24	0.00	1.93	-2.60	0.00	0.00	0.00	
65.025	166.56	1.22	0.00	1.37	-2.50	0.00	0.00	0.00	
66.012	166.48	1.20	0.00	1.38	-2.39	0.00	0.00	0.00	
67.029	166.41	1.18	0.00	1.38	-2.33	0.00	0.00	0.00	
68.046	166.34	1.16	0.00	1.23	-2.27	0.00	0.00	0.00	
69.038	166.26	1.13	0.00	0.94	-2.21	0.00	0.00	0.00	
70.055	166.17	1.10	0.00	0.94	-2.13	0.00	0.00	0.00	
71.009	166.08	1.08	0.00	0.94	-2.07	0.00	0.00	0.00	
72.010	165.99	1.05	0.00	0.79	-2.00	0.00	0.00	0.00	
73.043	165.88	1.02	0.00	0.50	-1.92	0.00	0.00	0.00	
74.076	165.77	0.99	0.00	0.50	-1.84	0.00	0.00	0.00	
75.030	165.66	0.96	0.00	0.50	-1.76	0.00	0.00	0.00	
76.063	165.55	0.93	0.00	0.50	-1.68	0.00	0.00	0.00	
77.017	165.45	0.90	0.00	0.50	-1.61	0.00	0.00	0.00	
78.050	165.35	0.88	0.00	0.51	-1.54	0.00	0.00	0.00	
79.004	165.26	0.85	0.00	0.51	-1.48	0.00	0.00	0.00	
80.037	165.17	0.83	0.00	0.51	-1.41	0.00	0.00	0.00	
81.070	165.07	0.80	0.00	0.50	-1.35	0.00	0.00	0.00	
82.024	164.99	0.78	0.00	0.51	-1.30	0.00	0.00	0.00	
83.057	164.91	0.77	0.00	0.51	-1.25	0.00	0.00	0.00	
84.011	164.83	0.77	0.00	0.51	-1.20	0.00	0.00	0.00	
85.044	164.76	0.76	0.00	0.51	-1.16	0.00	0.00	0.00	
86.005	164.69	0.75	0.00	0.51	-1.12	0.00	0.00	0.00	
87.005	164.63	0.75	0.00	0.51	-1.08	0.00	0.00	0.00	
88.005	164.57	0.74	0.00	0.51	-1.04	0.00	0.00	0.00	
89.005	164.51	0.74	0.00	0.52	-1.01	0.00	0.00	0.00	
90.005	164.46	0.73	0.00	0.52	-0.98	0.00	0.00	0.00	



91.005	164.41	0.73	0.00	0.52	-0.95	0.00	0.00	0.00
92.005	164.36	0.72	0.00	0.52	-0.95	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
93.055	164.00	0.69	0.00	0.52	-5.84	0.00	0.00	0.00	
94.015	163.29	0.63	0.00	0.52	-6.86	0.00	0.00	0.00	
95.018	162.98	0.00	0.00	0.52	-1.80	0.00	0.00	0.00	
96.031	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	163.00	0.61	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 3

0.000	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
1.050	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
2.019	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
3.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
4.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
5.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
6.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
7.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
8.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
9.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
10.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
11.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
12.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
13.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
14.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
15.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
16.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
17.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
18.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
19.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
20.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
21.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
22.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
23.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
24.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
25.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
26.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
27.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
28.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
29.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
30.014	165.00	0.59	0.00	0.00	0.00	0.00	0.00	0.00
31.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
32.014	165.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00
33.014	165.00	0.00	0.00	0.01	-0.01	0.00	0.00	0.00
34.014	165.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00
35.014	165.00	0.60	0.00	0.07	-0.07	0.00	0.00	0.00
36.014	165.00	0.60	0.00	0.10	-0.10	0.00	0.00	0.00
37.014	165.00	0.60	0.00	0.13	-0.13	0.00	0.00	0.00

38.014	165.00	0.60	0.00	0.15	-0.15	0.00	0.00	0.00
39.014	165.00	0.60	0.00	0.18	-0.18	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
40.014	165.00	0.60	0.00	0.21	-0.21	0.00	0.00	0.00	
41.014	165.00	0.60	0.00	0.24	-0.24	0.00	0.00	0.00	
42.014	165.00	0.60	0.00	0.27	-0.27	0.00	0.00	0.00	
43.014	165.00	0.60	0.00	0.29	-0.29	0.00	0.00	0.00	
44.014	165.00	0.60	0.00	0.31	-0.31	0.00	0.00	0.00	
45.014	165.00	0.60	0.00	0.33	-0.33	0.00	0.00	0.00	
46.014	165.00	0.60	0.00	0.35	-0.35	0.00	0.00	0.00	
47.003	165.00	0.00	0.00	0.37	-0.38	0.00	0.00	0.00	
48.035	165.00	0.00	0.00	0.44	-0.46	0.00	0.00	0.00	
49.022	165.00	0.60	0.00	0.56	-0.55	0.00	0.00	0.00	
50.017	165.00	0.60	0.00	0.64	-0.65	0.00	0.00	0.00	
51.031	165.00	0.60	0.00	0.75	-0.75	0.00	0.00	0.00	
52.025	165.00	0.00	0.00	0.86	-0.88	0.00	0.00	0.00	
53.030	165.00	0.60	0.00	1.05	-1.04	0.00	0.00	0.00	
54.008	165.00	0.00	0.00	1.20	-1.23	0.00	0.00	0.00	
55.018	165.00	0.00	0.00	1.48	-1.50	0.00	0.00	0.00	
56.061	165.00	0.00	0.00	1.88	-1.96	0.00	0.00	0.00	
57.014	165.00	0.00	0.00	2.55	-2.60	0.00	0.00	0.00	
58.044	165.00	0.60	0.00	3.57	-3.46	0.00	0.00	0.00	
59.002	165.19	0.61	0.00	6.78	-3.95	0.00	0.00	0.00	
60.006	168.62	0.95	0.00	65.35	-5.10	0.00	0.00	0.00	
61.006	171.04	1.23	0.00	10.73	-7.14	0.00	0.00	0.00	
62.006	171.10	1.24	0.00	6.21	-8.08	0.00	0.00	0.00	
63.016	170.96	1.22	0.00	4.46	-6.50	0.00	0.00	0.00	
64.032	170.92	1.22	0.00	3.86	-3.18	0.00	0.00	0.00	
65.025	170.99	1.22	0.00	2.73	-1.31	0.00	0.00	0.00	
66.012	171.09	1.24	0.00	2.73	-1.06	0.00	0.00	0.00	
67.029	171.21	1.25	0.00	2.73	-0.94	0.00	0.00	0.00	
68.046	171.32	1.27	0.00	2.41	-0.86	0.00	0.00	0.00	
69.038	171.40	1.28	0.00	1.85	-0.80	0.00	0.00	0.00	
70.055	171.47	1.29	0.00	1.84	-0.75	0.00	0.00	0.00	
71.009	171.54	1.30	0.00	1.84	-0.72	0.00	0.00	0.00	
72.010	171.61	1.30	0.00	1.55	-0.68	0.00	0.00	0.00	
73.043	171.64	1.31	0.00	0.97	-0.64	0.00	0.00	0.00	
74.076	171.67	1.31	0.00	0.97	-0.61	0.00	0.00	0.00	
75.030	171.69	1.31	0.00	0.97	-0.59	0.00	0.00	0.00	
76.063	171.71	1.32	0.00	0.97	-0.57	0.00	0.00	0.00	
77.017	171.74	1.32	0.00	0.98	-0.55	0.00	0.00	0.00	
78.050	171.77	1.32	0.00	0.98	-0.54	0.00	0.00	0.00	
79.004	171.79	1.33	0.00	0.98	-0.53	0.00	0.00	0.00	
80.037	171.82	1.33	0.00	0.98	-0.52	0.00	0.00	0.00	
81.070	171.85	1.34	0.00	0.97	-0.51	0.00	0.00	0.00	
82.024	171.88	1.34	0.00	0.97	-0.50	0.00	0.00	0.00	
83.057	171.91	1.34	0.00	0.98	-0.49	0.00	0.00	0.00	
84.011	171.94	1.35	0.00	0.98	-0.48	0.00	0.00	0.00	

85.044	171.97	1.35	0.00	0.98	-0.48	0.00	0.00	0.00
86.005	172.00	1.35	0.00	0.98	-0.47	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
87.005	172.03	1.36	0.00	0.98	-0.47	0.00	0.00	0.00
88.005	172.06	1.36	0.00	0.98	-0.46	0.00	0.00	0.00
89.005	172.09	1.37	0.00	0.99	-0.46	0.00	0.00	0.00
90.005	172.13	1.37	0.00	0.99	-0.45	0.00	0.00	0.00
91.005	172.16	1.38	0.00	0.99	-0.45	0.00	0.00	0.00
92.005	172.19	1.38	0.00	0.99	-0.45	0.00	0.00	0.00
93.055	172.23	1.38	0.00	0.99	-0.44	0.00	0.00	0.00
94.015	172.26	1.39	0.00	0.99	-0.44	0.00	0.00	0.00
95.018	172.29	1.39	0.00	0.98	-0.43	0.00	0.00	0.00
96.031	172.33	1.40	0.00	0.00	0.00	0.00	0.00	0.00
96.064	172.33	1.40	0.00	0.00	0.00	0.00	0.00	0.00

\*\*\* Group: BASE Node: 4

0.000	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
1.050	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
2.019	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
3.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
4.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
5.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
6.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
7.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
8.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
9.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
10.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
11.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
12.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
13.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
14.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
15.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
16.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
17.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
18.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
19.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
20.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
21.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
22.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
23.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
24.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
25.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
26.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
27.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
28.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
29.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
30.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00
31.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
34.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	177.00	0.73	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	177.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
46.014	177.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
47.003	177.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
48.035	177.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
49.022	177.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
50.017	177.00	0.00	0.00	0.07	-0.07	0.00	0.00	0.00	
51.031	177.00	0.00	0.00	0.10	-0.11	0.00	0.00	0.00	
52.025	177.00	0.00	0.00	0.15	-0.15	0.00	0.00	0.00	
53.030	177.00	0.00	0.00	0.21	-0.22	0.00	0.00	0.00	
54.008	177.00	0.00	0.00	0.28	-0.29	0.00	0.00	0.00	
55.018	177.00	0.00	0.00	0.39	-0.40	0.00	0.00	0.00	
56.061	177.00	0.00	0.00	0.56	-0.59	0.00	0.00	0.00	
57.014	177.00	0.00	0.00	0.84	-0.87	0.00	0.00	0.00	
58.044	177.00	0.00	0.00	1.30	-1.63	0.00	0.00	0.00	
59.002	176.99	0.00	0.00	2.74	-4.47	0.00	0.00	0.00	
60.006	178.32	0.89	0.00	34.68	-7.68	0.00	0.00	0.00	
61.006	179.37	1.02	0.00	6.23	-9.02	0.00	0.00	0.00	
62.006	179.01	0.97	0.00	3.69	-9.42	0.00	0.00	0.00	
63.016	178.49	0.91	0.00	2.68	-8.84	0.00	0.00	0.00	
64.032	177.91	0.84	0.00	2.33	-8.11	0.00	0.00	0.00	
65.025	177.42	0.78	0.00	1.66	-5.39	0.00	0.00	0.00	
66.012	177.19	0.75	0.00	1.67	-2.37	0.00	0.00	0.00	
67.029	177.15	0.75	0.00	1.68	-1.63	0.00	0.00	0.00	
68.046	177.16	0.75	0.00	1.49	-1.45	0.00	0.00	0.00	
69.038	177.16	0.75	0.00	1.14	-1.23	0.00	0.00	0.00	
70.055	177.15	0.75	0.00	1.14	-1.14	0.00	0.00	0.00	
71.009	177.15	0.75	0.00	1.15	-1.10	0.00	0.00	0.00	
72.010	177.16	0.75	0.00	0.96	-0.92	0.00	0.00	0.00	
73.043	177.16	0.75	0.00	0.61	-0.69	0.00	0.00	0.00	
74.076	177.15	0.75	0.00	0.60	-0.60	0.00	0.00	0.00	
75.030	177.15	0.75	0.00	0.60	-0.60	0.00	0.00	0.00	
76.063	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
77.017	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	
78.050	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00	



79.004	177.15	0.75	0.00	0.62	-0.61	0.00	0.00	0.00
80.037	177.15	0.75	0.00	0.61	-0.61	0.00	0.00	0.00





LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
28.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
46.014	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
47.003	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
48.035	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
49.022	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
50.017	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
51.031	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
52.025	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
53.030	199.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00	
54.008	199.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
55.018	199.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
56.061	199.00	0.00	0.00	0.01	-0.03	0.00	0.00	0.00	
57.014	199.00	0.00	0.00	0.08	-0.09	0.00	0.00	0.00	
58.044	199.00	0.00	0.00	0.21	-0.41	0.00	0.00	0.00	
59.002	198.99	0.00	0.00	0.62	-3.58	0.00	0.00	0.00	
60.006	199.16	1.01	0.00	12.86	-7.24	0.00	0.00	0.00	
61.006	199.29	1.02	0.00	2.57	-4.89	0.00	0.00	0.00	
62.006	199.19	1.01	0.00	1.56	-1.71	0.00	0.00	0.00	
63.016	199.18	1.01	0.00	1.14	-1.21	0.00	0.00	0.00	
64.032	199.18	1.01	0.00	1.01	-0.97	0.00	0.00	0.00	
65.025	199.18	1.01	0.00	0.72	-0.79	0.00	0.00	0.00	
66.012	199.17	1.01	0.00	0.73	-0.73	0.00	0.00	0.00	
67.029	199.17	1.01	0.00	0.73	-0.71	0.00	0.00	0.00	
68.046	199.18	1.01	0.00	0.65	-0.64	0.00	0.00	0.00	
69.038	199.17	1.01	0.00	0.50	-0.54	0.00	0.00	0.00	
70.055	199.17	1.01	0.00	0.51	-0.50	0.00	0.00	0.00	
71.009	199.17	1.01	0.00	0.51	-0.49	0.00	0.00	0.00	
72.010	199.18	1.01	0.00	0.43	-0.41	0.00	0.00	0.00	

73.043	199.17	1.01	0.00	0.27	-0.31	0.00	0.00	0.00
74.076	199.17	1.01	0.00	0.27	-0.27	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)	
75.030	199.17	1.01	0.00	0.27	-0.27	0.00	0.00	0.00
76.063	199.17	1.01	0.00	0.27	-0.27	0.00	0.00	0.00
77.017	199.17	1.01	0.00	0.27	-0.27	0.00	0.00	0.00
78.050	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
79.004	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
80.037	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
81.070	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
82.024	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
83.057	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
84.011	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
85.044	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
86.005	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
87.005	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
88.005	199.17	1.01	0.00	0.28	-0.28	0.00	0.00	0.00
89.005	199.17	1.01	0.00	0.29	-0.29	0.00	0.00	0.00
90.005	199.17	1.01	0.00	0.29	-0.29	0.00	0.00	0.00
91.005	199.17	1.01	0.00	0.29	-0.29	0.00	0.00	0.00
92.005	199.17	1.01	0.00	0.29	-0.29	0.00	0.00	0.00
93.055	199.17	1.01	0.00	0.29	-0.29	0.00	0.00	0.00
94.015	199.17	1.01	0.00	0.29	-0.29	0.00	0.00	0.00
95.018	199.17	1.01	0.00	0.29	-0.26	0.00	0.00	0.00
96.031	199.18	1.01	0.00	0.00	0.00	0.00	0.00	0.00
96.064	199.18	1.01	0.00	0.00	0.00	0.00	0.00	0.00

\*\*\* Group: BASE Node: 7

0.000	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
1.050	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
2.019	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
3.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
4.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
5.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
6.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
7.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
8.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
9.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
10.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
11.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
12.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
13.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
14.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
15.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
16.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
17.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
18.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
19.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00

20.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00
21.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
22.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	149.00	0.06	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	149.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
44.014	149.00	0.00	0.00	0.01	-0.02	0.00	0.00	0.00	
45.014	149.02	0.06	0.00	0.04	-0.02	0.00	0.00	0.00	
46.014	149.03	0.06	0.00	0.07	-0.07	0.00	0.00	0.00	
47.003	149.05	0.06	0.00	0.10	-0.07	0.00	0.00	0.00	
48.035	149.06	0.06	0.00	0.14	-0.14	0.00	0.00	0.00	
49.022	149.10	0.06	0.00	0.21	-0.15	0.00	0.00	0.00	
50.017	149.14	0.07	0.00	0.27	-0.27	0.00	0.00	0.00	
51.031	149.19	0.07	0.00	0.36	-0.28	0.00	0.00	0.00	
52.025	149.22	0.07	0.00	0.45	-0.46	0.00	0.00	0.00	
53.030	149.30	0.07	0.00	0.60	-0.47	0.00	0.00	0.00	
54.008	149.35	0.08	0.00	0.74	-0.76	0.00	0.00	0.00	
55.018	149.45	0.08	0.00	0.98	-0.77	0.00	0.00	0.00	
56.061	149.51	0.09	0.00	1.33	-1.36	0.00	0.00	0.00	
57.014	149.73	0.10	0.00	1.92	-1.39	0.00	0.00	0.00	
58.044	149.71	0.10	0.00	2.87	-3.28	0.00	0.00	0.00	
59.002	150.38	0.15	0.00	5.84	-3.34	0.00	0.00	0.00	
60.006	154.49	0.51	0.00	68.25	-38.73	0.00	0.00	0.00	
61.006	154.69	0.53	0.00	11.97	-38.54	0.00	0.00	0.00	
62.006	151.95	0.29	0.00	7.05	-7.82	0.00	0.00	0.00	
63.016	151.05	0.21	0.00	5.10	-9.52	0.00	0.00	0.00	
64.032	150.31	0.14	0.00	4.44	-3.30	0.00	0.00	0.00	
65.025	150.69	0.18	0.00	3.15	-2.79	0.00	0.00	0.00	
66.012	150.92	0.20	0.00	3.16	-2.51	0.00	0.00	0.00	



67.029	151.21	0.22	0.00	3.18	-2.37	0.00	0.00	0.00
68.046	151.47	0.25	0.00	2.81	-2.20	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
69.038	151.59	0.26	0.00	2.16	-2.02	0.00	0.00	0.00	
70.055	151.65	0.26	0.00	2.16	-1.90	0.00	0.00	0.00	
71.009	151.75	0.27	0.00	2.16	-1.81	0.00	0.00	0.00	
72.010	151.82	0.28	0.00	1.82	-1.68	0.00	0.00	0.00	
73.043	151.78	0.27	0.00	1.14	-1.50	0.00	0.00	0.00	
74.076	151.69	0.26	0.00	1.14	-1.37	0.00	0.00	0.00	
75.030	151.63	0.26	0.00	1.14	-1.30	0.00	0.00	0.00	
76.063	151.59	0.26	0.00	1.14	-1.24	0.00	0.00	0.00	
77.017	151.57	0.25	0.00	1.15	-1.20	0.00	0.00	0.00	
78.050	151.56	0.25	0.00	1.16	-1.17	0.00	0.00	0.00	
79.004	151.56	0.25	0.00	1.16	-1.15	0.00	0.00	0.00	
80.037	151.56	0.25	0.00	1.16	-1.12	0.00	0.00	0.00	
81.070	151.58	0.25	0.00	1.15	-1.10	0.00	0.00	0.00	
82.024	151.59	0.26	0.00	1.16	-1.09	0.00	0.00	0.00	
83.057	151.62	0.26	0.00	1.16	-1.08	0.00	0.00	0.00	
84.011	151.64	0.26	0.00	1.16	-1.07	0.00	0.00	0.00	
85.044	151.68	0.26	0.00	1.16	-1.06	0.00	0.00	0.00	
86.005	151.71	0.27	0.00	1.17	-1.05	0.00	0.00	0.00	
87.005	151.75	0.27	0.00	1.17	-1.05	0.00	0.00	0.00	
88.005	151.78	0.27	0.00	1.17	-1.04	0.00	0.00	0.00	
89.005	151.83	0.28	0.00	1.18	-1.04	0.00	0.00	0.00	
90.005	151.87	0.28	0.00	1.18	-1.03	0.00	0.00	0.00	
91.005	151.91	0.28	0.00	1.19	-1.03	0.00	0.00	0.00	
92.005	151.96	0.29	0.00	1.19	-1.03	0.00	0.00	0.00	
93.055	152.01	0.29	0.00	1.18	-1.02	0.00	0.00	0.00	
94.015	152.05	0.30	0.00	1.18	-1.02	0.00	0.00	0.00	
95.018	152.10	0.30	0.00	1.18	-0.98	0.00	0.00	0.00	
96.031	152.23	0.31	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	152.23	0.31	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 8

0.000	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
1.050	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
2.019	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
3.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
4.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
5.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
6.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
7.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
8.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
9.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
10.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
11.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
12.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00
13.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
16.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
37.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
38.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
39.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
40.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
41.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
42.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
43.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
44.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
45.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
46.014	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
47.003	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
48.035	235.00	0.29	0.00	0.00	0.00	0.00	0.00	0.00	
49.022	235.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
50.017	235.00	0.00	0.00	0.00	-0.00	0.00	0.00	0.00	
51.031	235.00	0.00	0.00	0.00	-0.01	0.00	0.00	0.00	
52.025	235.00	0.00	0.00	0.02	-0.02	0.00	0.00	0.00	
53.030	235.00	0.00	0.00	0.04	-0.04	0.00	0.00	0.00	
54.008	235.00	0.00	0.00	0.06	-0.06	0.00	0.00	0.00	
55.018	235.00	0.00	0.00	0.09	-0.09	0.00	0.00	0.00	
56.061	235.00	0.00	0.00	0.14	-0.15	0.00	0.00	0.00	
57.014	235.00	0.00	0.00	0.23	-0.24	0.00	0.00	0.00	
58.044	235.00	0.00	0.00	0.37	-0.46	0.00	0.00	0.00	
59.002	235.00	0.00	0.00	0.82	-1.03	0.00	0.00	0.00	
60.006	236.16	0.41	0.00	11.58	-1.76	0.00	0.00	0.00	

61.006	237.05	0.50	0.00	2.14	-2.26	0.00	0.00	0.00
62.006	236.94	0.48	0.00	1.28	-2.45	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
63.016	236.71	0.46	0.00	0.93	-2.35	0.00	0.00	0.00	
64.032	236.44	0.43	0.00	0.81	-2.23	0.00	0.00	0.00	
65.025	236.16	0.41	0.00	0.58	-2.09	0.00	0.00	0.00	
66.012	235.86	0.38	0.00	0.58	-1.95	0.00	0.00	0.00	
67.029	235.56	0.35	0.00	0.59	-1.79	0.00	0.00	0.00	
68.046	235.29	0.32	0.00	0.52	-1.43	0.00	0.00	0.00	
69.038	235.12	0.30	0.00	0.40	-0.79	0.00	0.00	0.00	
70.055	235.07	0.30	0.00	0.40	-0.40	0.00	0.00	0.00	
71.009	235.07	0.30	0.00	0.40	-0.39	0.00	0.00	0.00	
72.010	235.08	0.30	0.00	0.34	-0.32	0.00	0.00	0.00	
73.043	235.07	0.30	0.00	0.21	-0.24	0.00	0.00	0.00	
74.076	235.07	0.30	0.00	0.21	-0.21	0.00	0.00	0.00	
75.030	235.07	0.30	0.00	0.21	-0.21	0.00	0.00	0.00	
76.063	235.07	0.30	0.00	0.21	-0.21	0.00	0.00	0.00	
77.017	235.07	0.30	0.00	0.22	-0.21	0.00	0.00	0.00	
78.050	235.07	0.30	0.00	0.22	-0.22	0.00	0.00	0.00	
79.004	235.07	0.30	0.00	0.22	-0.22	0.00	0.00	0.00	
80.037	235.07	0.30	0.00	0.22	-0.21	0.00	0.00	0.00	
81.070	235.08	0.30	0.00	0.22	-0.17	0.00	0.00	0.00	
82.024	235.09	0.30	0.00	0.22	-0.14	0.00	0.00	0.00	
83.057	235.11	0.30	0.00	0.22	-0.15	0.00	0.00	0.00	
84.011	235.13	0.30	0.00	0.22	-0.15	0.00	0.00	0.00	
85.044	235.15	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
86.005	235.17	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
87.005	235.19	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
88.005	235.21	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
89.005	235.23	0.31	0.00	0.22	-0.14	0.00	0.00	0.00	
90.005	235.25	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
91.005	235.27	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
92.005	235.30	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
93.055	235.32	0.32	0.00	0.22	-0.14	0.00	0.00	0.00	
94.015	235.34	0.33	0.00	0.22	-0.14	0.00	0.00	0.00	
95.018	235.36	0.33	0.00	0.22	-0.13	0.00	0.00	0.00	
96.031	235.39	0.33	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	235.39	0.33	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 9

0.000	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
1.050	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
2.019	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
3.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
4.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
5.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
6.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00
7.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00



LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	<-----Inflow----->					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
10.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
11.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
12.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
13.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
14.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
15.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
16.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
17.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
18.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
19.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
20.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
21.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
22.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
23.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
24.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
25.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
26.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
27.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
28.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
29.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
30.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
31.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
32.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
33.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
34.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
35.014	236.00	1.72	0.00	0.00	0.00	0.00	0.00	0.00	
36.014	236.00	1.72	0.00	0.01	0.00	0.00	0.00	0.00	
37.014	236.00	1.72	0.00	0.02	0.00	0.00	0.00	0.00	
38.014	236.00	1.72	0.00	0.03	0.00	0.00	0.00	0.00	
39.014	236.00	1.72	0.00	0.04	0.00	0.00	0.00	0.00	
40.014	236.01	1.72	0.00	0.05	0.00	0.00	0.00	0.00	
41.014	236.01	1.72	0.00	0.06	0.00	0.00	0.00	0.00	
42.014	236.01	1.72	0.00	0.07	0.00	0.00	0.00	0.00	
43.014	236.02	1.72	0.00	0.08	0.00	0.00	0.00	0.00	
44.014	236.02	1.72	0.00	0.08	0.00	0.00	0.00	0.00	
45.014	236.02	1.72	0.00	0.09	0.00	0.00	0.00	0.00	
46.014	236.03	1.72	0.00	0.10	0.00	0.00	0.00	0.00	
47.003	236.03	1.72	0.00	0.10	0.00	0.00	0.00	0.00	
48.035	236.04	1.73	0.00	0.13	0.00	0.00	0.00	0.00	
49.022	236.05	1.73	0.00	0.16	0.00	0.00	0.00	0.00	
50.017	236.05	1.73	0.00	0.18	0.00	0.00	0.00	0.00	
51.031	236.06	1.73	0.00	0.22	0.00	0.00	0.00	0.00	
52.025	236.07	1.73	0.00	0.25	0.00	0.00	0.00	0.00	
53.030	236.09	1.73	0.00	0.31	0.00	0.00	0.00	0.00	
54.008	236.10	1.74	0.00	0.36	0.00	0.00	0.00	0.00	



55.018	236.12	1.74	0.00	0.44	0.00	0.00	0.00	0.00
56.061	236.15	1.74	0.00	0.57	0.00	0.00	0.00	0.00

LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar. (ac)	!<-----Inflow----->!					Link Q (cfs)	Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
57.014	236.18	1.75	0.00	0.77	0.00	0.00	0.00	0.00	
58.044	236.22	1.76	0.00	1.09	0.00	0.00	0.00	0.00	
59.002	236.29	1.77	0.00	2.09	0.00	0.00	0.00	0.00	
60.006	236.82	1.86	0.00	20.73	0.00	0.00	0.00	0.00	
61.006	237.34	1.95	0.00	3.44	0.00	0.00	0.00	0.00	
62.006	237.46	1.97	0.00	2.00	0.00	0.00	0.00	0.00	
63.016	237.53	1.98	0.00	1.43	0.00	0.00	0.00	0.00	
64.032	237.59	1.99	0.00	1.24	0.00	0.00	0.00	0.00	
65.025	237.63	2.00	0.00	0.88	0.00	0.00	0.00	0.00	
66.012	237.67	2.00	0.00	0.88	0.00	0.00	0.00	0.00	
67.029	237.70	2.01	0.00	0.88	0.00	0.00	0.00	0.00	
68.046	237.74	2.01	0.00	0.78	0.00	0.00	0.00	0.00	
69.038	237.77	2.02	0.00	0.60	0.00	0.00	0.00	0.00	
70.055	237.79	2.02	0.00	0.60	0.00	0.00	0.00	0.00	
71.009	237.82	2.03	0.00	0.60	0.00	0.00	0.00	0.00	
72.010	237.84	2.03	0.00	0.50	0.00	0.00	0.00	0.00	
73.043	237.85	2.03	0.00	0.31	0.00	0.00	0.00	0.00	
74.076	237.87	2.04	0.00	0.31	0.00	0.00	0.00	0.00	
75.030	237.88	2.04	0.00	0.31	0.00	0.00	0.00	0.00	
76.063	237.89	2.04	0.00	0.31	0.00	0.00	0.00	0.00	
77.017	237.91	2.04	0.00	0.32	0.00	0.00	0.00	0.00	
78.050	237.92	2.04	0.00	0.32	0.00	0.00	0.00	0.00	
79.004	237.93	2.05	0.00	0.32	0.00	0.00	0.00	0.00	
80.037	237.94	2.05	0.00	0.32	0.00	0.00	0.00	0.00	
81.070	237.96	2.05	0.00	0.31	0.00	0.00	0.00	0.00	
82.024	237.97	2.05	0.00	0.32	0.00	0.00	0.00	0.00	
83.057	237.98	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
84.011	237.99	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
85.044	238.01	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
86.005	238.02	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
87.005	238.03	2.06	0.00	0.32	0.00	0.00	0.00	0.00	
88.005	238.04	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
89.005	238.06	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
90.005	238.07	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
91.005	238.08	2.07	0.00	0.32	0.00	0.00	0.00	0.00	
92.005	238.10	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
93.055	238.11	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
94.015	238.12	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
95.018	238.13	2.08	0.00	0.32	0.00	0.00	0.00	0.00	
96.031	238.14	2.08	0.00	0.00	0.00	0.00	0.00	0.00	
96.064	238.14	2.08	0.00	0.00	0.00	0.00	0.00	0.00	

\*\*\* Group: BASE Node: 999  
 0.000 196.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  
 1.050 196.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00







LEGENDS OF CLERMONT 25YR96HR STORM EVENT

\*\*\*\*\* Node Time Series by Node - LEGENDS \*\*\*\*\*

Time (hrs)	Stage (ft)	Surface Ar.(ac)	!<-----Inflow----->!					Link Q (cfs)	Link Outflow (cfs)
			Base Q (cfs)	Onsite (cfs)	Offsite (cfs)	Bndry Q (cfs)	Link Q (cfs)		
51.031	196.70	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
52.025	196.73	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
53.030	196.77	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
54.008	196.80	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
55.018	196.83	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
56.061	196.87	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
57.014	196.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
58.044	196.93	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
59.002	196.97	0.00	0.00	0.01	0.00	0.00	0.00	0.00	
60.006	197.00	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
61.006	197.03	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
62.006	197.06	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
63.016	197.08	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
64.032	197.11	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
65.025	197.14	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
66.012	197.17	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
67.029	197.20	0.00	0.00	0.17	0.00	0.00	0.00	0.00	
68.046	197.22	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
69.038	197.25	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
70.055	197.28	0.00	0.00	0.16	0.00	0.00	0.00	0.00	
71.009	197.31	0.00	0.00	0.15	0.00	0.00	0.00	0.00	
72.010	197.33	0.00	0.00	0.15	0.00	0.00	0.00	0.00	
73.043	197.36	0.00	0.00	0.14	0.00	0.00	0.00	0.00	
74.076	197.39	0.00	0.00	0.14	0.00	0.00	0.00	0.00	
75.030	197.42	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
76.063	197.45	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
77.017	197.47	0.00	0.00	0.13	0.00	0.00	0.00	0.00	
78.050	197.50	0.00	0.00	0.12	0.00	0.00	0.00	0.00	
79.004	197.53	0.00	0.00	0.12	0.00	0.00	0.00	0.00	
80.037	197.56	0.00	0.00	0.11	0.00	0.00	0.00	0.00	
81.070	197.59	0.00	0.00	0.11	0.00	0.00	0.00	0.00	
82.024	197.61	0.00	0.00	0.11	0.00	0.00	0.00	0.00	
83.057	197.64	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
84.011	197.67	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
85.044	197.70	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
86.005	197.72	0.00	0.00	0.10	0.00	0.00	0.00	0.00	
87.005	197.75	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
88.005	197.78	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
89.005	197.81	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
90.005	197.83	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
91.005	197.86	0.00	0.00	0.09	0.00	0.00	0.00	0.00	
92.005	197.89	0.00	0.00	0.08	0.00	0.00	0.00	0.00	
93.055	197.92	0.00	0.00	0.08	0.00	0.00	0.00	0.00	
94.015	197.94	0.00	0.00	0.08	0.00	0.00	0.00	0.00	
95.018	197.97	0.00	0.00	0.08	0.00	0.00	0.00	0.00	

96.031	198.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
96.064	198.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



**"PONDS" INFILTRATION ANALYSIS  
25 YEAR-96 HOUR STORM**



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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND1  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 450.00  
Equivalent Pond Width, [W] (ft): 85.00

Base Of Aquifer Elevation, [B] (ft above datum): 189.18  
Water Table Elevation, [WT] (ft above datum): 189.28  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 42.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 21.00  
Maximum area for unsaturated infiltration, (sq ft): 35165

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
200.000	11173.0
201.000	15030.0
202.000	19325.0
203.000	24007.0
204.000	29436.0
205.000	35165.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	15.94
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	134436

Stage

-----

Peak Stage, (ft datum):	202.47
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	4.9360
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	134436

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND2A  
Engineer: KK  
Date: 6/22/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 60.00

Base Of Aquifer Elevation, [B] (ft above datum): 186.00  
Water Table Elevation, [WT] (ft above datum): 186.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 28.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 14.00  
Maximum area for unsaturated infiltration, (sq ft): 21703

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
190.000	8544.0
191.000	9991.0
192.000	11494.0
193.000	13054.0
194.000	14671.0
195.000	16344.0
196.000	18074.0
197.000	19860.0
198.000	21703.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	20.41
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	172484

Stage  
-----

Peak Stage, (ft datum):	195.51
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	3.2333
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	117016

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND2B  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 830.00  
Equivalent Pond Width, [W] (ft): 80.00

Base Of Aquifer Elevation, [B] (ft above datum): 159.00  
Water Table Elevation, [WT] (ft above datum): 159.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 27.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 13.50  
Maximum area for unsaturated infiltration, (sq ft): 75398

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
180.000	48345.0
181.000	53643.0
182.000	58997.0
183.000	64408.0
184.000	69875.0
185.000	75398.0



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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	43.08
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	363741

Stage

-----

Peak Stage, (ft datum):	182.17
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	9.2742
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	363741

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND2C  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 580.00  
Equivalent Pond Width, [W] (ft): 220.00

Base Of Aquifer Elevation, [B] (ft above datum): 150.00  
Water Table Elevation, [WT] (ft above datum): 150.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 29.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 14.50  
Maximum area for unsaturated infiltration, (sq ft): 53126

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
163.000	59806.0
164.000	66928.0
165.000	74127.0
166.000	92834.0
167.000	112932.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs): 30.17  
Time, (hrs): 60.00

Cumulative Inflow Volume, (ft<sup>3</sup>): 254366

Stage

-----

Peak Stage, (ft datum): 165.08  
Time, (hrs): 63.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs): 0.00  
Time, (hrs): 0.00

Cumulative weir discharge volume, (ft<sup>3</sup>): 0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs): 6.9325  
Time, (hrs): 94.00

Cumulative Infiltration Volume, (ft<sup>3</sup>): 254368

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND3  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 120.00

Base Of Aquifer Elevation, [B] (ft above datum): 154.30  
Water Table Elevation, [WT] (ft above datum): 154.40  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 26.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 13.00  
Maximum area for unsaturated infiltration, (sq ft): 86562

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
165.000	25902.0
166.000	29827.0
167.000	33926.0
168.000	38307.0
169.000	42990.0
170.000	47981.0
171.000	53382.0
172.000	58983.0
173.000	64842.0
174.000	79437.0
175.000	86562.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	65.67
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	561960

Stage

-----

Peak Stage, (ft datum):	171.08
Time, (hrs):	62.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	8.0853
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	491994

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND4  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 166.78  
Water Table Elevation, [WT] (ft above datum): 166.88  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 38.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 19.00  
Maximum area for unsaturated infiltration, (sq ft): 71144

Groundwater mound intersects pond bottom?: Yes



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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
177.000	31738.0
178.000	36864.0
179.000	42308.0
180.000	48005.0
181.000	53614.0
182.000	59360.0
183.000	70317.0
184.000	88888.0
185.000	117772.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	34.85
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	294210

Stage

-----

Peak Stage, (ft datum):	179.29
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	9.4196
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	294210

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND6  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 169.51  
Water Table Elevation, [WT] (ft above datum): 169.61  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 43.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 20.00  
Maximum area for unsaturated infiltration, (sq ft): 51685

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
199.000	43522.0
200.000	46914.0
201.000	50362.0
202.000	53868.0
203.000	57429.0
204.000	61047.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	12.92
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	113080

Stage

-----

Peak Stage, (ft datum):	176.90
Time, (hrs):	96.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	7.2553
Time, (hrs):	60.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	113080

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND7  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 360.00

Base Of Aquifer Elevation, [B] (ft above datum): 141.00  
Water Table Elevation, [WT] (ft above datum): 141.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 25.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 82379.00  
Maximum area for unsaturated infiltration, (sq ft): 13

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
149.000	2470.0
150.000	4992.0
155.000	24257.0
160.000	46329.0
165.000	73571.0
170.000	155713.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	68.59
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	578292

Stage  
-----

Peak Stage, (ft datum):	156.99
Time, (hrs):	60.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	38.7256
Time, (hrs):	60.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	556190



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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: PONDS  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 232.00  
Water Table Elevation, [WT] (ft above datum): 232.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 19.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 10.00  
Maximum area for unsaturated infiltration, (sq ft): 51038

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
235.000	12733.0
236.000	17045.0
237.000	21240.0
238.000	30362.0
239.000	51919.0
240.000	106391.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	11.64
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	98770

Stage

-----

Peak Stage, (ft datum):	237.03
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	2.4461
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	94603

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND10  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 240.00

Base Of Aquifer Elevation, [B] (ft above datum): 200.25  
Water Table Elevation, [WT] (ft above datum): 200.35  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 40.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 20.00  
Maximum area for unsaturated infiltration, (sq ft): 68074

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
210.000	4032.0
211.000	7773.0
212.000	16102.0
213.000	30736.0
214.000	47421.0
215.000	55253.0
216.000	61490.0
217.000	67885.0
218.000	75221.0
219.000	84246.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	30.38
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	256356

Stage

-----

Peak Stage, (ft datum):	214.19
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	10.4336
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	256357

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND11  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 370.00  
Equivalent Pond Width, [W] (ft): 70.00

Base Of Aquifer Elevation, [B] (ft above datum): 197.80  
Water Table Elevation, [WT] (ft above datum): 197.90  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 26.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 13.00  
Maximum area for unsaturated infiltration, (sq ft): 36816

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
211.000	18190.0
212.000	20681.0
213.000	23229.0
214.000	25833.0
215.000	28494.0
216.000	31212.0
217.000	33986.0
218.000	36816.0



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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	24.96
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	210515

Stage  
-----

Peak Stage, (ft datum):	214.50
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	4.0706
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	210515

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND12  
Engineer: KK  
Date: 6/29

II. Input Data

Equivalent Pond Length, [L] (ft): 170.00  
Equivalent Pond Width, [W] (ft): 50.00

Base Of Aquifer Elevation, [B] (ft above datum): 197.70  
Water Table Elevation, [WT] (ft above datum): 197.80  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 44.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 22.00  
Maximum area for unsaturated infiltration, (sq ft): 24475

Groundwater mound intersects pond bottom?: Yes

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	32.14
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	271208

Stage  
-----

Peak Stage, (ft datum):	215.21
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	7.0660
Time, (hrs):	63.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	205658

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
205.000	3877.0
206.000	5013.0
207.000	6244.0
208.000	7558.0
209.000	8962.0
210.000	10421.0
211.000	12127.0
212.000	13925.0
213.000	16505.0
214.000	19138.0
215.000	21778.0
216.000	24475.0

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND14  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 200.00  
Equivalent Pond Width, [W] (ft): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 225.35  
Water Table Elevation, [WT] (ft above datum): 225.45  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 15.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 8.00  
Maximum area for unsaturated infiltration, (sq ft): 19390

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data

Stage (ft datum)	Area (ft <sup>2</sup> )
230.000	7999.0
231.000	9374.0
232.000	10806.0
233.000	12294.0
234.000	13839.0
235.000	15441.0
236.000	17099.0
237.000	18813.0
238.000	20585.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	10.80
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	91352

Stage

-----

Peak Stage, (ft datum):	233.64
Time, (hrs):	62.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	1.3758
Time, (hrs):	66.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	64960

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND15  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 460.00  
Equivalent Pond Width, [W] (ft): 70.00

Base Of Aquifer Elevation, [B] (ft above datum): 187.50  
Water Table Elevation, [WT] (ft above datum): 187.60  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 32.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 16.00  
Maximum area for unsaturated infiltration, (sq ft): 61245

Groundwater mound intersects pond bottom?: Yes



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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
194.000	15942.0
195.000	19950.0
196.000	26789.0
197.000	32495.0
198.000	38594.0
199.000	46652.0
200.000	53840.0
201.000	61245.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	34.39
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	289952

Stage

-----

Peak Stage, (ft datum):	198.07
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	7.3214
Time, (hrs):	65.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	250093

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND16  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 148.92  
Water Table Elevation, [WT] (ft above datum): 149.02  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 33.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 17.00  
Maximum area for unsaturated infiltration, (sq ft): 79894

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
159.000	24947.0
160.000	28793.0
161.000	32699.0
162.000	36816.0
163.000	48429.0
164.000	53637.0
165.000	66228.0
166.000	72248.0
167.000	87797.0
168.000	95584.0
169.000	103960.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	41.62
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	352208

Stage  
-----

Peak Stage, (ft datum):	162.85
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	8.8647
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	352209

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND18  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 1120.00  
Equivalent Pond Width, [W] (ft): 115.00

Base Of Aquifer Elevation, [B] (ft above datum): 154.40  
Water Table Elevation, [WT] (ft above datum): 154.50  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 40.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 20.00  
Maximum area for unsaturated infiltration, (sq ft): 126563

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
165.000	54929.0
166.000	63859.0
167.000	74662.0
168.000	86031.0
169.000	102410.0
170.000	117830.0
171.000	144184.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	53.72
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	453589

Stage

-----

Peak Stage, (ft datum):	166.88
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	16.3594
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	453589



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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND19  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 140.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.20  
Water Table Elevation, [WT] (ft above datum): 165.30  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 20.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 10.00  
Maximum area for unsaturated infiltration, (sq ft): 48337

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
178.000	31630.0
179.000	34770.0
180.000	38011.0
181.000	41352.0
182.000	44794.0
183.000	48337.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	23.65
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	199413

Stage

-----

Peak Stage, (ft datum):	179.97
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	4.3688
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	199413

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND20  
Engineer: KK  
Date: 7/20/98

II. Input Data

Equivalent Pond Length, [L] (ft): 350.00  
Equivalent Pond Width, [W] (ft): 200.00

Base Of Aquifer Elevation, [B] (ft above datum): 187.00  
Water Table Elevation, [WT] (ft above datum): 187.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 12.00  
Maximum area for unsaturated infiltration, (sq ft): 49575

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
191.000	17861.0
192.000	21422.0
193.000	27278.0
194.000	34259.0
195.000	41553.0
196.000	50338.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	18.28
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	154099

Stage  
-----

Peak Stage, (ft datum):	193.34
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	4.0251
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	121789

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND21  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 370.00  
Equivalent Pond Width, [W] (ft): 250.00

Base Of Aquifer Elevation, [B] (ft above datum): 182.00  
Water Table Elevation, [WT] (ft above datum): 182.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 14.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 7.00  
Maximum area for unsaturated infiltration, (sq ft): 93128

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
190.000	21423.0
191.000	34973.0
192.000	48552.0
193.000	59854.0
194.000	71514.0
195.000	81528.0
196.000	93128.0



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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	59.19
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	501594

Stage

-----

Peak Stage, (ft datum):	194.58
Time, (hrs):	62.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	6.2374
Time, (hrs):	63.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	366446

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND22  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 670.00  
Equivalent Pond Width, [W] (ft): 110.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.00  
Water Table Elevation, [WT] (ft above datum): 165.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 11.50  
Maximum area for unsaturated infiltration, (sq ft): 68868

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
169.000	11428.0
170.000	14734.0
171.000	18283.0
172.000	22005.0
173.000	27913.0
174.000	35306.0
175.000	51427.0
176.000	68868.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow  
-----

Peak Inflow Rate, (cfs):	27.20
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	229614

Stage  
-----

Peak Stage, (ft datum):	173.66
Time, (hrs):	61.00

Overflow Discharge  
-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate  
-----

Peak Infiltration Rate, (cfs):	4.3363
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	207526

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND23  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 400.00

Base Of Aquifer Elevation, [B] (ft above datum): 122.00  
Water Table Elevation, [WT] (ft above datum): 122.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes

Unsaturated vertical infiltration rate, (ft/day): 11.50

Maximum area for unsaturated infiltration, (sq ft): 104788

Groundwater mound intersects pond bottom?: Yes

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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
134.000	10714.0
135.000	14385.0
136.000	18695.0
137.000	23006.0
138.000	27317.0
139.000	31627.0
140.000	35938.0
141.000	41998.0
142.000	48059.0
143.000	54120.0
144.000	60180.0
145.000	66241.0
146.000	73950.0
147.000	81660.0
150.000	104788.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	103.50
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	872691

Stage

-----

Peak Stage, (ft datum):	145.59
Time, (hrs):	62.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	10.2308
Time, (hrs):	82.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	815997

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Retention Pond Recovery Analysis - Inflow Hydrograph  
-----

I. Job Information

Job Name: POND24  
Engineer: KK  
Date: 6/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 530.00  
Equivalent Pond Width, [W] (ft): 480.00

Base Of Aquifer Elevation, [B] (ft above datum): 101.50  
Water Table Elevation, [WT] (ft above datum): 101.60  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 31.00  
Fillable Porosity of Aquifer, [n] (%): 30.00

Is there a ditch parallel to the pond length axis?: No

Is there a ditch parallel to the pond width axis?: No

Include unsaturated vertical infiltration?: Yes  
Unsaturated vertical infiltration rate, (ft/day): 15.50  
Maximum area for unsaturated infiltration, (sq ft): 174170

Groundwater mound intersects pond bottom?: Yes



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III. Input Data - Discharge Structures  
-----

Weir (or Orifice) #1 is Inactive

Weir (or Orifice) #2 is Inactive

Weir (or Orifice) #3 is Inactive

IV. Input Data - Stage vs Area Data  
-----

Stage (ft datum)	Area (ft <sup>2</sup> )
112.000	82911.0
113.000	91524.0
114.000	101700.0
115.000	122694.0
116.000	130872.0
117.000	152453.0
118.000	173761.0
119.000	187863.0

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VIII. Summary - Cumulative Volumes, Peaks Rates, and Peak Stage

Inflow

-----

Peak Inflow Rate, (cfs):	163.28
Time, (hrs):	60.00
Cumulative Inflow Volume, (ft <sup>3</sup> ):	1378484

Stage

-----

Peak Stage, (ft datum):	116.80
Time, (hrs):	61.00

Overflow Discharge

-----

Peak Discharge Rate, (cfs):	0.00
Time, (hrs):	0.00
Cumulative weir discharge volume, (ft <sup>3</sup> ):	0

Infiltration Rate

-----

Peak Infiltration Rate, (cfs):	26.4106
Time, (hrs):	62.00
Cumulative Infiltration Volume, (ft <sup>3</sup> ):	968937

**"PONDS" RECOVERY ANALYSIS  
TREATMENT VOLUME**

Since every basin consists of less than 40 percent impervious, the following calculations for all basins are based on formula:

$$V_T = \frac{1}{2} (\text{area}) + \frac{1}{2} (\text{area} - \text{for volume treatment}) = 1" (\text{area})$$

Per 40C - 42 FAC

$$V_{\text{TPOND1}} = 1" \times (341,508 \text{ Sq. Ft.}) = 28,459 \text{ Cu. Ft.}$$

$$V_{\text{TP2A}} = 1" \times (376,356 \text{ Sq. Ft.}) = 31,363 \text{ Cu. Ft.}$$

$$V_{\text{TP2B}} = 1" \times (816,312 \text{ Sq. Ft.}) = 68,026 \text{ Cu. Ft.}$$

$$V_{\text{TP2C}} = 1" \times (646,428 \text{ Sq. Ft.}) = 53,869 \text{ Cu. Ft.}$$

$$V_{\text{TP3}} = 1" \times (1,027,584 \text{ Sq. Ft.}) = 85,632 \text{ Cu. Ft.}$$

$$V_{\text{TP4}} = 1" \times (801,060 \text{ Sq. Ft.}) = 66,755 \text{ Cu. Ft.}$$

$$V_{\text{TP6}} = 1" \times (456,072 \text{ Sq. Ft.}) = 38,006 \text{ Cu. Ft.}$$

$$V_{\text{TP7}} = 1" \times (1,422,228 \text{ Sq. Ft.}) = 118,519 \text{ Cu. Ft.}$$

$$V_{\text{TP8}} = 1" \times (301,428 \text{ Sq. Ft.}) = 25,119 \text{ Cu. Ft.}$$

$$V_{\text{TP10}} = 1" \times (592,416 \text{ Sq. Ft.}) = 49,368 \text{ Cu. Ft.}$$

$$V_{\text{TP11}} = 1" \times (501,804 \text{ Sq. Ft.}) = 41,817 \text{ Cu. Ft.}$$

$$V_{\text{TP12}} = 1" \times (626,820 \text{ Sq. Ft.}) = 52,235 \text{ Cu. Ft.}$$

$$V_{\text{TP14}} = 1" \times (208,644 \text{ Sq. Ft.}) = 17,387 \text{ Cu. Ft.}$$

$$V_{\text{TP15}} = 1" \times (697,824 \text{ Sq. Ft.}) = 58,152 \text{ Cu. Ft.}$$

$$V_{\text{TP16}} = 1" \times (747,480 \text{ Sq. Ft.}) = 62,290 \text{ Cu. Ft.}$$

$$V_{\text{TP18}} = 1" \times (1,046,736 \text{ Sq. Ft.}) = 87,228 \text{ Cu. Ft.}$$

$$V_{\text{TP19}} = 1" \times (490,476 \text{ Sq. Ft.}) = 40,873 \text{ Cu. Ft.}$$

$$V_{\text{TP20}} = 1" \times (378,972 \text{ Sq. Ft.}) = 31,581 \text{ Cu. Ft.}$$

$$V_{\text{TP21}} = 1" \times (1,036,284 \text{ Sq. Ft.}) = 86,357 \text{ Cu. Ft.}$$

$$V_{TP22} = 1" \times (625,080 \text{ Sq. Ft.}) = 52,090 \text{ Cu. Ft.}$$

$$V_{TP23} = 1" \times (2,217,204 \text{ Sq. Ft.}) = 184,767 \text{ Cu. Ft.}$$

$$V_{TP24} = 1" \times (3,752,688 \text{ Sq. Ft.}) = 312,724 \text{ Cu. Ft.}$$

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND1  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	450.00
Equivalent Pond Width, [W] (ft):	85.00
Pond Bottom Elevation, [PB] (ft above datum):	200.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	189.18
Water Table Elevation, [WT] (ft above datum):	189.28
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	42.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.00
Runoff Volume, [V] (cubic feet)	28459.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0354
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	28459.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0354
Total Recovered Volume, [V] (ft <sup>3</sup> ):	28459.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND2A  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	60.00
Pond Bottom Elevation, [PB] (ft above datum):	190.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	186.00
Water Table Elevation, [WT] (ft above datum):	186.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	28.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.00
Runoff Volume, [V] (cubic feet)	31363.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0836
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	28079.96

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0239
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	3283.04
Maximum Radius Of Influence, [R] (ft):	6.02
Maximum Driving Head, [Hmax] (ft):	4.037
Minimum Driving Head, [Hmin] (ft):	3.900

TOTAL

Total Recovery Time, [T] (days):	0.1074
Total Recovered Volume, [V] (ft <sup>3</sup> ):	31363.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND2B  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	830.00
Equivalent Pond Width, [W] (ft):	80.00
Pond Bottom Elevation, [PB] (ft above datum):	180.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	159.00
Water Table Elevation, [WT] (ft above datum):	159.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	27.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.50
Runoff Volume, [V] (cubic feet)	68026.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0759
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	68026.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0759
Total Recovered Volume, [V] (ft <sup>3</sup> ):	68026.00



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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND2C  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	582.00
Equivalent Pond Width, [W] (ft):	220.00
Pond Bottom Elevation, [PB] (ft above datum):	163.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	150.00
Water Table Elevation, [WT] (ft above datum):	150.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	29.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.50
Runoff Volume, [V] (cubic feet)	53869.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0290
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	53869.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0290
Total Recovered Volume, [V] (ft <sup>3</sup> ):	53869.00

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Retention Pond Recovery Analysis  
-----

I. Job Information

Job Name: POND3  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 120.00  
Pond Bottom Elevation, [PB] (ft above datum): 165.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 154.30  
Water Table Elevation, [WT] (ft above datum): 154.40  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 26.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 13.00

Runoff Volume, [V] (cubic feet) 85632.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1663  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 85632.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.1663  
Total Recovered Volume, [V] (ft<sup>3</sup>): 85632.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND4  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	177.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	166.78
Water Table Elevation, [WT] (ft above datum):	166.88
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	38.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	19.00
Runoff Volume, [V] (cubic feet)	66755.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0439
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	66755.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0439
Total Recovered Volume, [V] (ft <sup>3</sup> ):	66755.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND6  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	420.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	199.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	169.51
Water Table Elevation, [WT] (ft above datum):	169.61
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	43.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.50
Runoff Volume, [V] (cubic feet)	38006.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0210
Recovered Volume From Unsaturated Flow, [V1] (ft^3):	38006.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft^3):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0210
Total Recovered Volume, [V] (ft^3):	38006.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND7  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	360.00
Pond Bottom Elevation, [PB] (ft above datum):	149.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	141.00
Water Table Elevation, [WT] (ft above datum):	141.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	25.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	12.50
Runoff Volume, [V] (cubic feet)	118519.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0439
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	118519.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0439
Total Recovered Volume, [V] (ft <sup>3</sup> ):	118519.00

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Retention Pond Recovery Analysis

I. Job Information

Job Name: PONDS  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 600.00  
Equivalent Pond Width, [W] (ft): 200.00  
Pond Bottom Elevation, [PB] (ft above datum): 235.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 232.00  
Water Table Elevation, [WT] (ft above datum): 232.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 19.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 9.50

Runoff Volume, [V] (cubic feet) 25119.00  
Percent Recovery Of Runoff Volume, [PV] (%): 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.0220  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 25119.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.0220  
Total Recovered Volume, [V] (ft<sup>3</sup>): 25119.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND10  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	240.00
Pond Bottom Elevation, [PB] (ft above datum):	210.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	200.25
Water Table Elevation, [WT] (ft above datum):	200.35
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	49368.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0257
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	49368.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0257
Total Recovered Volume, [V] (ft <sup>3</sup> ):	49368.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND11  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	370.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	211.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.80
Water Table Elevation, [WT] (ft above datum):	197.90
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	26.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.00
Runoff Volume, [V] (cubic feet)	41817.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1242
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	41817.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1242
Total Recovered Volume, [V] (ft <sup>3</sup> ):	41817.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND12  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	170.00
Equivalent Pond Width, [W] (ft):	50.00
Pond Bottom Elevation, [PB] (ft above datum):	205.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.70
Water Table Elevation, [WT] (ft above datum):	197.81
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	44.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	22.00
Runoff Volume, [V] (cubic feet)	52235.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0980
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	18334.51

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.6482
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	33900.49
Maximum Radius Of Influence, [R] (ft):	56.33
Maximum Driving Head, [Hmax] (ft):	11.178
Minimum Driving Head, [Hmin] (ft):	7.190

TOTAL

Total Recovery Time, [T] (days):	0.7463
Total Recovered Volume, [V] (ft <sup>3</sup> ):	52235.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND14  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	200.00
Equivalent Pond Width, [W] (ft):	100.00
Pond Bottom Elevation, [PB] (ft above datum):	230.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	225.35
Water Table Elevation, [WT] (ft above datum):	225.45
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	15.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	7.50
Runoff Volume, [V] (cubic feet)	17387.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1159
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	17387.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1159
Total Recovered Volume, [V] (ft <sup>3</sup> ):	17387.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND15  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	460.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	194.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	187.50
Water Table Elevation, [WT] (ft above datum):	187.60
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	32.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.00
Runoff Volume, [V] (cubic feet)	58152.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1129
Recovered Volume From Unsaturated Flow, [V1] (ft^3):	58152.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft^3):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1129
Total Recovered Volume, [V] (ft^3):	58152.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND16  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	159.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	148.92
Water Table Elevation, [WT] (ft above datum):	149.02
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	33.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.50
Runoff Volume, [V] (cubic feet)	62290.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0315
Recovered Volume From Unsaturated Flow, [V1] (ft^3):	62290.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft^3):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0315
Total Recovered Volume, [V] (ft^3):	62290.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND18  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	1120.00
Equivalent Pond Width, [W] (ft):	115.00
Pond Bottom Elevation, [PB] (ft above datum):	165.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	154.40
Water Table Elevation, [WT] (ft above datum):	154.50
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	87228.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0339
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	87228.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0339
Total Recovered Volume, [V] (ft <sup>3</sup> ):	87228.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND19  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	330.00
Equivalent Pond Width, [W] (ft):	140.00
Pond Bottom Elevation, [PB] (ft above datum):	178.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	165.20
Water Table Elevation, [WT] (ft above datum):	165.30
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	20.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	10.00
Runoff Volume, [V] (cubic feet)	40873.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0885
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	40873.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0885
Total Recovered Volume, [V] (ft <sup>3</sup> ):	40873.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND20  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	350.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	191.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	187.00
Water Table Elevation, [WT] (ft above datum):	187.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	23.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	11.50
Runoff Volume, [V] (cubic feet)	31581.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0392
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	31581.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0392
Total Recovered Volume, [V] (ft <sup>3</sup> ):	31581.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND21  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 370.00  
Equivalent Pond Width, [W] (ft): 250.00  
Pond Bottom Elevation, [PB] (ft above datum): 190.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 182.00  
Water Table Elevation, [WT] (ft above datum): 182.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 14.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 7.00

Runoff Volume, [V] (cubic feet) 86357.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1334  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 86357.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.1334  
Total Recovered Volume, [V] (ft<sup>3</sup>): 86357.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND22  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 670.00  
Equivalent Pond Width, [W] (ft): 110.00  
Pond Bottom Elevation, [PB] (ft above datum): 169.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.00  
Water Table Elevation, [WT] (ft above datum): 165.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 11.50

Runoff Volume, [V] (cubic feet) 52090.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.0615  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 52090.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.0615  
Total Recovered Volume, [V] (ft<sup>3</sup>): 52090.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND23  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 420.00  
Equivalent Pond Width, [W] (ft): 400.00  
Pond Bottom Elevation, [PB] (ft above datum): 130.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 122.00  
Water Table Elevation, [WT] (ft above datum): 122.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 11.50

Runoff Volume, [V] (cubic feet) 184767.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.0956  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 184767.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.0956  
Total Recovered Volume, [V] (ft<sup>3</sup>): 184767.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND24  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	530.00
Equivalent Pond Width, [W] (ft):	480.00
Pond Bottom Elevation, [PB] (ft above datum):	112.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	101.45
Water Table Elevation, [WT] (ft above datum):	101.55
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	31.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	15.50
Runoff Volume, [V] (cubic feet)	312724.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0793
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	312724.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0793
Total Recovered Volume, [V] (ft <sup>3</sup> ):	312724.00

**"PONDS" RECOVERY ANALYSIS  
TOTAL RUNOFF VOLUME**

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND1  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	450.00
Equivalent Pond Width, [W] (ft):	85.00
Pond Bottom Elevation, [PB] (ft above datum):	200.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	189.18
Water Table Elevation, [WT] (ft above datum):	189.28
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	42.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.00
Runoff Volume, [V] (cubic feet)	125474.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1531
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	123012.02

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0003
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	2461.98
Maximum Radius Of Influence, [R] (ft):	1.43
Maximum Driving Head, [Hmax] (ft):	10.784
Minimum Driving Head, [Hmin] (ft):	10.720

TOTAL

Total Recovery Time, [T] (days):	0.1535
Total Recovered Volume, [V] (ft <sup>3</sup> ):	125474.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND2A  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	60.00
Pond Bottom Elevation, [PB] (ft above datum):	190.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	186.00
Water Table Elevation, [WT] (ft above datum):	186.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	28.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.00
Runoff Volume, [V] (cubic feet)	161595.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0836
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	28079.96

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	13.3363
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	133515.05
Maximum Radius Of Influence, [R] (ft):	176.87
Maximum Driving Head, [Hmax] (ft):	9.463
Minimum Driving Head, [Hmin] (ft):	3.900

TOTAL

Total Recovery Time, [T] (days):	13.4199
Total Recovered Volume, [V] (ft <sup>3</sup> ):	161595.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND2B  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	830.00
Equivalent Pond Width, [W] (ft):	80.00
Pond Bottom Elevation, [PB] (ft above datum):	180.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	159.00
Water Table Elevation, [WT] (ft above datum):	159.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	27.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.50
Runoff Volume, [V] (cubic feet)	340530.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.3799
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	340530.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.3799
Total Recovered Volume, [V] (ft <sup>3</sup> ):	340530.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND2C  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	582.00
Equivalent Pond Width, [W] (ft):	220.00
Pond Bottom Elevation, [PB] (ft above datum):	163.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	150.00
Water Table Elevation, [WT] (ft above datum):	150.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	29.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	14.50
Runoff Volume, [V] (cubic feet)	229315.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1235
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	229315.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1235
Total Recovered Volume, [V] (ft <sup>3</sup> ):	229315.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND3  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	330.00
Equivalent Pond Width, [W] (ft):	120.00
Pond Bottom Elevation, [PB] (ft above datum):	165.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	154.30
Water Table Elevation, [WT] (ft above datum):	154.40
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	26.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.00
Runoff Volume, [V] (cubic feet)	529004.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.2446
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	125928.08

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	8.3100
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	403075.94
Maximum Radius Of Influence, [R] (ft):	194.05
Maximum Driving Head, [Hmax] (ft):	20.779
Minimum Driving Head, [Hmin] (ft):	10.600

TOTAL

Total Recovery Time, [T] (days):	8.5546
Total Recovered Volume, [V] (ft <sup>3</sup> ):	529004.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND4  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	400.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	177.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	166.78
Water Table Elevation, [WT] (ft above datum):	166.88
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	38.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	19.00
Runoff Volume, [V] (cubic feet)	274150.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1598
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	242879.89

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0538
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	31270.11
Maximum Radius Of Influence, [R] (ft):	16.68
Maximum Driving Head, [Hmax] (ft):	10.511
Minimum Driving Head, [Hmin] (ft):	10.120

TOTAL

Total Recovery Time, [T] (days):	0.2135
Total Recovered Volume, [V] (ft <sup>3</sup> ):	274150.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND6  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	420.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	199.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	169.51
Water Table Elevation, [WT] (ft above datum):	169.61
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	43.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	21.50
Runoff Volume, [V] (cubic feet)	104466.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0578
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	104466.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0578
Total Recovered Volume, [V] (ft <sup>3</sup> ):	104466.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND7  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	360.00
Pond Bottom Elevation, [PB] (ft above datum):	149.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	141.00
Water Table Elevation, [WT] (ft above datum):	141.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	25.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	12.50
Runoff Volume, [V] (cubic feet)	540164.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1896
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	511919.63

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0564
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	28244.38
Maximum Radius Of Influence, [R] (ft):	12.25
Maximum Driving Head, [Hmax] (ft):	8.031
Minimum Driving Head, [Hmin] (ft):	7.900

TOTAL

Total Recovery Time, [T] (days):	0.2460
Total Recovered Volume, [V] (ft <sup>3</sup> ):	540164.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: PONDS  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	235.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	232.00
Water Table Elevation, [WT] (ft above datum):	232.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	19.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	9.50
Runoff Volume, [V] (cubic feet)	91795.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0805
Recovered Volume From Unsaturated Flow, [V1] (ft^3):	91795.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft^3):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.0805
Total Recovered Volume, [V] (ft^3):	91795.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND10  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 400.00  
Equivalent Pond Width, [W] (ft): 240.00  
Pond Bottom Elevation, [PB] (ft above datum): 210.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 200.35  
Water Table Elevation, [WT] (ft above datum): 200.45  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 40.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 20.00

Runoff Volume, [V] (cubic feet) 239820.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1249  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 239820.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0000  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 0.00  
Maximum Radius Of Influence, [R] (ft): 0.00  
Maximum Driving Head, [Hmax] (ft): 0.000  
Minimum Driving Head, [Hmin] (ft): 0.000

TOTAL

Total Recovery Time, [T] (days): 0.1249  
Total Recovered Volume, [V] (ft<sup>3</sup>): 239820.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND11  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	370.00
Equivalent Pond Width, [W] (ft):	70.00
Pond Bottom Elevation, [PB] (ft above datum):	211.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.80
Water Table Elevation, [WT] (ft above datum):	197.90
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	26.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	13.00
Runoff Volume, [V] (cubic feet)	196788.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.3023
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	101787.05

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.4777
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	95000.95
Maximum Radius Of Influence, [R] (ft):	49.18
Maximum Driving Head, [Hmax] (ft):	16.768
Minimum Driving Head, [Hmin] (ft):	13.100

TOTAL

Total Recovery Time, [T] (days):	0.7800
Total Recovered Volume, [V] (ft <sup>3</sup> ):	196788.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND12  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	170.00
Equivalent Pond Width, [W] (ft):	50.00
Pond Bottom Elevation, [PB] (ft above datum):	205.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	197.70
Water Table Elevation, [WT] (ft above datum):	197.81
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	44.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	22.00
Runoff Volume, [V] (cubic feet)	253713.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.0980
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	18334.51

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	6.6094
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	235378.50
Maximum Radius Of Influence, [R] (ft):	234.43
Maximum Driving Head, [Hmax] (ft):	34.882
Minimum Driving Head, [Hmin] (ft):	7.190

TOTAL

Total Recovery Time, [T] (days):	6.7074
Total Recovered Volume, [V] (ft <sup>3</sup> ):	253713.00



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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND14  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 200.00  
Equivalent Pond Width, [W] (ft): 100.00  
Pond Bottom Elevation, [PB] (ft above datum): 230.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 225.35  
Water Table Elevation, [WT] (ft above datum): 225.45  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 15.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 7.50

Runoff Volume, [V] (cubic feet) 85646.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1820  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 27300.02

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 10.6471  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 58345.98  
Maximum Radius Of Influence, [R] (ft): 104.42  
Maximum Driving Head, [Hmax] (ft): 7.467  
Minimum Driving Head, [Hmin] (ft): 4.550

TOTAL

Total Recovery Time, [T] (days): 10.8291  
Total Recovered Volume, [V] (ft<sup>3</sup>): 85646.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND15  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 460.00  
Equivalent Pond Width, [W] (ft): 70.00  
Pond Bottom Elevation, [PB] (ft above datum): 194.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 187.50  
Water Table Elevation, [WT] (ft above datum): 187.60  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 32.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 16.00

Runoff Volume, [V] (cubic feet) 270835.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1200  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 61823.95

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 6.2372  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 209011.06  
Maximum Radius Of Influence, [R] (ft): 156.81  
Maximum Driving Head, [Hmax] (ft): 12.891  
Minimum Driving Head, [Hmin] (ft): 6.400

TOTAL

Total Recovery Time, [T] (days): 6.3572  
Total Recovered Volume, [V] (ft<sup>3</sup>): 270835.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND16  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	600.00
Equivalent Pond Width, [W] (ft):	200.00
Pond Bottom Elevation, [PB] (ft above datum):	159.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	148.92
Water Table Elevation, [WT] (ft above datum):	149.02
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	33.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	16.50
Runoff Volume, [V] (cubic feet)	330209.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1668
Recovered Volume From Unsaturated Flow, [V1] (ft^3):	330209.00

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0000
Recovered Volume From Saturated Flow, [V2] (ft^3):	0.00
Maximum Radius Of Influence, [R] (ft):	0.00
Maximum Driving Head, [Hmax] (ft):	0.000
Minimum Driving Head, [Hmin] (ft):	0.000

TOTAL

Total Recovery Time, [T] (days):	0.1668
Total Recovered Volume, [V] (ft^3):	330209.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND18  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	1120.00
Equivalent Pond Width, [W] (ft):	115.00
Pond Bottom Elevation, [PB] (ft above datum):	165.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	154.40
Water Table Elevation, [WT] (ft above datum):	154.50
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	40.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	20.00
Runoff Volume, [V] (cubic feet)	424644.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.1575
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	405720.03

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	0.0041
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	18923.97
Maximum Radius Of Influence, [R] (ft):	4.84
Maximum Driving Head, [Hmax] (ft):	10.647
Minimum Driving Head, [Hmin] (ft):	10.500

TOTAL

Total Recovery Time, [T] (days):	0.1616
Total Recovered Volume, [V] (ft <sup>3</sup> ):	424644.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND19  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 330.00  
Equivalent Pond Width, [W] (ft): 140.00  
Pond Bottom Elevation, [PB] (ft above datum): 178.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.20  
Water Table Elevation, [WT] (ft above datum): 165.30  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 20.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 10.00

Runoff Volume, [V] (cubic feet) 186265.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.3810  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 176021.97

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 0.0093  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 10243.03  
Maximum Radius Of Influence, [R] (ft): 5.65  
Maximum Driving Head, [Hmax] (ft): 12.922  
Minimum Driving Head, [Hmin] (ft): 12.700

TOTAL

Total Recovery Time, [T] (days): 0.3903  
Total Recovered Volume, [V] (ft<sup>3</sup>): 186265.00

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### Retention Pond Recovery Analysis

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#### I. Job Information

Job Name: POND20  
Engineer: KK  
Date: 7/29/98

#### II. Input Data

Equivalent Pond Length, [L] (ft): 350.00  
Equivalent Pond Width, [W] (ft): 200.00  
Pond Bottom Elevation, [PB] (ft above datum): 191.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 187.00  
Water Table Elevation, [WT] (ft above datum): 187.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 11.50

Runoff Volume, [V] (cubic feet) 143939.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

#### III. Results

##### UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1017  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 81899.88

##### SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 5.5814  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 62039.13  
Maximum Radius Of Influence, [R] (ft): 83.22  
Maximum Driving Head, [Hmax] (ft): 4.786  
Minimum Driving Head, [Hmin] (ft): 3.900

##### TOTAL

Total Recovery Time, [T] (days): 5.6832  
Total Recovered Volume, [V] (ft<sup>3</sup>): 143939.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND21  
Engineer: KR  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	370.00
Equivalent Pond Width, [W] (ft):	250.00
Pond Bottom Elevation, [PB] (ft above datum):	190.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	182.00
Water Table Elevation, [WT] (ft above datum):	182.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	14.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	7.00
Runoff Volume, [V] (cubic feet)	470593.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.3386
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	219224.84

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	12.5759
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	251368.16
Maximum Radius Of Influence, [R] (ft):	138.62
Maximum Driving Head, [Hmax] (ft):	10.617
Minimum Driving Head, [Hmin] (ft):	7.900

TOTAL

Total Recovery Time, [T] (days):	12.9145
Total Recovered Volume, [V] (ft <sup>3</sup> ):	470593.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND22  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 670.00  
Equivalent Pond Width, [W] (ft): 110.00  
Pond Bottom Elevation, [PB] (ft above datum): 169.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 165.00  
Water Table Elevation, [WT] (ft above datum): 165.10  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 23.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 11.50

Runoff Volume, [V] (cubic feet) 213958.00  
Percent Recovery Of Runoff Volume, [PV] (%) 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.1017  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 86228.87

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 9.9849  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 127729.13  
Maximum Radius Of Influence, [R] (ft): 120.48  
Maximum Driving Head, [Hmax] (ft): 5.633  
Minimum Driving Head, [Hmin] (ft): 3.900

TOTAL

Total Recovery Time, [T] (days): 10.0867  
Total Recovered Volume, [V] (ft<sup>3</sup>): 213958.00



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Retention Pond Recovery Analysis

I. Job Information

Job Name: POND23  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft):	420.00
Equivalent Pond Width, [W] (ft):	400.00
Pond Bottom Elevation, [PB] (ft above datum):	130.00
Porosity Of Material Within Pond, [p] (%):	100.00
Base Of Aquifer Elevation, [B] (ft above datum):	122.00
Water Table Elevation, [WT] (ft above datum):	122.10
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day)	23.00
Fillable Porosity of Aquifer, [n] (%):	30.00
Vertical Unsaturated Infiltration, [Iv] (ft/day):	11.50
Runoff Volume, [V] (cubic feet)	814515.00
Percent Recovery Of Runoff Volume, [PV] (%)	100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days):	0.2061
Recovered Volume From Unsaturated Flow, [V1] (ft <sup>3</sup> ):	398160.09

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days):	12.3604
Recovered Volume From Saturated Flow, [V2] (ft <sup>3</sup> ):	416354.91
Maximum Radius Of Influence, [R] (ft):	175.09
Maximum Driving Head, [Hmax] (ft):	10.378
Minimum Driving Head, [Hmin] (ft):	7.900

TOTAL

Total Recovery Time, [T] (days):	12.5665
Total Recovered Volume, [V] (ft <sup>3</sup> ):	814515.00

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Retention Pond Recovery Analysis  
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I. Job Information

Job Name: POND24  
Engineer: KK  
Date: 7/29/98

II. Input Data

Equivalent Pond Length, [L] (ft): 530.00  
Equivalent Pond Width, [W] (ft): 480.00  
Pond Bottom Elevation, [PB] (ft above datum): 112.00  
Porosity Of Material Within Pond, [p] (%): 100.00

Base Of Aquifer Elevation, [B] (ft above datum): 101.45  
Water Table Elevation, [WT] (ft above datum): 101.55  
Horizontal Saturated Hydraulic Conductivity, [Kh] (ft/day) 31.00  
Fillable Porosity of Aquifer, [n] (%): 30.00  
Vertical Unsaturated Infiltration, [Iv] (ft/day): 15.50

Runoff Volume, [V] (cubic feet) 1284497.00  
Percent Recovery Of Runoff Volume, [PV] (%): 100.00

III. Results

UNSATURATED FLOW

Recovery Time From Unsaturated Flow, [T1] (days): 0.2023  
Recovered Volume From Unsaturated Flow, [V1] (ft<sup>3</sup>): 797543.81

SATURATED FLOW

Recovery Time From Saturated Flow, [T2] (days): 4.1882  
Recovered Volume From Saturated Flow, [V2] (ft<sup>3</sup>): 486953.19  
Maximum Radius Of Influence, [R] (ft): 134.92  
Maximum Driving Head, [Hmax] (ft): 12.364  
Minimum Driving Head, [Hmin] (ft): 10.450

TOTAL

Total Recovery Time, [T] (days): 4.3904  
Total Recovered Volume, [V] (ft<sup>3</sup>): 1284497.00

Geotechnical Investigation  
of Potential Karst Activity  
**LAKE LOUISA CLUB**  
Lake County, Florida



**Andreyev  
Engineering,  
Inc.**

▼ 4500 Orange Blvd.  
Sanford, Florida 32771  
TEL (407) 330-7763  
FAX (407) 330-7765

November 22, 1996  
Project No. PGT-96-165

**TO:** Farner Barley & Associates, Inc.  
350 North Sinclair Avenue  
Tavares, FL 32778

**Attention:** Mr. Robert E. Farner, P.E.

**SUBJECT:** Geotechnical Investigation of Potential Karst Activity, Lake Louisa Club,  
Lake County, Florida

Dear Mr. Farner:

As requested, Andreyev Engineering, Inc. (AEI) has completed a geotechnical investigation of potential karst activity at the subject site. Work was performed in general accordance with AEI proposal No. P-96-116 dated October 15, 1996.

The attached report presents the findings, evaluations and recommendations. AEI appreciates the opportunity to participate in this project and trusts that the information contained herein is sufficient for your immediate needs. If you have any questions or comments, please contact the undersigned.

Sincerely,

ANDREYEV ENGINEERING, INC.

Scott Cavin, P.E.  
Senior Project Engineer  
Florida Registration No. 48125

Nicolas E. Andreyev, P.E.  
President  
Florida Registration No. 35459

## Site and Project Description

The proposed Lake Louisa Club development is located on the west side of U.S. Highway 27 approximately four (4) miles southeast of Clermont, Florida. The property encompasses about 400 acres of land in portions of Sections 4, 5, 8 and 9 of Township 23 South, Range 26 East, Lake County, Florida. The subject site is approximately 1500 feet north of Lake Louisa. Refer to **Figure 1** for a Vicinity Map. The site topography consists of hills and depressions with an estimated elevation change on the order of 150 feet. At the time of AEI's field explorations, the property was undeveloped except for a few abandoned structures. Most of the site had been cleared except for some of the depressions which contained mature trees. It appears that the subject site was formerly a citrus grove.

It is understood that the proposed development will include single family residences, paved streets, a golf course, drainage retention areas, and lake/conservation areas. The residential lot sizes will range from approximately 0.19 to 0.24 acre.

## Purpose and Scope

The purpose of this study was to obtain information on the general subsurface conditions within existing depressions at the site, evaluate the stability of the depressions, and evaluate the potential for sinkhole activity. To accomplish this purpose, the following tasks were performed:

- Review available published data regarding the subsurface and surface conditions in the vicinity of the subject site.
- Locate and identify the boring locations within the depressions.
- Drill six (6) Standard Penetration Test (SPT) borings to a depth of 150 feet below existing ground surface.
- Visually classify and stratify samples recovered from the borings and perform index property tests on selected samples.
- Prepare a report which summarizes the work performed, the field and laboratory data generated, and engineering analyses and recommendations.

## Review of Available U.S. Geological Survey Map

The "Clermont East, Florida" topographic map published by the U.S. Geological Survey (U.S.G.S.) dated 1962 (photorevised 1986) was reviewed. Refer to **Figure 1** for a copy of a portion of this map showing the subject site location. The topography of the site is characterized by hills and depressions. The ground surface elevation ranges from approximately +100 feet, NGVD near the northwest corner of the site to about +250 feet, NGVD in the east central portion of the property.

There are two (2) relatively large circular depressions located in the western portion of the site. The largest is on the western property boundary. This largest feature is approximately 1500 to 2000 feet in diameter by 50 to 75 feet deep. The second large depression is located about 2000 feet southeast of the largest depression. The smaller feature is about 800 to 1000 feet in diameter by 40 feet deep. Three (3) other depressions and topographic low areas are identified on the map within the site boundary. These areas are located along U.S. Highway 27 on the eastern site boundary in the south central portion of the site near the south property boundary, and on the northeastern portion of this site at the northern property boundary.

The topography surrounding the site is similar to the site, consisting of hills and depressions. Swamp symbols are shown in some of the low areas on adjacent properties. The water elevations of Lake Louisa to the south and Lake Felter to the north of the subject site are shown at +94 and +85 feet, NGVD, respectively.

### S.C.S. Soil Survey

The "Soil Survey Report, Maps and Interpretations, Lake County Area, Florida" published by the U.S. Department of Agriculture Soil Conservation Service (S.C.S.) was reviewed. Within the subject property boundaries, the shallow soil types consist of Candler and Lake sands. These soils are deep, excessively well drained soils with a seasonal high groundwater table greater than six (6) feet below ground surface.

### Potentiometric Surface Map

The map "Potentiometric Surface of the Upper Floridan Aquifer in the St. John's River Water Management District and Vicinity, Florida, September 1995" published by the U.S.G.S. was reviewed. The elevation of the potentiometric surface in the vicinity of the subject site is approximately +85 feet, NGVD. Groundwater flow in the Upper Floridan Aquifer is to the northeast.

### Area Geology

The geology of the Central Florida areas is characterized by sedimentary strata formed during three distinct geologic periods. The surficial stratum is composed of undifferentiated Holocene/Pleistocene/Pliocene age sands, containing varying amounts of silt and clay, which extend typically to depths on the order of 40 to 60 feet below ground surface. This upper, mostly sandy zone contains the surficial (water table) aquifer. A Miocene age deposit, the Hawthorne Formation, frequently underlies the surficial sand and is typically composed of clay, clayey sand and sandy limestone containing appreciable amounts of phosphate. This relatively impermeable stratum extends to typical depths of 125 to 150 feet beneath ground surface and serves as the confining layer for the underlying Floridan aquifer. The Floridan aquifer, composed of Eocene age Ocala, Avon Park and Lake City Limestones, is highly productive and supplies most of the drinking water for Central Florida. The extremely high productivity of this aquifer is directly related to its many cavities and interconnected channels. These cavities and channels were formed by dissolution of the limestone caused by the movement of slightly acidic water through the rock.

The geology of the area, as described above, is conducive to the development of sinkholes. The solution features within the limestone can collapse or can allow the downward movement of overlying soils, known as ravelling, to produce depressions at the surface which are typically circular in shape (sinkholes). Sinkholes can occur nearly anywhere in Central Florida, but are more likely to occur in areas characterized by thin confining beds, large differences between the water table elevation and the Floridan aquifer potentiometric level and the presence of limestone in relatively close proximity to the ground surface.

### Previous Geotechnical Reports

The following reports were supplied to AEI for review:

- "Report of Preliminary Subsurface Exploration, Sinkhole Risk Analysis and Effluent Disposal Evaluation, West Hills, Lake County, Florida" dated August 14, 1990 by Westinghouse Environmental and Geotechnical Services, Inc.

- "Report of Subsurface Exploration and Geotechnical Engineering Evaluation for Existing Depression areas, Kings Point Subdivision (Formerly Clermont Hills), Lake County, Florida" dated February 14, 1995 by L.J. Nodarse & Associates, Inc.

The Westinghouse study was located in Sections 3, 4, 5 and 9 and the L.J. Nodarse study was located in Section 4 of Township 23 South, Range 26 East. These study areas are within or adjacent to the sections studied for the proposed Lake Louisa Club development. Both studies found relatively thick deposits of sand grading downward into silt and clayey sand at depths between 75 and 100 feet below existing ground surface. Limestone was found in only one (1) of ten (10) SPT borings performed for both studies. The limestone was encountered at approximately elevation +10 feet, NGVD. Both studies concluded that existing subsurface conditions are stable and that the risk of future sinkhole development is moderate to low.

### Field Exploration/Laboratory Testing

The field exploration for the Lake Louisa Club development was performed between October 22nd and November 4, 1996. Six (6) Standard Penetration Test (SPT) borings were drilled in the existing depressions and topographic low areas at the subject site. The borings were advanced to a depth of 150 feet below existing ground surface. SPT N-values were recorded continuously in the upper ten (10) feet of each boring and at five (5) foot intervals thereafter. The borings were completed using the mud rotary method and were grout sealed upon completion. Samples were recovered from each boring and returned to AEI's laboratory for classification and stratification. Index property tests, consisting of moisture content and percent passing the No. 200 sieve were performed on selected samples. Approximate locations of the borings are shown on **Figure 2** and results of the borings in profile form are presented on **Figure 3**. SPT N-values and laboratory test results are shown at the approximate depths adjacent to the profiles on **Figure 3**. On the profiles, horizontal lines designating the interface between differing intervals represent approximate boundaries. The transition between layers is typically gradual.

### Subsurface Conditions

In general, the borings encountered fine sand, slightly silty fine sand, and silty fine sand (Strata 1, 2 and 3) to the termination depths. Exceptions were noted in borings TB-1, TB-2 and TB-3 where relatively minor amounts of slightly clayey to clayey fine sand (Stratum 4) were found at various depths. Refer to the boring profiles on **Figure 3** for a more complete description of the subsoils found.

SPT N-values were generally less than ten (10) in the upper ten (10) feet of each boring. Below ten (10) feet, the N-values were generally greater than 15 and in most cases greater than 20. An exception was noted between the depths of 140 and 150 feet in boring TB-4 where N-values of four (4) and five (5) were recorded. Drilling fluid circulation losses were not noted during drilling. However, a greater than normal use of fluid was noted in boring TB-2 between the depths of 100 and 150 feet.

### Evaluation

As discussed above, the geology of the area where the subject site is located is conducive to the development of sinkholes. Solution features within the limestone that underlies the area can collapse or can allow the downward movement of overlying soils to produce depressions at the surface which are typically circular in shape. The depressions on the subject site and on adjacent properties are believed to have formed by these processes. The depressional features are relatively old as evidenced by the presence of mature trees (where clearing has not occurred) and

the presence of stable slopes. The stability of the depressions and the potential for future suitable activity can be evaluated by analysis of the SPT boring results and the geologic and hydrogeologic conditions in the area.

Sinkholes in the Central Florida area normally develop by subsidence or collapse of unconsolidated soils that overlie the limestone into openings and very loose zones in the limestone. Conditions that favor sinkhole development include the following:

- The presence of openings and very loose (ravelled) zones in the limestone.
- Easily erodible soils above the limestone.
- The presence of a significant hydraulic head between a shallow and a deep water table which promotes a downward erosion process.

Limestone was not found in the borings performed for this study to a depth of 150 feet and limestone was found in only one (1) boring performed at the adjacent properties. However, it is well documented that limestone underlies the area and that the surface of the limestone has been subjected to chemical erosion, creating openings and very loose zones. The sandy soils that were found in the borings are easily erodible if present in a loose condition. However, the relatively high SPT N-values recorded in the borings indicate that the sands are not loose, except in the near surface deposits, which is a typical condition in most of Central Florida. Lastly, the presence of low permeability soils (sandy clay and clay) found near the bottom of some of the borings, indicate a presence of a semi-eroded Hawthorn Formation above the limestone, that will provide confinement between the water table aquifer and the underlying limestone aquifer.

The conditions prior to depression development more than likely included loose sands and thin or leaky Hawthorn deposits. The present conditions at the boring locations indicate relatively dense soils through out the soil profile. The potential for future sinkhole development at the subject site in its present conditions is low relative the other sites in Central Florida. However, alteration of the site can increase the potential for further subsidence. To minimize the potential for future subsidence the development shall implement design and construction techniques to minimize increasing of hydraulic heads and overburdened loads in the depressional areas.

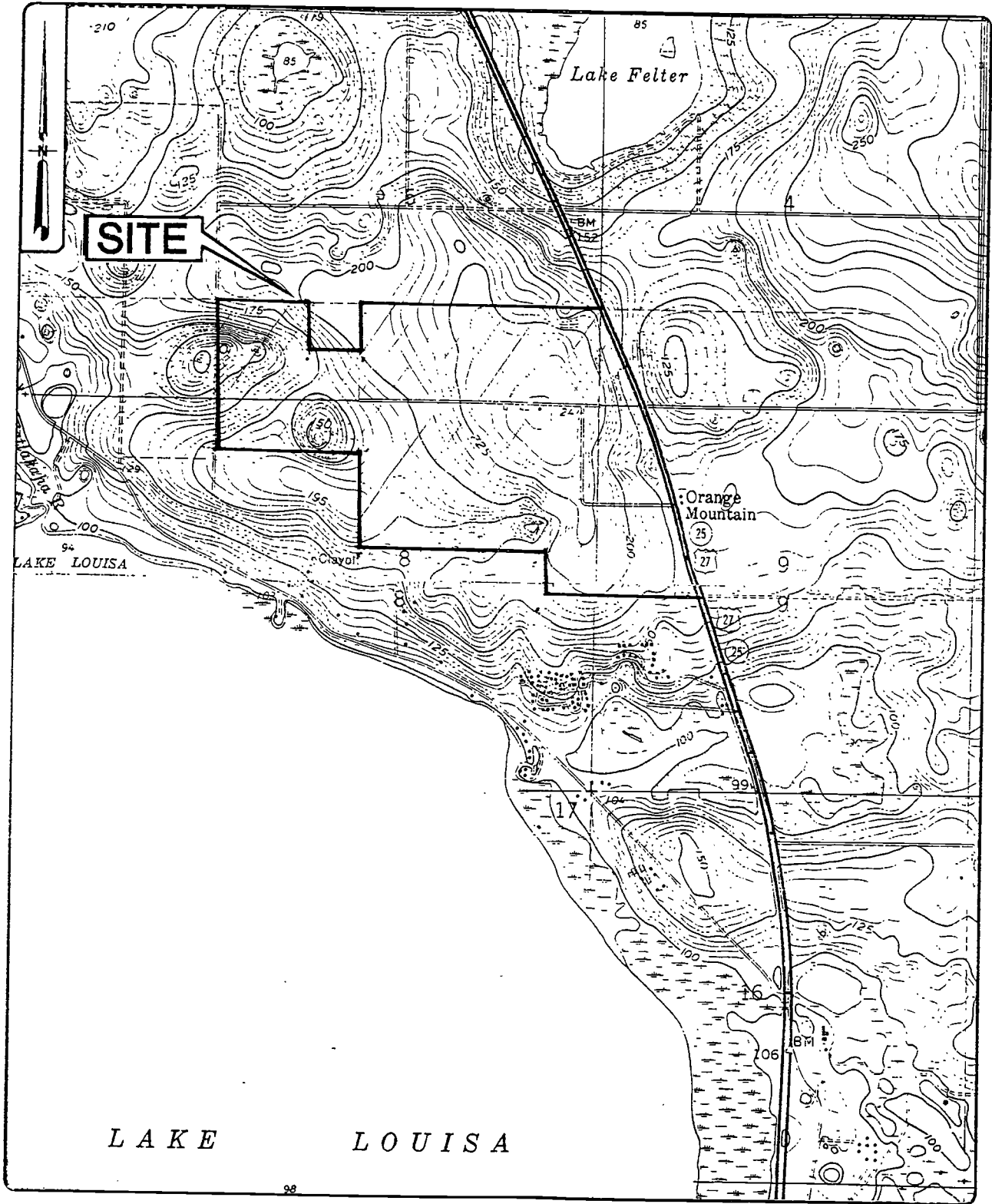
### **Recommendations**

Induced sinkholes, or those caused by man's activities, result from ponding of water, groundwater level declines caused by pumping from the limestone, and significant removal of overburden above the limestone. At the subject site, it is recommended that structures be located at least 200 feet from the edge of proposed surface water bodies and areas where surface water accumulates, such as lakes, drainage retention areas and depressions. In addition, on-site wells should be installed with cased depths of a minimum of 50 feet into the limestone. Due to the thickness of soils over the limestone at the site, significant removal of overburden is not anticipated.

Futher site specific investigations and construction recommendations should be made for all depressional areas during the final design and construction activity on this project.



**FIGURES**



**REFERENCE:**

U.S.G.S. CLERMONT EAST, FLA.  
 QUADRANGLE MAP  
 DATED 1962  
 PHOTOREVISED 1980  
 SECTION 4  
 TOWNSHIP 23 SOUTH  
 RANGE 26 EAST



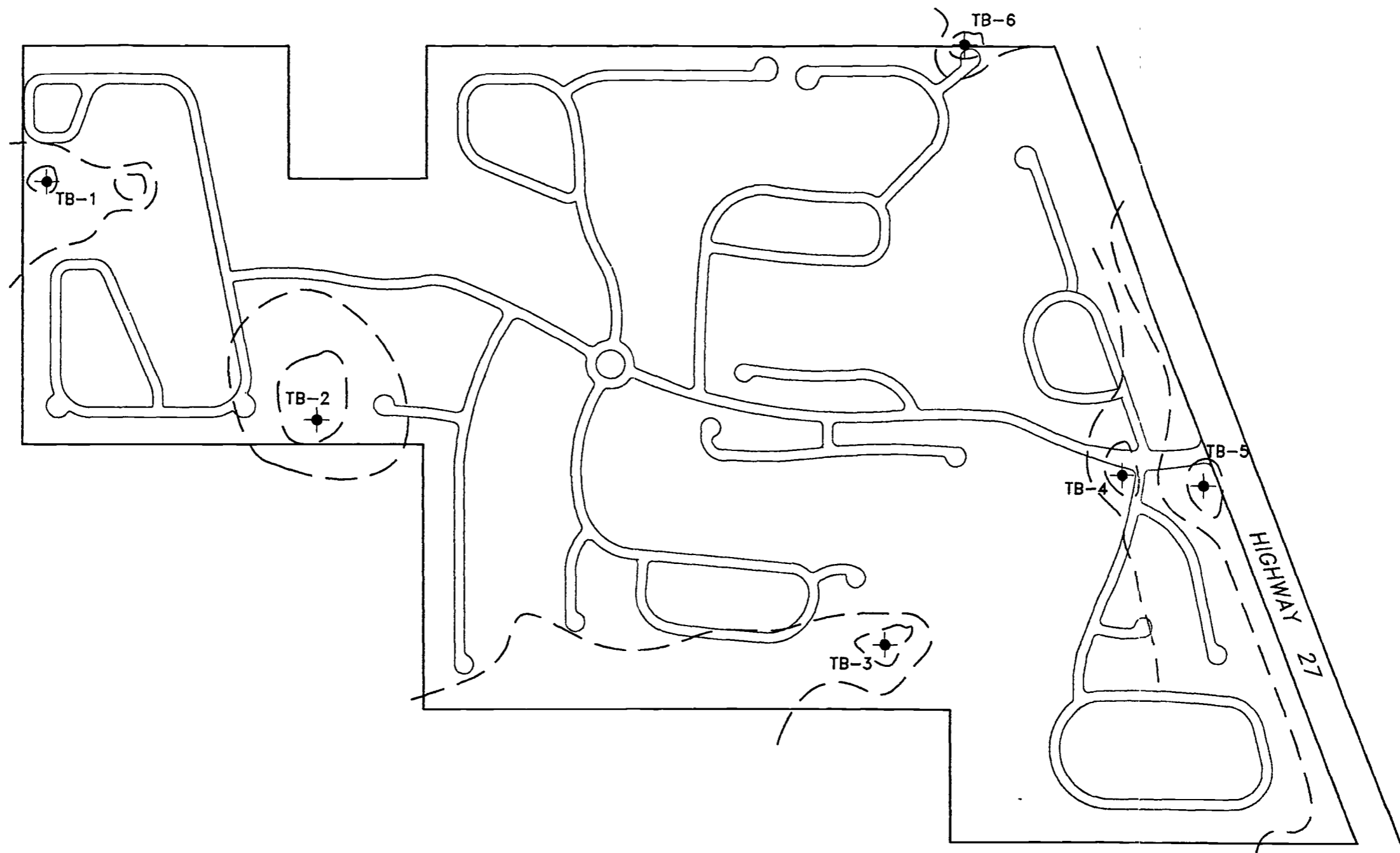
**Andreyev  
 Engineering,  
 Inc.**

GEOTECHNICAL INVESTIGATION  
**LAKE LOUISA CLUB**  
 LAKE COUNTY, FLORIDA


DATE: 11-15-96	SCALE: 1"=2000'
ENGINEER: SC	PN: PGT-96-165


VICINITY MAP

FIGURE 1



**LEGEND**


 APPROXIMATE LOCATION  
 OF SPT BORING

 <b>Andreyev Engineering, Inc.</b>	
DATE: 11/13/96	SCALE: 1"=600'
ENGINEER: SC	PN: PGT-96-165

GEOTECHNICAL INVESTIGATION <b>LAKE LOUISA CLUB</b> LAKE COUNTY, FLORIDA
<b>LOCATION PLAN</b> FIGURE 2

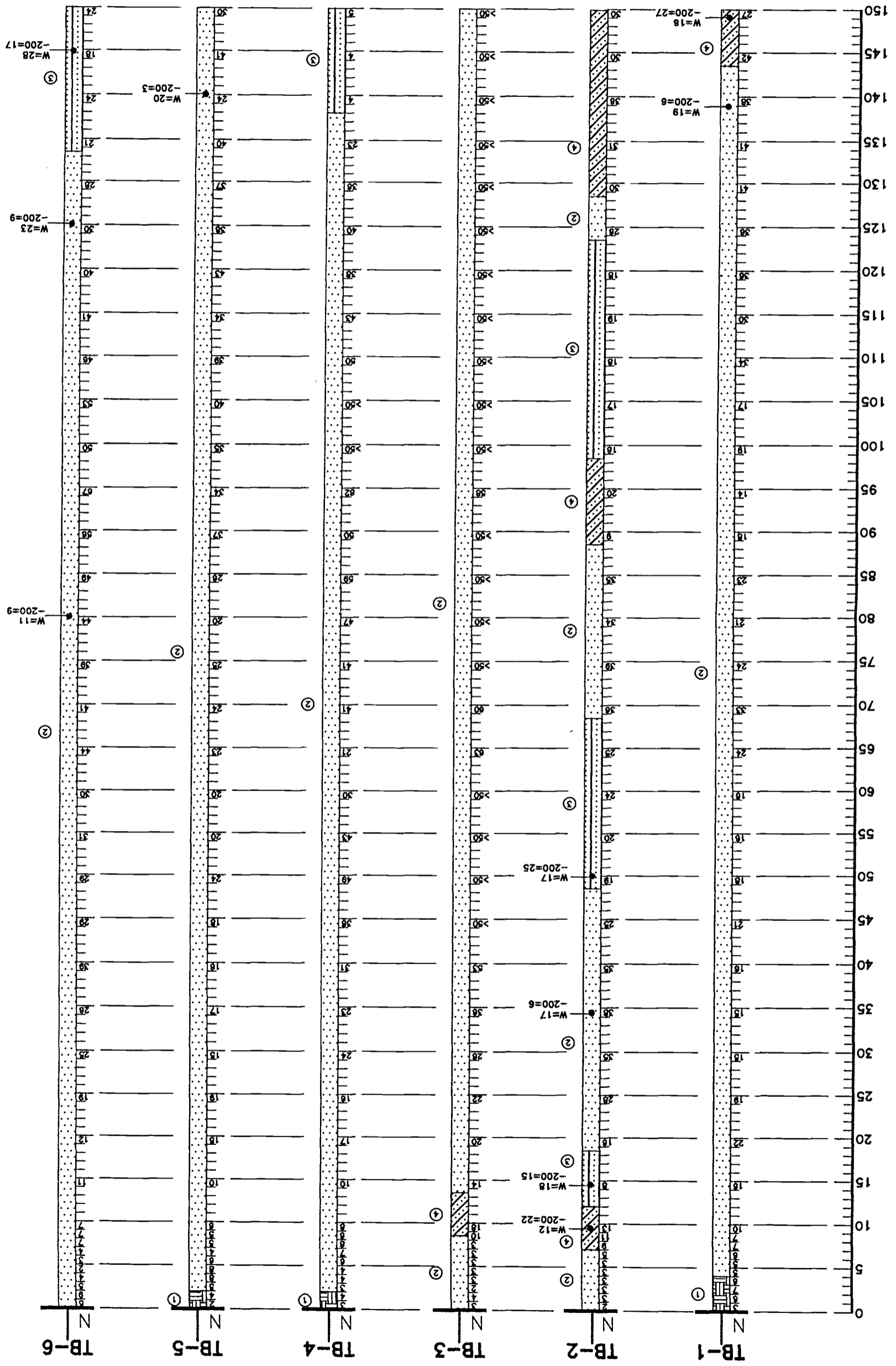
GEOTECHNICAL INVESTIGATION <b>LAKE LOUISA CLUB</b> LAKE COUNTY, FLORIDA <b>SOIL PROFILES</b>	ENGINEER, SC PN: PGT-96-165
	DATE: 11-15-96 SCALE: 1"=12' <b>Andreyev Engineering, Inc.</b>

N STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT  
 -200 PERCENT OF FINES PASSING THE U.S. NO. 200 SIEVE  
 W NATURAL MOISTURE CONTENT IN PERCENT  
 (SP) UNIFIED SOIL CLASSIFICATION GROUP SYMBOL  
 CLAYEY FINE SAND (SP/SC) (SC)  
 LIGHT BROWN TO ORANGISH BROWN SLIGHTLY CLAYEY TO SILTY TO SILTY FINE SAND (SP/SM) (SM)  
 LIGHT GRAY TO LIGHT BROWN TO ORANGISH BROWN SLIGHTLY SILTY FINE SAND (SP) (SP/SM)  
 BROWN TO LIGHT BROWN TO ORANGISH BROWN TO LIGHT GRAY GRAYISH BROWN FINE SAND WITH SMALL ROOTS (TOPSOIL) (SP)

NOTE: GREATER THAN NOMINAL USE OF DRILLING FLUID NOTED IN BORING TB-2 FROM 100 TO 150 FEET.

**LEGEND**

DEPTH IN FEET



Geotechnical Engineering Study,  
Proposed Stormwater  
Management Area  
**PHASE I**  
**LAKE LOUISA CLUB**  
Lake County, Florida



**Andreyev  
Engineering,  
Inc.**

▼ 4500 Orange Blvd.  
Sanford, Florida 32771  
TEL (407) 330-7763  
FAX (407) 330-7765

April 14, 1997  
Project No: PGT-96-165

**TO:** Lennar Homes  
7600 Nob Hill Road  
Tamarac, Florida 33321

**Attention:** Mr. Robert Ahrens

**SUBJECT:** Geotechnical Engineering Study of Proposed Stormwater Management Areas,  
Phase I, Lake Louisa Club, Lake County, Florida

Dear Mr. Ahrens:

As requested, Andreyev Engineering, Inc. (AEI) has completed a geotechnical engineering study for the subject project. The work was performed in general accordance with AEI Proposal No. DJR-97-006, dated April 3, 1997 with written authorization to proceed received on April 8, 1997.

The attached report presents the findings of the study and engineering analyses and recommendations to guide design and construction of the stormwater management areas. AEI appreciates the opportunity to participate in this project and trusts that the information herein is sufficient for your immediate needs. If you have any questions or comments concerning the contents of this report, or if we may be of further service, please do not hesitate to contact the undersigned.

Sincerely,

**ANDREYEV ENGINEERING, INC.**

David J. Rathbun, P.E.  
Senior Project Manager  
Florida Registration No. 40494

Nicolas E. Andreyev, P.E.  
President  
Florida Registration No. 35459

xc: Farner, Barley and Associates, Inc.

## 1.0 SITE AND PROJECT DESCRIPTION

The proposed Lake Louisa Club development is located on the west side of U.S. Highway 27 approximately four (4) miles southeast of Clermont, Florida. The property encompasses about 400 acres of land in portions of Sections 4, 5, 8 and 9 of Township 23 South, Range 26 East, Lake County, Florida. The subject site is approximately 1,500 feet north of Lake Louisa. Refer to Figure 1 for a Vicinity Map. The site topography consists of hills and depressions with an estimated elevation change on the order of 150 feet. At the time of AEI's field exploration, the property was undeveloped except for a few abandoned structures. Most of the site had been cleared except for some of the depressions which contained mature trees. It appears that the subject site was formerly a citrus grove.

It is understood that the proposed development will include single family residences, paved streets, a golf course, drainage retention areas (DRA) and lake/conservation areas. The residential lot sizes will range from approximately 0.19 to 0.24 acre. Phase I consists of the eastern approximately 100 acres of the site. Ten (10) DRA's are planned in Phase I. The proposed DRA locations are shown on Figure 2. Four (4) of the DRA's will be adjacent to the U.S. 27 right-of-way. Final grades have not been determined but it appears that berms will be required between the DRA's and U.S. 27. The DRA's are expected to be on the order of 10 feet deep. Dry ponds are planned except for the DRA between golf holes 1 and 10 which will be lined to create a lake. Boring AB-10 was drilled near the edge of the proposed DRA above the top of the proposed liner. Due to the rolling terrain at the site, cut and fill is planned in roadway and lot areas. A proposed deep cut on the order of 10 feet is planned west of golf hole 18. Boring AB-3 was drilled in this area to assess subsurface conditions up to and below the cut elevation.

## 2.0 PURPOSE AND SCOPE OF SERVICES

The purpose of the study was to explore subsurface conditions at proposed DRA sites and in the proposed roadway cut area and provide the following:

- Soil and groundwater conditions encountered.
- Normal seasonal high groundwater level estimates.
- Permeability test results.
- Slope stability analyses for the berms DRA's.
- Recommendations for berm seepage control adjacent to U.S. Highway 27.
- Recommendations for the roadway cut area, including suitability of soils for use as fill and subgrade.

The field work was performed on April 9 and 10, 1997 and consisted of 10 auger borings to a depth of 25 feet below existing ground surface. Nine (9) of the borings were drilled at proposed DRA locations and 1 boring (AB-3) was drilled in the roadway cut area. In addition, 4 Standard Penetration Test (SPT) borings were previously drilled in or near the DRA sites by AEI. The scope of services for the subject study also included a field permeability test in each of the 10 DRA locations.

Samples were recovered from each boring and returned to AEI's laboratory for visual classification. Moisture content and No. 200 sieve tests were performed on selected samples. Approximate boring locations are shown on Figure 2 and results of the borings in profile form are presented on Figure 3. The upper 25 feet of the previously performed SPT borings (TB-3 through TB-6) are also

shown on Figure 3. Results of the field permeability and laboratory tests are shown adjacent to the profiles. On the profiles, horizontal lines designating the interface between differing materials represent approximate boundaries. The transition between layers is typically gradual.

### 3.0 FINDINGS

#### 3.1 Subsurface Conditions

Fine sand to fine sand with silt (Stratum 1) was the predominant soil type found in the borings. Stratum 1 extended from the ground surface to the termination depth (25 feet) in borings AB-1, AB-3, AB-4, AB-7, AB-10, and TB-4 through TB-6. In borings AB-5, AB-6, and AB-8, Stratum 1 was underlain by fine to medium sand (Stratum 3) at depths ranging from about 18 ½ to 22 feet. In boring AB-9, Stratum 1 extended to a depth of approximately 9 feet where it was underlain by clayey fine sand (Stratum 4) and sandy clay (Stratum 5). Strata 4 and 5 extended to a depth of 22 feet in boring AB-9 where Stratum 1 was encountered to the boring termination depth. The groundwater table was not found in the borings.

The previously performed SPT borings were drilled to a depth of 150 feet below existing ground surface. Below the 25 foot depth shown on Figure 3, the SPT borings encountered fine sand to sand with silt (Stratum 1) for their entire depth.

#### 3.2 S.C.S. Soil Survey

The "Soil Survey Report, Maps and Interpretations, Lake County Area, Florida" published by the U.S. Department of Agriculture Soil Conservation Service (S.C.S.) was reviewed. The shallow soil types within the subject property boundaries consist of Candler and Lake sands. These soils are deep, excessively well drained soils with a seasonal high groundwater table greater than six (6) feet below ground surface.

#### 3.3 Permeability Test Results

The field permeability tests were conducted in temporary PVC slotted casings installed in the boreholes. The slotted PVC casings were installed to create open-hole permeability method. The tests were performed by applying a continuous flow of water to the open-holes to maintain a constant water level. The volume of water used was measured and the permeability was calculated per procedures recommended by the U.S. Bureau of Reclamation (Earth Manual, E-19). Results are as follows:

<u>Location</u>	<u>Tested Depth Interval Below Existing Ground Surface (feet)</u>	<u>Coefficient of Horizontal Permeability (feet per day)</u>
AB-1	5 ½ - 12	28
AB-2	5 ½ - 11 ½	27
AB-4	7 - 12	23
AB-5	7 ½ - 11 ½	29
AB-6	4 - 12	26
AB-7	7 - 12	38
AB-8	4 - 12	25
AB-9	5 - 10	81
AB-10	7 - 12	25
TB-5	7 - 12	19



## **4.0 EVALUATION AND RECOMMENDATIONS**

### **4.1 Drainage Retention Area Design Parameters**

The soils found in each DRA boring except AB-9 and TB-3 consisted of the Stratum 1, 2 and 3 sands. These sands are moderately to highly permeable and will be suitable for exfiltration of stormwater. The Strata 4 and 5 soils found in borings AB-9 and TB-3 have a relatively high fines content and therefore will have a very low permeability. Strata 4 and 5 should be considered as confining layers for purposes of infiltration analysis.

The normal seasonal high groundwater table is estimated to be below the depth of the borings (more than 25 feet below ground surface). However, water will temporarily perch on the Strata 4 and 5 soils after periods of heavy or prolonged rainfall.

### **4.2 Slope Stability**

Pond slopes of 3:1 (H:V) or flatter are expected to be stable. The stability of a 3:1 slope 12 feet high was analyzed using the computer program PCSTABL. The analysis was performed assuming that the pond was full of water and the soils below the water level were saturated. The resulting factor of safety was 1.9. Results are included in **Appendix A**. After final grades have been determined, additional slope stability analyses should be performed based on the actual pond geometry if higher or steeper slopes are planned.

### **4.3 Berm Seepage Control**

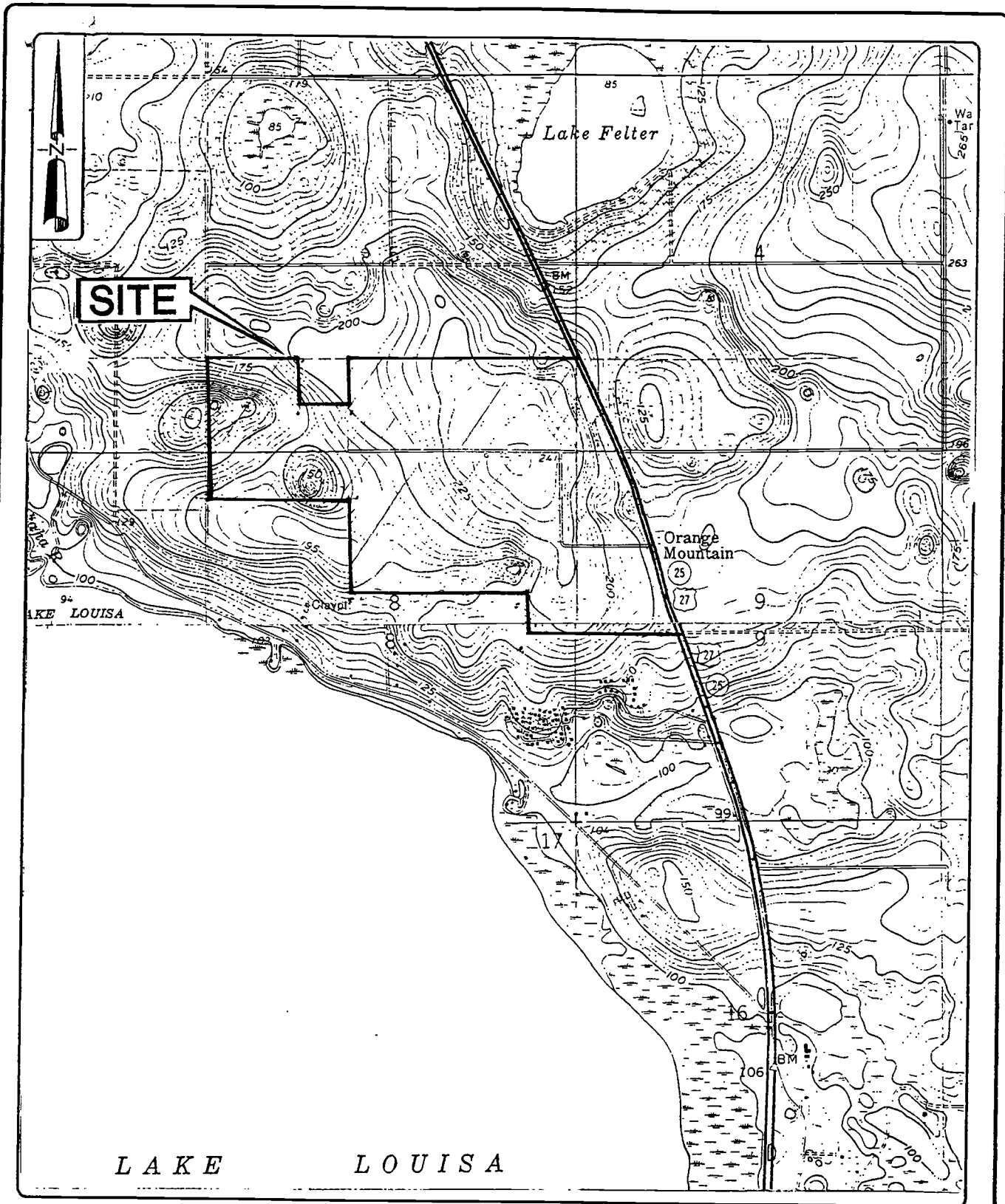
Depending on final grades, berms may be required for the DRA's adjacent to the U.S. 27 right-of-way. Water seepage through the berms can be controlled with a clay core. The core should be at least 2 feet wide, located in the center of the berms, and extend at least 3 feet below the surface elevation of the adjacent right-of-way. The core material should consist of clayey sand or sandy clay having at least 30 percent by weight passing the No. 200 sieve, a liquid limit between 30 and 50, and a plasticity index between 15 and 30. The core material should be placed in maximum 8 inch thick loose lifts and each lift should be compacted to at least 95 percent of the modified Proctor (ASTM D1557) maximum dry density of the soil. A moisture content between 1 percent below and 3 percent above the ASTM D1557 optimum moisture content is recommended during compaction. After plans have been prepared, additional recommendations can be provided regarding the horizontal and vertical extent of the clay core.

### **4.4 Roadway Cut Area**

Stratum 1 sands were found the entire depth of boring AB-3 which was performed in the proposed cut area. These sands are suitable for roadway support and for fill below pavement and structures.

The Stratum 2 and 3 soils found in some of the borings will also be suitable for roadway support and fill. However, the Stratum 4 and 5 clayey soils will not be suitable for roadway or structure support. Stratum 4 and 5 can be used in lower portions of fills but not within 4 feet of pavements and structures.

**FIGURES**



REFERENCE:  
 U.S.G.S. CLERMONT EAST, FLA.  
 QUADRANGLE MAP  
 DATED 1962  
 PHOTOREVISED 1980  
 SECTION 4  
 TOWNSHIP 23 SOUTH  
 RANGE 26 EAST



**Andreyev  
 Engineering,  
 Inc.**

DATE: 4-11-97    SCALE: 1"=2000'  
 ENGINEER: DJR    PN: PGT-96-165

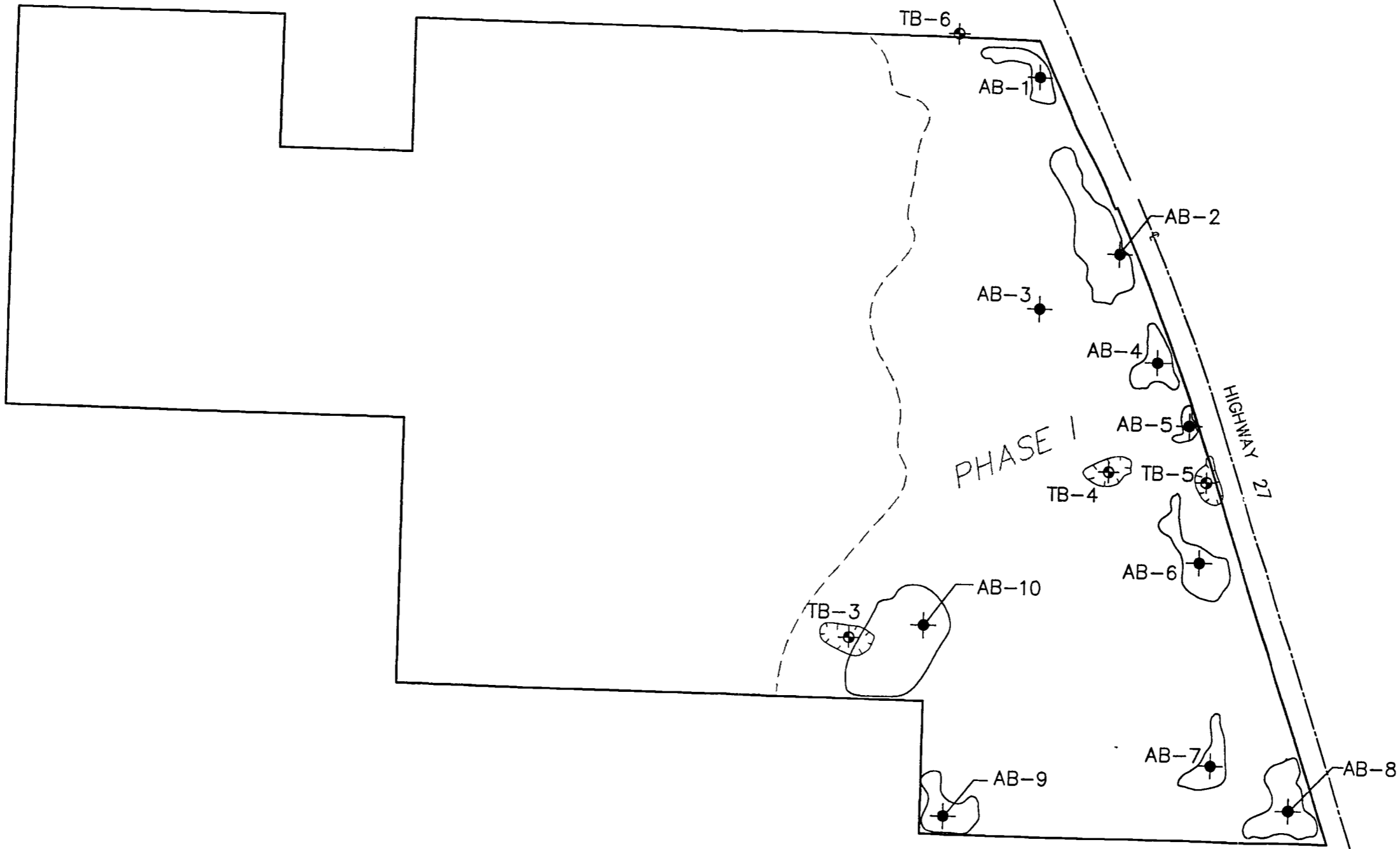
GEOTECHNICAL INVESTIGATION

LAKE LOUISA CLUB

LAKE COUNTY, FLORIDA


VICINITY MAP

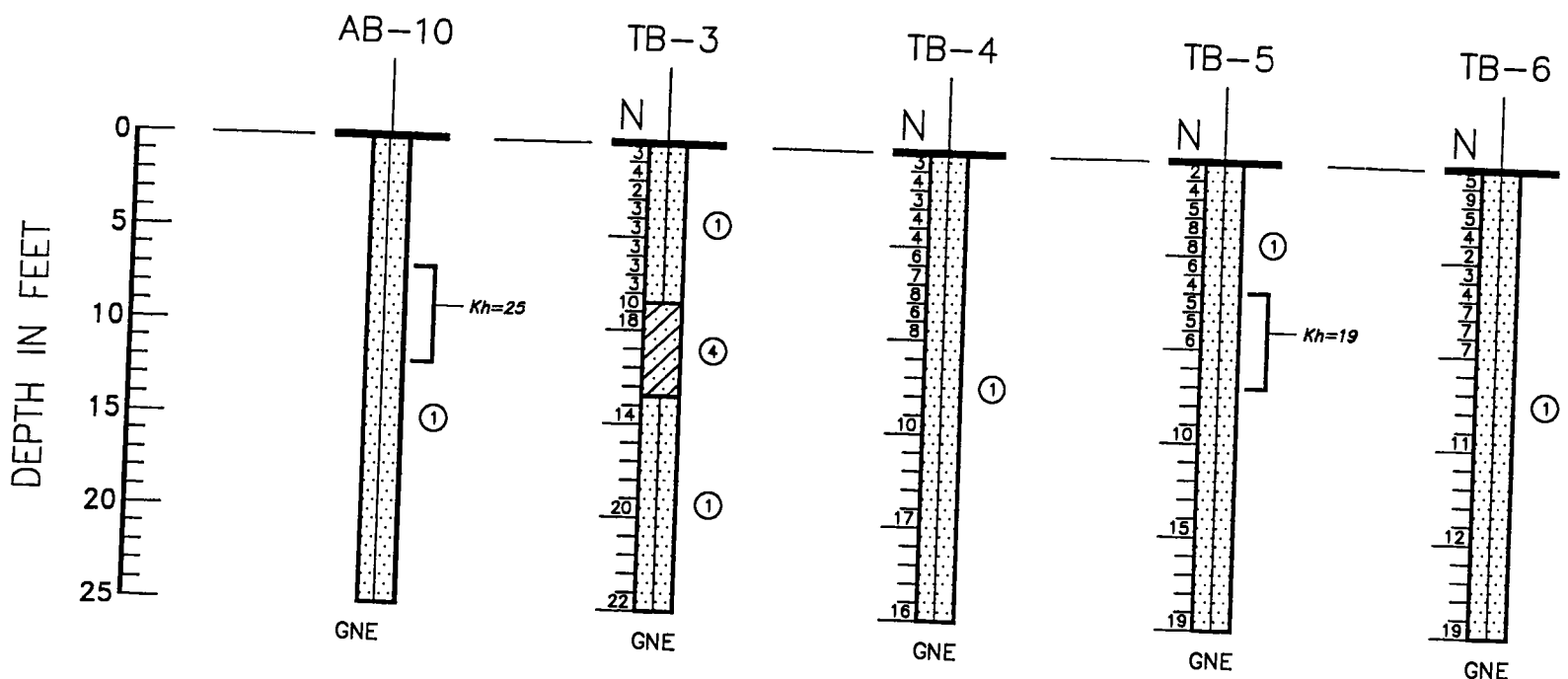
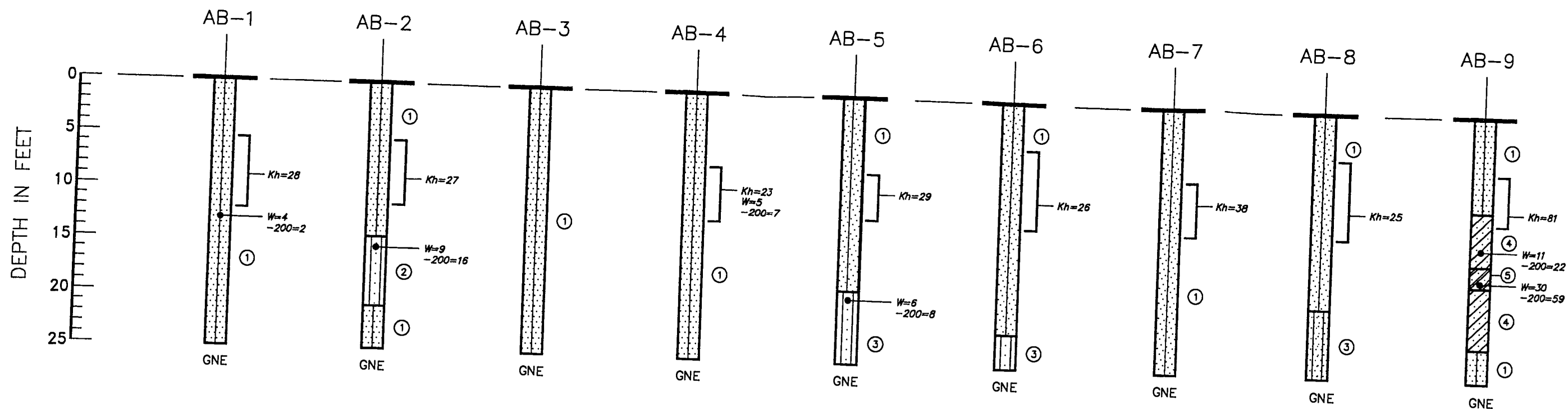
FIGURE 1



**LEGEND**


- LOCATION OF AUGER BORING
- ⊕ LOCATION OF SPT BORING (DRILLED 11/96)

 <b>Andreyev Engineering, Inc.</b>	GEOTECHNICAL INVESTIGATION LAKE LOUISA CLUB LAKE COUNTY, FLORIDA	
	LOCATION PLAN FIGURE 2	
DATE: 4-11-97 ENGINEER: DJR	SCALE: 1"=600' PN: PGT-96-165	



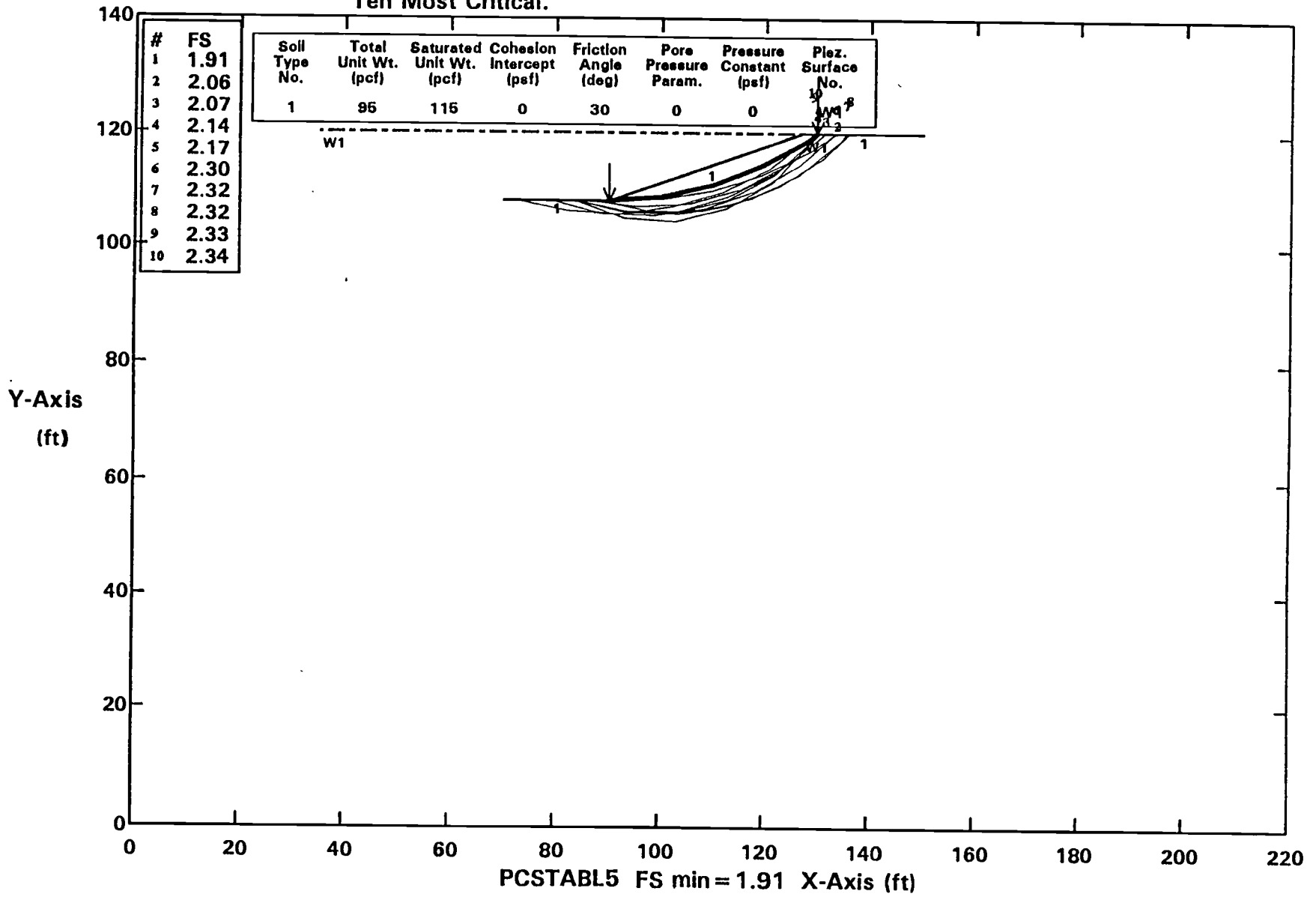
**LEGEND**

- ① BROWN TO REDDISH BROWN FINE SAND TO FINE SAND WITH SILT (SP) (SP-SM)
- ② REDDISH BROWN SILTY FINE SAND (SM)
- ③ LIGHT BROWN TO REDDISH BROWN FINE TO MEDIUM SAND (SP)
- ④ REDDISH BROWN TO GRAY CLAYEY FINE SAND (SC)
- ⑤ GRAY SANDY CLAY (CH)
- (SP) UNIFIED SOIL CLASSIFICATION GROUP SYMBOL
- N STANDARD PENETRATION RESISTANCE IN BLOWS PER FOOT
- W NATURAL MOISTURE CONTENT, IN PERCENT
- 200 PERCENT OF FINES PASSING THE U.S. No. 200 SIEVE
- Kh HORIZONTAL COEFFICIENT OF PERMEABILITY, IN FEET PER DAY
- GNE GROUNDWATER LEVEL NOT ENCOUNTERED TO MAXIMUM DEPTH OF BORING

 <b>Andreyev Engineering, Inc.</b>	GEOTECHNICAL INVESTIGATION LAKE LOUISA CLUB LAKE COUNTY, FLORIDA	
	DATE: 4-11-97 ENGINEER: DJR	SCALE: 1"=10' PN: PGT-96-165

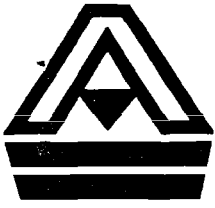
**APPENDIX A**

Ten Most Critical.



**GEOTECHNICAL  
INVESTIGATION OF  
LEGENDS SUDIVISION  
Clermont  
Lake County, Florida**





# Andreyev Engineering, Inc.

**SANFORD OFFICE**  
105 Coastline Road  
Sanford, Florida 32771  
407-330-7763  
Fax: 407-330-7765  
Email: [ANDENGI@AOL.COM](mailto:ANDENGI@AOL.COM)

▼ Groundwater ▼ Environmental ▼ Geotechnical ▼ Construction Materials Testing

July 22, 1998  
Project No: TPGT 98-061

**TO:** Lennar Homes  
c/o Farner Barley & Associates, Inc.  
350 North Sinclair  
Tavares, Florida 32778

**Attention:** Duane Booth, P.E.

**SUBJECT:** Geotechnical Investigation of Legends Subdivision, Stormwater Retention Systems,  
Clermont, Lake County, Florida

Dear Mr. Booth

As requested, Andreyev Engineering, Inc. (AEI) has completed a geotechnical investigation for the subject site. The following report presents the results of our field and laboratory investigation along with evaluation and recommendations for the proposed site.

## **SITE LOCATION AND DESCRIPTION**

The subject site property is located just south of Clermont on the west side of U.S. 27 across from the KingsRidge Subdivision. We understand that the property will be used for residential development. Approximately twenty (20) stormwater retention areas associated with the proposed development will be located as shown on the attached site plan labeled **Figure 1**.

## **PURPOSE AND SCOPE OF SERVICES**

The purpose of this study was to explore shallow subsurface conditions at the proposed retention areas to determine the suitability for stormwater retention. The field exploration consisted of drilling twenty-five (25) auger borings to depths of 10 to 20 feet within the proposed retention areas. In addition, twenty-one (21) field permeability tests and three (3) laboratory permeability tests were conducted at selected borings in order to measure the hydraulic conductivity of the soils.

Field permeability tests were conducted at selected borings within the proposed retention pond areas to measure the horizontal hydraulic conductivity of the soils. These tests were conducted by installing a screen PVC piezometer in the ground to varying depths between 10 and 20 feet below the ground surface, and conducting a constant head field permeability test, per designation E-19, Earth Manual, 1974. The results of these tests are shown adjacent to the sampled depth interval on Figures 2 & 3.

In order to measure the vertical hydraulic conductivity of the shallow soils within both proposed retention ponds, undisturbed tube sample were extracted from varying depths at borings AB-31, AB-32 and AB-34. The coefficient of permeability was measured in our laboratory using a falling head test. The results of these tests are shown adjacent to the sampled depths on Figure 3.

Samples were recovered from the borings and returned to AEI 's laboratory for visual classification and stratification. Soil strata were classified according to the Unified Soil Classification System. Approximate boring locations are shown on Figure 1 and results of the borings in profile form are presented on Figures 2 & 3. Also shown on Figures 2 & 3 next to the tested depths are the results of the permeability testing. On the profiles, horizontal lines designating the interface between differing materials represent approximate boundaries. The actual transition between layers is typically gradual.

#### **SUBSURFACE CONDITIONS**

Five (5) soil strata were identified in the borings. Strata 1 and 2 were the predominant surficial soils extending from the ground surface to the boring termination depths. Stratum 3, slightly clayey to clayey fine sand, was found at varying depths between 5 and 20 foot below ground surface. Stratum 4, slightly silty to silty fine sand, was also found at sporadic depths between 5 and 20 feet below ground surface. Stratum 5, fine sand with dry muck and organic material, was found in borings AB-32 and AB-33 from the ground surface to about 1 foot below ground surface.

Field permeability tests measured the shallow soil hydraulic conductivity at the proposed retention areas. In general, soil hydraulic conductivity measured between 15 and 50 feet per day in the strata 1 and 2 sandy soils, 1 to 4 feet per day in the slightly clayey to clayey soils, and 5 to 12 feet per day

in the slightly silty to silty soils. Results of these tests are shown next to the tested depths and borings on Figure 2 & 3.

The groundwater table was not encountered in any of the borings except AB-18, AB-19, and AB-28 where the ground water levels were encountered at depths of 10, 6, and 10 feet, respectively. However, these water table measurements are believed to be perched groundwater above the Stratum 3 soils, which resulted from the heavy rainfall at the time of measurement. The actual groundwater table at this site is estimated to be well below the termination depths of the borings.

For purposes of design and evaluation of retention area recovery, it can be assumed that the seasonal high groundwater table exists at more than 20 feet below the ground surface. However, at the locations where clayey soils of Stratum 3 are present, the groundwater table should be assumed to occur at about 1.0 foot above the top of Stratum 3.

#### **EVALUATION AND RECOMMENDATIONS**

Based on the results of borings, field permeability tests, and laboratory permeability tests, we conclude that the site is suitable for construction and long-term performance of dry stormwater retention systems. Adequate separation between the bottom of the proposed ponds and the groundwater table should not be a problem, except for possible groundwater conditions. The well-drained and, highly permeable nature of the surficial soils, and deep ground water table should be well suited for dry stormwater retention areas. However, temporary perching is expected to occur above the Stratum 3 clayey soils.

To mitigate potential negative impact of perched groundwater conditions, it is recommended that the Stratum 3 clayey soils be excavated from beneath the pond bottom to allow a hydraulic connection to deeper more permeable soils below. Provided that an effective hydraulic connection is made to the lower permeable soil, the pond will operate under true groundwater levels and not perched conditions.

For analysis and design purposes the following aquifer characteristics should be used. These aquifer characteristics were determined from the results of the field and laboratory investigations:

Boring	Bottom of Aquifer *(ft) Without Excavation of Stratum 3	Bottom of Aquifer*(ft) With Excavation of Stratum 3	Estimated Perched Wet Season GWT *(ft)	Estimated Normal Seasonal High GWT *(ft)	Kh** (ft/day)	Kv** (ft/day)
AB-10	15		20	20	-	
AB-11	15		20	20	43	
AB-12	14	20	13.5	20	-	
AB-13	10		20	20	33	
AB-14	7	15	6	20	50	
AB-15	15		15	20	31	
AB-16	15		15	20	20	
AB-17	11	20	10	20	-	
AB-18	11.5	15	10.5	20	32	
AB-19	10	15	9	20	19	
AB-20	13	13	12	20	15	
AB-21	8	N/A	7	20	-	
AB-22	6.5	N/A	5.5	20	-	
AB-23	20		20	20	28	
AB-24	10		10	20	42	
AB-25	15		15	20	40	
AB-26	16	20	15	20	44	
AB-27	20		20	20	26	
AB-28	12	15	11	20	24	
AB-29	8	20	7	20	14	
AB-30	8	20	7	20	7	
AB-30	8	20	7	20	20	
AB-31	6	15	5	20	26	
AB-31	6	15	5	20	4	
AB-31	6	15	5	20		12
AB-32	7	10	6	20	23	
AB-32	7	10	6	20		15
AB-33	13	15	12	20	-	
AB-34	7	15	6	20	5	
AB-34	7	15	6	20		31

\*-depth below existing ground surface

\*\* - See depth of tests and test intervals on soil profiles, Figures 2 & 3.

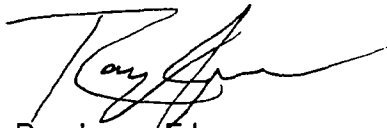
Specific Recommendations for the ponds corresponding to borings AB-14, AB-31, and AB-32 are as follows. Clayey material in the vicinity of AB-31 should be excavated from 6 to 12 feet below ground surface and replaced with clean fine sand. In the vicinity of AB-14, the clayey material should be excavated from 7 to 10 feet below ground surface and replaced with clean fine sand. Also, in order to provide effective infiltration in the area of AB-32, the clayey material and muck material should be over-excavated from ground surface to 6 foot below ground surface.

CLOSURE

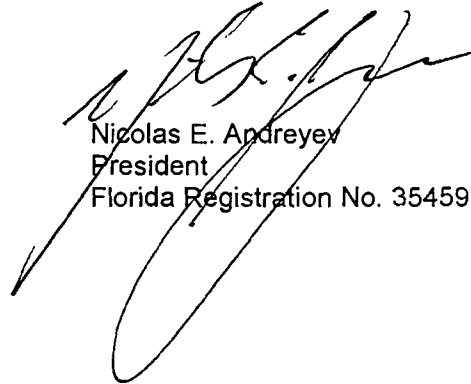
AEI appreciates the opportunity to participate in this project, and we trust that the information herein is sufficient for your immediate needs. If you have any questions or comments concerning the contents of this report, please do not hesitate to contact the undersigned.

Sincerely,

ANDREYEV ENGINEERING, INC.

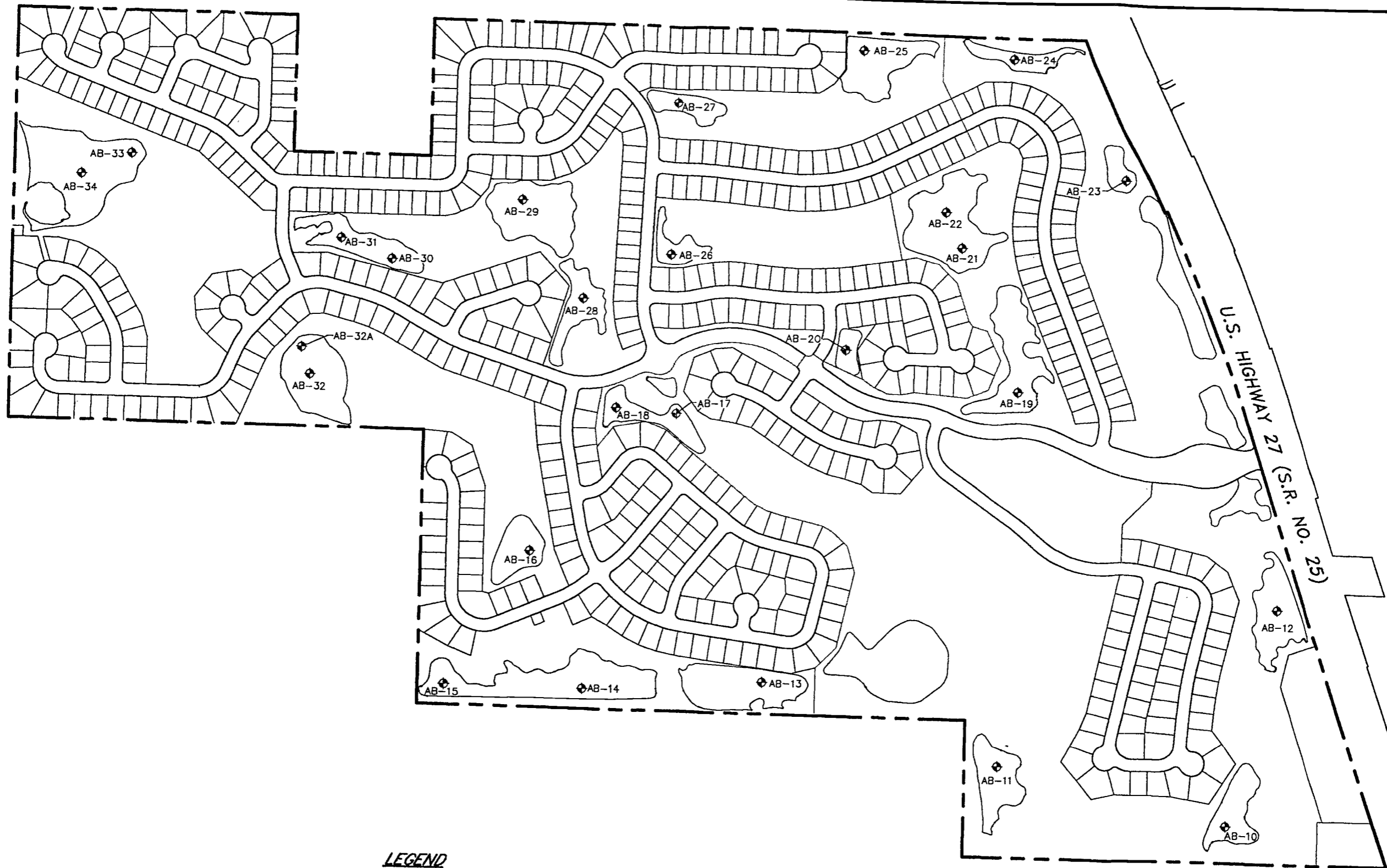


Ray Jones, E.I.  
Project Engineer  
Tavares Office



Nicolas E. Andreyev  
President  
Florida Registration No. 35459

## FIGURES



**LEGEND**  
◆ AUGER BORING LOCATION



**Andreyev  
Engineering,  
Inc.**

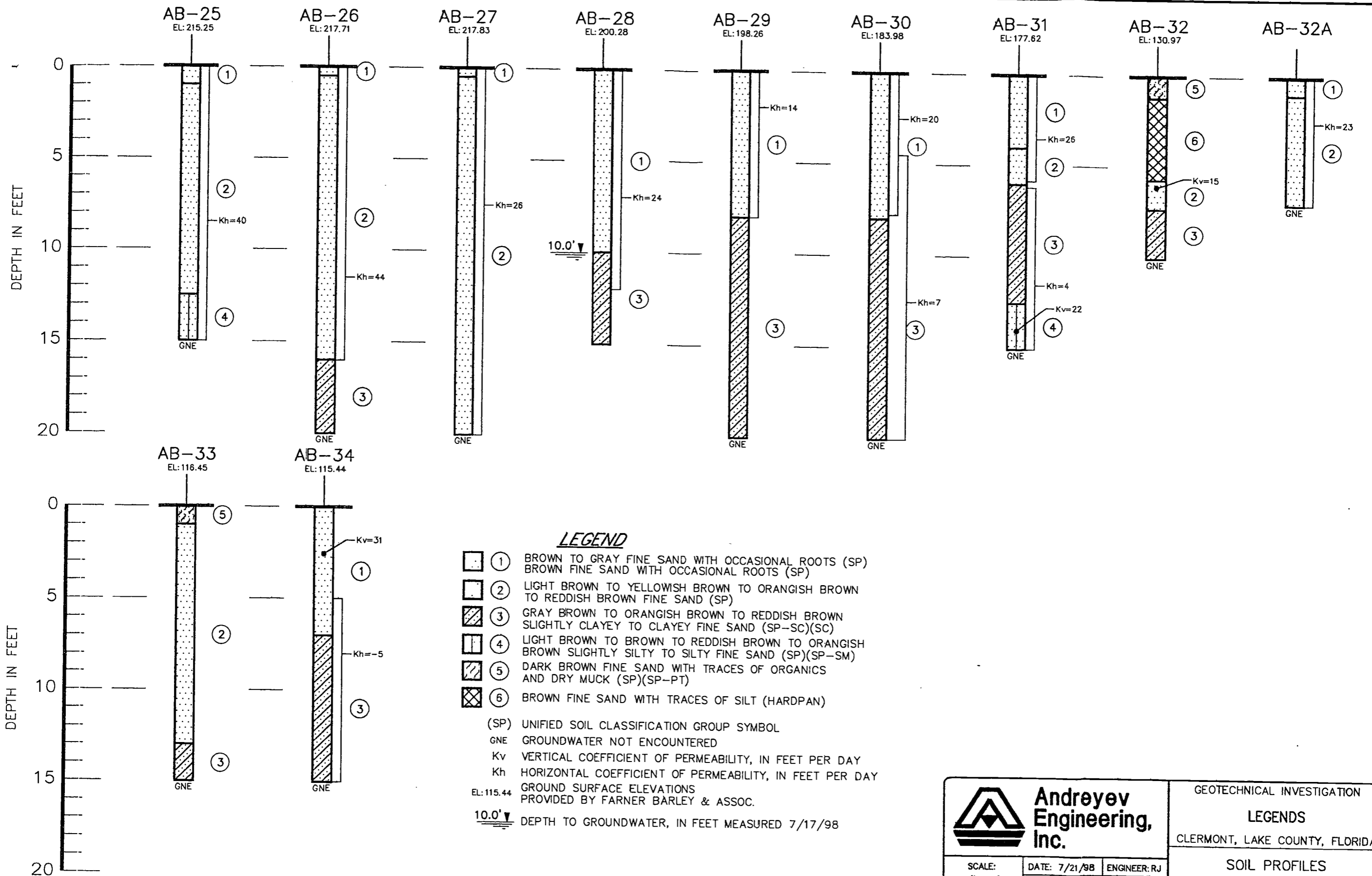
GEOTECHNICAL INVESTIGATION  
**LEGENDS**  
CLERMONT, LAKE COUNTY, FLORIDA

SCALE:  
1" = 500'

DATE: 7/22/98  
PN: TPGT-98-061

ENGINEER: RJ  
DRAWN BY: MK

**SITE PLAN**  
FIGURE 1



		GEOTECHNICAL INVESTIGATION <b>LEGENDS</b> CLERMONT, LAKE COUNTY, FLORIDA	
		SOIL PROFILES FIGURE 3	
SCALE: 1" = 5'	DATE: 7/21/98 PN: TPGT-98-061	ENGINEER: RJ DRAWN BY: MK	





# Andreyev Engineering, Inc.

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▼ Groundwater ▼ Environmental ▼ Geotechnical ▼ Construction Materials Testing

July 28, 1998

Mr. Duane Booth  
FARNER-BARLEY & ASSOCIATES  
350 North Sinclair Ave.  
Tavares, FL 32778

Re: Legends Subdivision, Clermont, Lake County, FL

Dear Duane,

Per our conversation, the bottom of aquifer for Boring AB-19 without excavation of Stratum 3 should be set at 6 feet below ground surface.

It is understood that the pond bottom will be set at 8 feet below the existing ground surface. Due to the low permeability Stratum 3 soils encountered, we recommend over-excavating the clayey material to a depth of 11 feet below ground surface and replacing it with clean fine sand. This should provide adequate buffer between the pond bottom and the Stratum 3 soils.

Further, our field permeability test was conducted from ground surface to a depth of 9.5 feet and the horizontal hydraulic conductivity measured 19 feet per day.

If you have any questions or if I may be of any further assistance, please do not hesitate to call.

Sincerely,

ANDREYEV ENGINEERING, INC.



Ray Jones, E.I.  
Project Manager

RJ/mls