# Waterbrooke Traffic Impact Study 

Prepared For:

## Mattamy Homes

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### 1.0 Introduction

This traffic impact study has been prepared to evaluate the impacts to the roadway network and intersections that may result from the development of the Waterbrooke residential project in Clermont, Florida. The project site is located south of SR 50 at Emil Jahna Road (see Figure 1.1), in southeastern Lake County, and will be incorporated into the City of Clermont.

The proposed development is planned to include $771 \pm$ single-family homes and $302 \pm$ townhomes/duplexes, for a total of 1,073 dwelling units. However, for the purposes of this analysis, the development will be analyzed as 1,100 single-family dwelling units to allow for minor changes in product offerings as plans are finalized for the development. The development will also contain an amenity center and park for exclusive use of the community residents. Build-out of the development is expected by 2025, with approximately $80-150$ homes constructed per year.

The site originally included a sand mine, and there are two lakes within the property, which are the former borrow pits from the previous mining activities. In 2006, the site was approved for an age-restricted residential planned unit development. Two additional traffic impact studies have been completed for this development. The initial study (August 2013) analyzed the proposed development with 894 residential units and a single connection to SR 50 via Emil Jahna Road. The second study increased the number of dwelling units to 950 as well as added additional access to SR 50 via a realigned/extended Hartle Road, and no age restrictions on the residential units. This study builds upon the previous analysis to increase the total number of dwelling units to 1,073 and add an access to Hancock Road.

The proposed development will be developed in six phases (see Figure 1.2). The first three phases are located north of the larger of the two lakes/borrow pits, and will have access to SR 50 via Emil Jahna Road and Hartle Road ( 599 dwelling units). The fourth phase is located south of the large lake, between the powerline easement and Hartle Road ( 68 dwelling units). The fifth phase is located between Hancock Road and the powerline easement ( 272 dwelling units). Two access scenarios will be analyzed for the fourth and fifth phases - one scenario where both portions of the development can access both Hancock Road and Hartle Road, and one where only an emergency-access is provided across the powerline easement (loading all of the fourth phase onto Hartle Road and all of the fifth phase onto Hancock Road). The sixth phase is located east of Hartle Road and will access Hartle Road only (134 dwelling units). As the communities are planned to be gated, there is no cut-through assumed from the properties in Phases 4-6 in order to access Emil Jahna Road. However, the residential areas will be connected by an internal sidewalk/bicycle path system.


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Figure 1.2 - Project Phases


### 2.0 Existing Conditions

### 2.1 Data Collection

As per the methodology approved by Lake-Sumter MPO staff, data from the previous study was utilized for the three study intersections along SR 50, and collected for the three study intersections on Johns Lake Road.

- SR 50 @ Hancock Road
- SR 50 @ Emil Jahna Road
- SR 50 @ Hartle Road

■ Johns Lake Road @ US 27
■ Johns Lake Road @ Citrus Tower Boulevard
■ Johns Lake Road @ Hancock Road
As this is planned as a residential community, turning movement counts for each of the intersections were collected for both the AM (7-9 AM) and PM (4-6 PM) peak periods on August 12, 2015 (SR 50) and May 11, 2016 (Johns Lake Road). The turning movement counts are included in Appendix A.

The volumes for each of these intersections recorded during field data collection are shown on Figure 2.1. Before any analysis was conducted, the turning movement counts were adjusted based on the Seasonal Factor in the Peak Season Factor Category Report using a factor of 1.06 for the SR 50 counts and 1.00 for the Johns Lake Road counts (a copy of this report is included in Appendix B).

### 2.2 Intersection Analysis

Each of the existing study intersections were evaluated with the existing geometrics and signal timings using Synchro 8 (existing signal timing information is included in Appendix C). Per the Lake County and City of Clermont Comprehensive Plans, the minimum LOS standard for all roadways which are not on the Strategic Intermodal System/Florida Intrastate Highway System is LOS D, which was applied to the intersection analysis as well. The results of that analysis indicate that the intersections of SR 50/Emil Jahna Road, SR 50/Hartle Road, Citrus Tower Boulevard/Johns Lake Road, and Hancock Road/Johns Lake Road operate at an acceptable overall level of service during both peak periods, although there are movements at most of these intersections which do not meet the level of service standard. The intersection of SR 50/Hancock Road does not meet the level of service standard overall, or for any movements other than the westbound approach, in both the AM and PM peak period. This is due to high through volumes on SR 50 as well as high volumes on the minor street approaches. The intersection of US 27/Johns Lake Road does not meet the minimum LOS standards in the AM Peak Period, overall and on the approaches, due to the fact that the LOS standard is LOS C for state highways. A LOS C standard is difficult to achieve for signalized intersections in an urban environment, as the major through movements can generally only have a green time of $50-70 \%$ of the $100+$ second cycle length.


However, as the average vehicular delay on the approaches is generally within between 50-80\% of the cycle length for these intersections, all vehicles should be able to clear the intersection within one cycle during the peak periods. Details of the intersection analysis results are shown in Table 2.1 and copies of the Synchro analysis printouts are included in Appendix D.

Table 2.1 - Existing Intersection Level of Service

| Intersection | Stop Control | Intersection Conditions | Approach |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Overall | EB | WB | NB | SB |
| AM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | E | E | D | F | E |
|  |  | Delay (sec/veh) | 67.2 | 76.7 | 42.7 | 85.7 | 74.0 |
| SR 50 @ Emil Jahna Rd | Signal | LOS | B | B | A | A | E |
|  |  | Delay (sec/veh) | 10.3 | 10.1 | 6.7 | 0.0 | 76.0 |
| SR 50 @ Hartle Rd | Signal | LOS | C | C | C | F | F |
|  |  | Delay (sec/veh) | 34.1 | 29.7 | 21.6 | 84.7 | 84.0 |
| US 27 @ Johns Lake Rd | Signal | LOS | D | E | D | D | D |
|  |  | Delay (sec/veh) | 50.7 | 64.0 | 50.9 | 49.9 | 48.1 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | C | D | C | C |
|  |  | Delay (sec/veh) | 30.0 | 34.8 | 40.6 | 28.8 | 20.5 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | D | E | C | D |
|  |  | Delay (sec/veh) | 38.0 | 46.0 | 69.8 | 29.6 | 43.6 |
| PM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | E | E | D | F | E |
|  |  | Delay (sec/veh) | 61.1 | 56.7 | 52.2 | 98.6 | 79.8 |
| SR 50 @ <br> Emil Jahna Rd | Signal | LOS | B | A | B | A | E |
|  |  | Delay (sec/veh) | 10.6 | 8.6 | 10.4 | 0.0 | 76.7 |
| $\text { SR } 50 @$Hartle Rd | Signal | LOS | D | B | C | F | F |
|  |  | Delay (sec/veh) | 36.6 | 18.3 | 29.2 | 112.1 | 161.5 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | E | E | C | C |
|  |  | Delay (sec/veh) | 34.9 | 62.4 | 64.9 | 28.8 | 29.9 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | C | C | C | B |
|  |  | Delay (sec/veh) | 22.0 | 30.4 | 30.3 | 21.0 | 17.9 |
| Hancock Road @ Johns Lake Road | Signal | LOS | C | E | F | B | C |
|  |  | Delay (sec/veh) | 33.6 | 74.8 | 86.2 | 18.2 | 23.6 |

Source: Littlejohn Engineering Associates

### 2.3 Existing Roadway Analysis

The existing AADT, peak-hour volumes, and committed trips for the roadways in the study area were compiled from the Lake-Sumter MPO Lake County Transportation Management System Segment Report, dated April 3, 2015, the 2016 Lake County Traffic Count Database, and FDOT's 2014 Florida Transportation Information (FTI). Based on the data provided in the 2016 Lake County Traffic Count Database, an average annual growth rate of $3.0 \%$ county-wide was calculated from data from 2013 and 2016, and thus the FDOT data was grown at a $3.0 \%$ rate from the 2013 count data provided in the 2014 FTI to match the 2016 data from Lake County. Using the Level of Service

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thresholds published within the segment report, the existing level of service for each roadway was determined (based on existing trips). The results of that analysis are shown on Table 2.2.

Table 2.2 - Existing Roadway Segment Analysis

| Roadway | Segment | $\begin{aligned} & \text { LOS } \\ & \text { Std } \end{aligned}$ | LOS Capacity | AADT | $\begin{aligned} & \text { Pk } \\ & \text { Dir } \end{aligned}$ | Pk Hr/ <br> Pk Dir <br> Existing | v/c | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 50 | CR 561 to East Ave | D | 2,000 | 34,421 | WB | 1,688 | 0.84 | C |
|  | East Ave to US 27 | D | 3,020 | 43,709 | WB | 2,144 | 0.71 | C |
|  | US 27 to Hancock Road | D | 3,020 | 44,255 | WB | 2,171 | 0.72 | C |
|  | Hancock Road to Emil Jahna Rd | D | 3,020 | 56,275 | WB | 2,760 | 0.91 | C |
|  | Emil Jahna Rd to CR 455 | D | 3,020 | 56,275 | WB | 2,760 | 0.91 | C |
|  | CR 455 to Orange County Line | D | 3,020 | 47,534 | WB | 2,332 | 0.77 | C |
| US 27 | Grand Hwy to SR 50 | C | 2,940 | 27,865 | NB | 1,367 | 0.46 | C |
|  | SR 50 to Johns Lake Rd | C | 2,940 | 37,153 | SB | 1,822 | 0.62 | C |
|  | Johns Lake Rd to Hartwood Marsh Rd | C | 2,940 | 33,328 | NB | 1,635 | 0.56 | C |
|  | Hartwood Marsh Rd to Lake Louisa Rd | C | 2,940 | 22,947 | NB | 1,126 | 0.38 | C |
|  | Lake Louisa Rd to Boggy Marsh Rd | C | 2,940 | 24,586 | SB | 1,206 | 0.41 | C |
| Old Hwy 50 | US 27 to Turkey Farm Rd | D | 792 | 7,238 | WB | 378 | 0.48 | C |
|  | Turkey Farm Rd to CR 455 | D | 792 | 5,592 | EB | 448 | 0.57 | C |
|  | CR 455 to Orange County Line | D | 792 | 5,950 | WB | 513 | 0.65 | C |
| CR 455 | Ridgewood Ave to CR 455/CR 50 | D | 1,200 | 6,879 | SB | 331 | 0.28 | B |
|  | CR 455/CR 50 to SR 50 | D | 675 | 7,844 | NB | 398 | 0.59 | D |
| Citrus Tower Boulevard | US 27 to Oakley Seaver Dr | D | 792 | 12,177 | SB | 601 | 0.76 | C |
|  | Oakley Seaver Dr to SR 50 | D | 1,800 | 16,110 | NB | 692 | 0.38 | C |
|  | SR 50 to Hooks St | D | 1,800 | 17,355 | SB | 834 | 0.46 | C |
|  | Hooks St to Johns Lake Rd | D | 1,800 | 18,431 | SB | 922 | 0.51 | C |
|  | Johns Lake Rd to US 27 | D | 1,800 | 14,579 | SB | 713 | 0.40 | C |
| Hancock Road | CR 50 to Ridge Blvd | D | 1,800 | 11,023 | SB | 472 | 0.26 | C |
|  | Ridge Blvd to SR 50 | D | 1,800 | 14,533 | NB | 643 | 0.36 | C |
|  | SR 50 to Hooks St | D | 1,800 | 18,478 | SB | 932 | 0.52 | C |
|  | Hooks St to Johns Lake Rd | D | 792 | 18,478 | SB | 932 | 1.18 | F |
|  | Johns Lake Rd to Hartwood Marsh Rd | D | 792 | 8,483 | SB | 405 | 0.51 | C |
| Hartwood Marsh Road | US 27 to Hancock Road | D | 675 | 14,102 | SB | 771 | 1.14 | F |
|  | Hancock Road to 90 Degree Bend | D | 675 | 10,247 | NB | 720 | 1.07 | F |
|  | 90 Degree Bend to Orange County Line | D | 675 | 10,247 | NB | 720 | 1.07 | F |

Table 2.2 con't. - Existing Roadway Segment Analysis

| Roadway | Segment | $\begin{aligned} & \text { LOS } \\ & \text { Std } \end{aligned}$ | LOS Capacity | AADT | $\begin{aligned} & \text { Pk } \\ & \text { Dir } \end{aligned}$ | Pk Hr/ <br> Pk Dir <br> Existing | v/c | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lake Louisa Road | Lakeshore Dr to Vista Del Lago Blvd | D | 675 | 3,456 | NB | 163 | 0.24 | C |
|  | Vista Del Lago Blvd to US 27 | D | 675 | 4,044 | SB | 301 | 0.45 | C |
| Grand Highway | Citrus Tower Blvd to SR 50 | D | 675 | 6,436 | NB | 309 | 0.46 | C |
|  | SR 50 to Hooks St | D | 1,800 | 6,292 | SB | 303 | 0.17 | C |
| Hooks Street | Lakeshore Dr to US 27 | D | 675 | 7,007 | EB | 347 | 0.51 | D |
|  | US 27 to Oakley Seaver Dr | D | 1,800 | 9,512 | WB | 396 | 0.22 | C |
|  | Oakley Seaver Dr to Citrus Tower Blvd | D | 1,800 | 9,367 | WB | 398 | 0.22 | C |
|  | Citrus Tower Blvd to Hancock Rd | D | 1,800 | 11,451 | WB | 603 | 0.34 | C |
| Anderson Hill Road | Lakeshore Dr to US 27 | D | 675 | 1,584 | EB | 105 | 0.16 | C |
| East Avenue | CR 561 to SR 50 | D | 675 | 5,103 | WB | 286 | 0.42 | C |
| Hammock Ridge Road | Lakeshore Dr to US 27 | D | 1,800 | 15,472 | WB | 921 | 0.51 | C |
| Lakeshore Drive | Hammock Ridge Road to Anderson Hill Rd | D | 675 | 7,500 | EB | 416 | 0.62 | D |
| Turkey Farm Road | E Grassy Lake Road to CR 50 | D | 675 | 344 | EB | 22 | 0.03 | C |
| Johns Lake Road | US 27 to Hancock Road | D | 675 | 8,489 | EB | 390 | 0.58 | D |
| Blackstill Lake Road | Fosgate Rd to CR 50 | D | 612 | 3,135 | SB | 156 | 0.25 | C |

Source: Lake Sumter MPO TMS Report for Lake County, April 5, 2015 (LOS Standards/Roadway Capacity) Lake County 2016 Master Roadway Count Table (AADT for non-state/federal roadways) FDOT Florida Transportation Information 2014 (AADT for state/federal roadways, grown to 2016)

With only existing trips, there are four segments within the study area which do not meet the LOS standard for the roadway:

■ Hancock Road: Hooks Street to Johns Lake Road
■ Hartwood Marsh Road: US 27 to Hancock Road
■ Hartwood Marsh Road: Hancock Road to 90 Degree Bend

- Hartwood Marsh Road: 90 Degree Bend to Orange County Line

There are no current plans within the Lake-Sumter MPO Long Range Transportation Plan (Cost Feasible Projects) and/or Transportation Improvement Program to provide any capacity improvements on any of the deficient roadways.

### 3.0 Proposed Development Plan

### 3.1 Development Program

The proposed development program for the Waterbrooke development includes a total of 1,073 dwelling units ( 771 single-family dwelling units, 302 townhomes). However, for the purposes of this analysis, the development will be analyzed as 1,100 single-family dwelling units. This will allow for the maximum flexibility in product types offered within the development (i.e. - single family, townhome, duplex, senior adult) as plans for each phase are finalized, as single-family has the highest trip generation of any of the proposed uses. Thus, as long as the final development does not exceed 1,100 dwelling units, the impacts from the proposed development are included within this study.

### 3.2 Site Access \& Circulation

Access for the site will be provided from Emil Jahna Road, Hartle Road, and Hancock Road. There are a few features within the subject property which divide the development - the large lake/borrow pit, a powerline easement, and the extension of Hartle Road. The first three phases are all located on the north side of the largest lake/borrow pit, the fourth and fifth phases are located south of the lake/borrow pit between Hancock Road and Hartle Road, and the sixth phase is located east of Hartle Road (as is shown in Figure 1.2). The development north of the largest lake/borrow pit (phases 1-3) will have access to both Emil Jahna Road and Hartle Road. The development within Phase 6 will only have access to Hartle Road. The development within Phases 4 and 5 will be analyzed with two options for access - with both phases having access to both Hancock Road and Hartle Road and with only an emergency access between Phases 4 and 5 (and thus access to Phase 4 provided via Hartle Road, and access to Phase 5 provided via Hancock Road).

The study was also analyzed with two options for Emil Jahna Road. Within each build-out scenario, Emil Jahna Road was analyzed as both a two-lane roadway (Option 1) and as a four lane roadway (Option 2).

The development is proposed to be gated, and thus cut-through traffic between the various phases of development will not be permitted. However, there will be bicycle/pedestrian pathways linking the various development areas.

### 4.0 Trip Generation \& Assignment

### 4.1 Project Traffic Estimates

The traffic estimates for the project were developed using the information contained in the ITE Trip Generation Manual, $9^{\text {th }}$ Edition, using ITE Code 210 'Single Family Residential' for all dwelling units, as it produces the higher trip generation and thus will allow for minor variations in the proportion of each type of units provided as the final site plans are determined. These estimates were prepared to represent both the trips that will occur at the project driveways (inbound and outbound) for both the AM and PM peak-hour periods and for the net new trips that will be added to the external roadway network. The result of the trip generation estimation exercise is shown below in Table 4.1.

Internal trips are those which begin and end within the project site. External trips have either an origin or destination outside the project site. There will be no internal capture assumed for the proposed development, as the entire development is planned residential. Pass-by trips come directly from the traffic stream passing the facility on the adjacent street system and do not require a diversion from another roadway. Likewise, as the entire development is planned as residential, no pass-by is assumed for this project. No transit reduction will be assumed for this project, as there are no transit routes near the proposed development.

Table 4.1 - Trip Generation

| Land Use | $\begin{aligned} & \text { ITE } \\ & \text { Code } \end{aligned}$ | Intensity | Daily <br> Trip <br> Ends | Peak <br> Period | Total | In |  | Out |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | \% | Trips | \% | Trips |
| Single- |  |  |  | AM | 780 | 25\% | 195 | 75\% | 585 |
| Family | 210 | 1,100 DU | 9,536 | PM | 909 | 63\% | 573 | 37\% | 336 |

Source: ITE Trip Generation Manual, $9^{\text {th }}$ Edition

### 4.2 Trip Distribution

The proposed project was added into the currently approved Central Florida Regional Planning Model (CFRPM, v5.01) as three new TAZs, one with connections to Emil Jahna Road and Hartle Road, one with connections just to Hartle Road, and the last with connections to Hancock Road and Hartle Road. Both Emil Jahna Road and Hartle Road were added to the network as necessary. The model was run to determine the distribution of project trips onto the roadway network from the new development for the two scenarios. Print-outs of the model distribution are shown in

## Appendix E.

Both scenarios resulted in similar global distributions, with approximately $60 \%$ of the project trips to the east/northeast of the site, $25 \%$ of the project trips to the north/northwest, $10 \%$ to the south/southwest, and $5 \%$ in the TAZs near the project site. Based on the regional distribution of employment and attractions, this is a reasonable assignment.

Project trips were assigned to the site access points based on intensity of development within the various phases of development and the allowed access from each phase, the direction of travel to and from the site, as well as engineering judgment. The model distribution on the roadway network between project access points (i.e. - Hancock Road between SR 50 and the project access and SR 50 between Hancock Road and Hartle Road) was updated based on the projected distribution of project trips between access points. All project traffic was assumed to use the first access point encountered that provides access to the correct area of the development, except for trips from Phases 1-3 and locations east along SR 50. For purposes of analysis, it was assumed that the trips to/from SR 50 east of Hartle Road from Phases 1-3 would be split 50\%/50\% between Emil Jahna Road and Hartle Road, as the majority of parcels would have more direct access from Emil Jahna Road, although the Hartle Road access is "first" and may have less traffic. The distribution of project trips onto the regional roadway network is shown on Figure 4.1 and Figure

## 4.2.

### 4.3 Background Traffic Growth

The future analysis year for the proposed development is 2025. Background traffic volumes for the AM peak period intersection analysis were determined by growing the existing traffic volumes by 1\% per year (from 2015/16 to 2025). The committed trips for each roadway segment were added to the existing counts to determine the future PM roadway volumes, and applied to the intersections for the PM peak period intersection analysis. Generally, committed trips on the approach segment were applied to the intersections at a ratio of the existing turning movement volumes, although some adjustments were made to better match the committed trips on the departure segment (such as at SR 50/Hancock Road, where there are more northbound committed trips leaving the intersection than southbound committed trips)

### 4.4 Projected Future Traffic

The projected project trips on each segment and intersection turning movement were added to the projected background/committed trips at each of the study locations in order to determine the total future roadway segment and intersection turning movement volumes. The projected future turning movement volumes are shown on Figure 4.3 - Figure 4.6.



Figure 4.3
Build-Out Intersection Volumes - Scenario 1 AM





### 5.0 Evaluation

The post development condition was evaluated based on the anticipated addition of project traffic and a modest amount of growth in background traffic. These analyses were conducted assuming no roadway or intersection improvements (with the exception of site access connections) will be made to any of the study area roadways or intersections.

### 5.1 Future Intersection Analysis - No-Build

The projected background trips and committed trips (on SR 50) were analyzed as the no-build scenario for the study area intersections using Synchro 8. The results of this evaluation is shown on Table 5.1 with the printouts of the analysis shown in Appendix F. As this study covers a 10year period with significant additional proposed development outside of the project site, it was assumed that the signals on this corridor would be retimed/coordinated to better serve the adjustments for the future traffic patterns.

Table 5.1 - Future Intersection Level of Service - No-Build

| Intersection | Stop Control | Intersection Conditions | Approach |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Overall | EB | WB | NB | SB |
| AM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | E | D | D | F | E |
|  |  | Delay (sec/veh) | 56.7 | 53.5 | 35.4 | 109.5 | 72.2 |
| SR 50 @ Emil Jahna Rd | Signal | LOS | B | B | A | A | D |
|  |  | Delay (sec/veh) | 13.9 | 15.6 | 8.4 | 0.0 | 49.4 |
| SR 50 @ <br> Hartle Rd | Signal | LOS | D | D | C | F | F |
|  |  | Delay (sec/veh) | 45.4 | 46.9 | 22.2 | 94.9 | 93.5 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | D | C | D | C |
|  |  | Delay (sec/veh) | 32.5 | 46.0 | 34.0 | 39.8 | 22.1 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | D | D | C | C |
|  |  | Delay (sec/veh) | 34.2 | 40.2 | 48.4 | 32.1 | 22.5 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | E | E | C | D |
|  |  | Delay (sec/veh) | 39.8 | 62.1 | 73.6 | 29.3 | 38.5 |
| PM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | F | F | F | F | F |
|  |  | Delay (sec/veh) | 194.6 | 113.2 | 237.7 | 169.9 | 215.7 |
| SR 50 @ <br> Emil Jahna Rd | Signal | LOS | C | B | C | A | E |
|  |  | Delay (sec/veh) | 25.3 | 10.6 | 34.4 | 0.0 | 65.6 |
| SR 50 @ Hartle Rd | Signal | LOS | F | C | F | F | F |
|  |  | Delay (sec/veh) | 114.9 | 33.0 | 121.4 | 135.4 | 364.4 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | E | D | D | C |
|  |  | Delay (sec/veh) | 34.2 | 55.3 | 48.3 | 41.6 | 22.9 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | D | D | B | B |
|  |  | Delay (sec/veh) | 23.3 | 53.9 | 48.3 | 14.8 | 12.9 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | E | E | C | D |
|  |  | Delay (sec/veh) | 43.0 | 56.0 | 73.5 | 26.3 | 51.5 |

Source: Littlejohn Engineering Associates

The results of the analysis indicate there are significant delays in the no-build scenario, with the intersections of SR 50/Hancock Road and SR 50/Hartle Road not meeting the LOS standards overall and on most movements in the PM peak period and the minor street approaches not meeting the LOS standards in the AM peak period. Due to significantly high projected volumes on SR 50 (existing + committed trips), there is simply not sufficient green time available to serve the minor street approaches and major street left-turn movements. It should be noted that the programmed Turnpike interchange in Minneola may serve to reduce volumes on SR 50, as it is anticipated to divert a significant amount of traffic from the existing interchange on SR 50 in the Town of Oakland. These intersections are effectively "built-out" with turn lanes, leaving a solution of finding additional capacity at the intersections by widening SR 50 or an equivalent alternative.

While the intersection of US 27/Johns Lake Road does not meet the level of service standards for a roadway on the State Highway System (LOS C), the delays at this intersection are typical of an intersection in an urban environment, with average delays of up to 61.5 seconds throughout the movements.

An analysis of the $95^{\text {th }}$ percentile queue length of each of the turn lanes into and out of the site are shown in Table 5.2. Based on the queue lengths shown in the analysis, all turn lanes into and out of the site have sufficient length for the $95^{\text {th }}$ percentile queue and deceleration length, other than the westbound left-turn onto Hartle Road, which does not meet the required length by 8 feet. However, as this turn lane has 240 feet of deceleration length, this is not a substantial deficiency.

Table 5.2 - Queue Analysis - No-Build

| Intersection | Stop Control | Lane | $\begin{gathered} \text { Existing Lane } \\ \text { Length (ft) } \end{gathered}$ | 95 ${ }^{\text {tho }} \%$ Queue Length (ft) | Required dece length ${ }^{1}$ (ft) | Total length required (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | WB Left | 320 | 42 | 240 | 282 |
|  | Signal (Option 2) | WB Left | 320 | 42 | 240 | 282 |
| SR 50 @ Hartle Rd | Signal | EB Right | 480 | 7 | 240 | 247 |
|  |  | WB Left | 290 | 58 | 240 | 298 |
|  |  | NB Left | 120 | 95 | 0 | 95 |
|  | Signal (Improved) | EB Right | 480 | 7 | 240 | 247 |
|  |  | WB Left | 290 | 58 | 240 | 298 |
|  |  | NB Left | 120 | 95 | 0 | 95 |

${ }^{1}$ Does not include required taper length
Source: Littlejohn Engineering Associates

### 5.2 Future Intersection Analysis - Scenario 1

The combined background, committed (for SR 50), and project trips were analyzed for the Scenario 1 access using Synchro 8. The results of these evaluations are shown in Table $\mathbf{5 . 3}$ with the printouts of the analysis shown in Appendix G. As was completed for the no-build analysis, the traffic signals were retimed/optimized as it can be expected that retiming will occur over the next 10 years. The intersection of SR 50/Emil Jahna Road was analyzed with two options, with Option 1 being an improved two-lane roadway (bringing the roadway up to modern design standards) and Option 2 being a 4-lane roadway. All of the project access intersections operate within the level of service standards. Most of the deficiencies shown in Scenario 1 also operate below the level of service standard in the no-build condition, and thus are not the responsibility of the proposed development. All deficiencies on SR 50 are caused by high through movements on SR 50 which limit the available green time for turning movements and minor street approaches. Capacity improvements which would be necessary to serve the background traffic (widening to 8 lanes or equivalent improvement) would mitigate the traffic for the build-out scenarios as well. Additionally, the completion of the new Turnpike interchange in Minneola may offer some relief to SR 50 and lessen the demand on the through movements, improve the length of delays.

Table 5.3 - Future Intersection Level of Service - Scenario 1

| Intersection | Stop Control | Intersection Conditions | Approach |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Overall | EB | WB | NB | SB |
| AM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | E | D | D | F | E |
|  |  | Delay (sec/veh) | 61.2 | 52.6 | 39.3 | 139.3 | 77.7 |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | LOS | D | D | B | D | D |
|  |  | Delay (sec/veh) | 38.8 | 50.3 | 14.9 | 52.5 | 42.9 |
|  | Signal (Option 2) | LOS | C | C | B | D | D |
|  |  | Delay (sec/veh) | 23.8 | 27.7 | 11.2 | 50.4 | 46.9 |
| SR 50 @ Hartle Rd | Signal | LOS | E | E | C | F | F |
|  |  | Delay (sec/veh) | 70.4 | 77.6 | 29.2 | 165.5 | 110.7 |
|  | Signal (Improved) | LOS | E | E | C | E | F |
|  |  | Delay (sec/veh) | 66.3 | 78.2 | 29.3 | 77.4 | 109.1 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | D | D | D | C |
|  |  | Delay (sec/veh) | 32.5 | 46.0 | 33.7 | 39.8 | 22.1 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | D | D | C | C |
|  |  | Delay (sec/veh) | 34.4 | 40.5 | 48.5 | 32.3 | 22.5 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | E | E | D | D |
|  |  | Delay (sec/veh) | 51.4 | 65.8 | 79.4 | 44.0 | 51.4 |
| Hartle Road @ North Access | TWSC | LOS | - | B |  | A |  |
|  |  | Delay (sec/veh) | - | 10.8 |  | 0.0 |  |
| Hartle Road @ South Access | AWSC | LOS | - | A | A |  | A |
|  |  | Delay (sec/veh) | - | 8.1 | 6.9 |  | 7.4 |
| Hancock Road @ South Access | TWSC | LOS | - |  | C |  | A |
|  |  | Delay (sec/veh) | - |  | 21.1 |  | 9.9 |

Table 5.3 cont. - Future Intersection Level of Service - Scenario 1

| Intersection | Stop Control | Intersection Conditions | Approach |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Overall | EB | WB | NB | SB |
| PM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | F | F | F | F | F |
|  |  | Delay (sec/veh) | 184.5 | 104.8 | 221.8 | 175.4 | 221.0 |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | LOS | D | C | E | E | E |
|  |  | Delay (sec/veh) | 42.7 | 21.2 | 56.3 | 70.4 | 62.1 |
|  | Signal (Option 2) | LOS | C | B | D | E | E |
|  |  | Delay (sec/veh) | 32.7 | 17.5 | 41.5 | 67.5 | 63.9 |
| SR 50 @ Hartle Rd | Signal | LOS | F | D | F | F | F |
|  |  | Delay (sec/veh) | 134.0 | 48.1 | 139.0 | 158.8 | 391.0 |
|  | Signal (Improved) | LOS | F | D | F | F | F |
|  |  | Delay (sec/veh) | 131.5 | 48.1 | 139.0 | 89.0 | 391.0 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | D | D | D | C |
|  |  | Delay (sec/veh) | 34.4 | 52.1 | 49.1 | 40.9 | 24.3 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | D | D | B | B |
|  |  | Delay (sec/veh) | 23.5 | 54.1 | 48.5 | 14.9 | 13.0 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | E | E | C | D |
|  |  | Delay (sec/veh) | 41.3 | 59.7 | 78.3 | 26.2 | 45.9 |
| Hartle Road @ North Access | TWSC | LOS | - | B |  | A |  |
|  |  | Delay (sec/veh) | - | 10.8 |  | 0.0 |  |
| Hartle Road @ South Access | TWSC | LOS | - | A | A |  | A |
|  |  | Delay (sec/veh) | - | 8.0 | 7.0 |  | 8.0 |
| Hancock Road @ South Access | TWSC | LOS | - |  | C |  | A |
|  |  | Delay (sec/veh) | - |  | 22.7 |  | 10.0 |

Source: Littlejohn Engineering Associates
With the addition of project traffic at the SR 50/Emil Jahna Road intersection, the minor street approaches to this intersection operate below the level of service standard in the PM peak period. Both Options 1 and 2 for Emil Jahna Road (a 2-lane or 4-lane approach) result in operations below the level of service standard, although Option 2 allows more green time for the westbound leftturn approach, allowing that approach to meet level of service standards. However, with both options for Emil Jahna Road, the average delays for the minor street approaches are approximately half of the green time for the eastbound and westbound through volumes, indicating that all vehicles should be able to clear the intersection within one cycle, and that the delays are due to the extended green times required for the through volumes.

While there are existing deficiencies at the intersection of SR 50/Hartle Road, the addition of project trips significantly worsens the delays on the northbound approach in the AM peak period. The addition of an "overlap" phase (giving the northbound right-turns a green arrow while the westbound left-turns have a green arrow) would significantly lessen the delays on this movement/approach in the AM peak period. The existing turn-lanes at the intersection are sufficient to serve the traffic for each movement, and there are no additional turn lanes that would
mitigate any of the remaining deficiencies which are caused by the large volume of traffic on SR 50.

An analysis of the $95^{\text {th }}$ percentile queue length of each of the turn lanes into and out of the site are shown in Table 5.4.

Table 5.4 - Queue Analysis - Scenario 1

| Intersection | Stop Control | Lane | Existing Lane Length (ft) | 95 ${ }^{\text {tho }}$ \% Queue Length (ft) | Required decel length ${ }^{1}$ (ft) | Total length required (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | WB Left | 320 | 195 | 240 | 435 |
|  | Signal (Option 2) | WB Left | 320 | 201 | 240 | 441 |
| SR 50 @ Hartle Rd | Signal | EB Right | 480 | 4 | 240 | 244 |
|  |  | WB Left | 290 | 424 | 240 | 664 |
|  |  | NB Left | 120 | 114 | 0 | 114 |
|  | Signal (Improved) | EB Right | 480 | 4 | 240 | 244 |
|  |  | WB Left | 290 | 424 | 240 | 664 |
|  |  | NB Left | 120 | 114 | 0 | 114 |
| Hartle Road @ North Access | TWSC | SB Right | n/a | 0 | 95 | 95 |
|  |  | NB Left | n/a | 0 | 95 | 95 |
| Hancock Road @ South Access | TWSC | SB Left | n/a | 7 | 190 | 197 |
|  |  | NB Right | n/a | 0 | 190 | 190 |
|  |  | WB Left | n/a | 9 | 0 | 9 |

${ }^{1}$ Does not include required taper length
Source: Littlejohn Engineering Associates
When the required deceleration length is added to the projected 95th percentile queue for the roadway, the westbound left-turn lane at the intersection of SR 50/Emil Jahna Road, and the westbound left-turn lane at the intersection of SR 50/Hartle Road do not meet the required turn lane length. In lieu of extended the turn lanes at these intersections (as spacing to the upstream median openings prevents the extension of the lane to the proper length), a secondary left-turn lane may be added to store the vehicles.

### 5.3 Future Roadway Segment Analysis - Scenario 1

The project trips were added to the existing traffic volumes and committed trips shown in the Lake Sumter MPO TMS Report to determine the future roadway segment volumes. These volumes were identified and compared for each segment to the estimated capacity based on the FDOT Q/LOS Tables. The results of that analysis are shown in Table 5.5.

Based on the roadway segment analysis, there are seven (7) segments which are projected to operate below the level of service standard for the roadway. However, all of these segments are deficient with just the background and committed trips, and thus are backlogged before the addition of project trips.

Table 5.5 - Roadway Segment Analysis (2025) - Scenario 1

| Roadway | Segment | $\begin{aligned} & \text { LOS } \\ & \text { Std } \end{aligned}$ | $\begin{aligned} & \text { LOS } \\ & \text { Capacity } \\ & \hline \end{aligned}$ | AADT | $\begin{aligned} & \mathrm{Pk} \\ & \text { Dir } \end{aligned}$ | Pk Hr/Pk Dir Existing | LOS | Committed Trips | Pk Hr/Pk Dir with Committed Trips | LOS | $\begin{aligned} & \text { Project } \\ & \text { Trips } \end{aligned}$ | Background, Committed, and Project Trips | v/c | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 50 | CR 561 to East Ave | D | 2,000 | 34,421 | WB | 1,688 | C | 124 | 1,812 | C | 13 | 1,825 | 0.91 | C |
|  | East Ave to US 27 | D | 3,020 | 43,709 | WB | 2,144 | c | 156 | 2,300 | c | 19 | 2,319 | 0.77 | C |
|  | US 27 to Hancock Road | D | 3,020 | 44,255 | WB | 2,171 | c | 639 | 2,810 | C | 38 | 2,848 | 0.94 | C |
|  | Hancock Road to Emil Jahna Rd | D | 3,020 | 56,275 | WB | 2,760 | c | 854 | 3,614 | F | 94 | 3,708 | 1.23 | F |
|  | Emil Jahna Rd to CR 455 | D | 3,020 | 56,275 | WB | 2,760 | c | 854 | 3,614 | F | 114 | 3,728 | 1.23 | F |
|  | CR 455 to Orange County Line | D | 3,020 | 47,534 | WB | 2,332 | c | 907 | 3,239 | F | 263 | 3,502 | 1.16 | F |
| US 27 | Grand Hwy to SR 50 | C | 2,940 | 27,865 | NB | 1,367 | C | 173 | 1,540 | C | 2 | 1,542 | 0.52 | C |
|  | SR 50 to Johns Lake Rd | c | 2,940 | 37,153 | SB | 1,822 | c | 302 | 2,124 | c | 1 | 2,125 | 0.72 | C |
|  | Johns Lake Rd to Hartwood Marsh Rd | c | 2,940 | 33,328 | NB | 1,635 | c | 141 | 1,776 | c | 1 | 1,777 | 0.60 | C |
|  | Hartwood Marsh Rd to Lake Louisa Rd | c | 2,940 | 22,947 | NB | 1,126 | c | 141 | 1,267 | c | 13 | 1,280 | 0.44 | c |
|  | Lake Louisa Rd to Boggy Marsh Rd | C | 2,940 | 24,586 | SB | 1,206 | C | 50 | 1,256 | C | 7 | 1,263 | 0.43 | C |
| Old Hwy 50 | US 27 to Turkey Farm Rd | D | 792 | 7,238 | WB | 378 | C | 172 | 550 | C | 7 | 557 | 0.70 | C |
|  | Turkey Farm Rd to CR 455 | D | 792 | 5,592 | EB | 448 | c | 305 | 753 | D | 18 | 771 | 0.97 | D |
|  | CR 455 to Orange County Line | D | 792 | 5,950 | WB | 513 | C | 100 | 613 | C | 17 | 630 | 0.80 | C |
| CR 455 | Ridgewood Ave to CR 455/CR 50 | D | 1,200 | 6,879 | SB | 331 | B | 257 | 588 | C | 16 | 604 | 0.50 | C |
|  | CR 455/CR 50 to SR 50 | D | 675 | 7,844 | NB | 398 | D | 249 | 647 | D | 24 | 671 | 0.99 | D |
| Citrus Tower Boulevard | US 27 to Oakley Seaver Dr | D | 792 | 12,177 | SB | 601 | C | 6 | 607 | C | 11 | 618 | 0.78 | C |
|  | Oakley Seaver Dr to SR 50 | D | 1,800 | 16,110 | NB | 692 | C | 60 | 752 | C | 2 | 754 | 0.42 | C |
|  | SR 50 to Hooks St | D | 1,800 | 17,355 | SB | 834 | C | 102 | 936 | C | 14 | 950 | 0.53 | C |
|  | Hooks St to Johns Lake Rd | D | 1,800 | 18,431 | SB | 922 | c | 108 | 1,030 | C | 8 | 1,038 | 0.58 | C |
|  | Johns Lake Rd to US 27 | D | 1,800 | 14,579 | SB | 713 | c | 50 | 763 | C | 3 | 766 | 0.43 | C |
| Hancock Road | CR 50 to Ridge Blvd | D | 1,800 | 11,023 | SB | 472 | C | 394 | 866 | c | 27 | 893 | 0.50 | C |
|  | Ridge Blvd to SR 50 | D | 1,800 | 14,533 | NB | 643 | c | 611 | 1,254 | c | 31 | 1,285 | 0.71 | c |
|  | SR 50 to Hooks St | D | 1,800 | 18,478 | SB | 932 | c | 170 | 1,102 | c | 77 | 1,179 | 0.66 | C |
|  | Hooks St to Johns Lake Rd | D | 792 | 18,478 | SB | 932 | F | 161 | 1,093 | F | 74 | 1,167 | 1.47 | F |
|  | Johns Lake Rd to Hartwood Marsh Rd | D | 792 | 8,483 | SB | 405 | C | 139 | 544 | C | 14 | 558 | 0.71 | C |
| Hartwood Marsh Road | US 27 to Hancock Road | D | 675 | 14,102 | WB | 771 | F | 11 | 782 | F | 8 | 790 | 1.17 | F |
|  | Hancock Road to 90 Degree Bend | D | 675 | 10,247 | EB | 720 | F | 6 | 726 | F | 1 | 727 | 1.08 | F |
|  | 90 Degree Bend to Orange County Line | D | 675 | 10,247 | EB | 720 | F | 6 | 726 | F | 0 | 726 | 1.08 | F |
| Lake Louisa Road | Lakeshore Dr to Vista Del Lago Blvd | D | 675 | 3,456 | EB | 163 | C | 0 | 163 | C | 0 | 163 | 0.24 | C |
|  | Vista Del Lago Blvd to US 27 | D | 675 | 4,044 | WB | 301 | c | 0 | 301 | C | 0 | 301 | 0.45 | C |
| Grand Highway | Citrus Tower Blvd to SR 50 | D | 675 | 6,436 | NB | 309 | C | 5 | 314 | c | 0 | 314 | 0.47 | C |
|  | SR 50 to Hooks St | D | 1,800 | 6,292 | SB | 303 | C | 35 | 338 | c | 3 | 341 | 0.19 | C |

Table 5.5 cont. - Roadway Segment Analysis (2025) - Scenario 1

| Roadway | Segment | $\begin{aligned} & \text { LOS } \\ & \text { Std } \\ & \hline \end{aligned}$ | $\begin{gathered} \text { LOS } \\ \text { Capacity } \\ \hline \end{gathered}$ | AADT | $\begin{aligned} & \text { Pk } \\ & \text { Dir } \end{aligned}$ | Pk Hr/Pk Dir Existing | LOS | $\begin{array}{\|c} \hline \text { Committed } \\ \text { Trips } \end{array}$ | Pk Hr/Pk Dir with Committed Trips | LOS | $\begin{gathered} \text { Project } \\ \text { Trips } \\ \hline \end{gathered}$ | Background, Committed, and Project Trips | v/c | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hooks Street | Lakeshore Dr to US 27 | D | 675 | 7,007 | EB | 347 | D | 4 | 351 | D | 0 | 351 | 0.52 | D |
|  | US 27 to Oakley Seaver Dr | D | 1,800 | 9,512 | WB | 396 | C | 22 | 418 | C | 4 | 422 | 0.23 | C |
|  | Oakley Seaver Dr to Citrus Tower Blvd | D | 1,800 | 9,367 | WB | 398 | C | 22 | 420 | C | 8 | 428 | 0.24 | c |
|  | Citrus Tower Blvd to Hancock Rd | D | 1,800 | 11,451 | WB | 603 | C | 11 | 614 | C | 5 | 619 | 0.34 | c |
| Anderson Hill Road | Lakeshore Dr to US 27 | D | 675 | 1,584 | EB | 105 | C | 0 | 105 | C | 2 | 107 | 0.16 | C |
| East Avenue | CR 561 to SR 50 | D | 675 | 5,103 | SB | 286 | C | 0 | 286 | C | 3 | 289 | 0.43 | C |
| Hammock Ridge Road | Lakeshore Dr to US 27 | D | 1,800 | 15,472 | WB | 921 | C | 60 | 981 | C | 1 | 982 | 0.55 | C |
| Lakeshore Drive | Hammock Ridge Road to Anderson Hill Rd | D | 675 | 7,500 | NB | 416 | D | 13 | 429 | D | 3 | 432 | 0.64 | D |
| Turkey Farm Road | E Grassy Lake Road to CR 50 | D | 675 | 344 | NB | 22 | C | 0 | 22 | C | 9 | 31 | 0.05 | C |
| Johns Lake Road | US 27 to Hancock Road | D | 675 | 8,489 | EB | 390 | D | 26 | 416 | D | 6 | 422 | 0.62 | D |
| Blackstill Lake Road | Fosgate Rd to CR 50 | D | 612 | 3,135 | SB | 156 | C | 68 | 224 | C | 1 | 225 | 0.37 | C |

Source: Lake Sumter MPO TMS Report for Lake County, April 5, 2015; Florida Traffic Online; Littlejohn

The required improvements (widening for additional lanes or equivalent capacity improvement) would also satisfy the demands of the project trips, and thus the project cannot be held responsible for the improvements to these segments, per Florida Statute 163.3180 (5) (h) 2. b.

### 5.4 Future Intersection Analysis - Scenario 2

The combined background, committed (for SR 50), and project trips were analyzed for the Scenario 2 access using Synchro 8. The results of these evaluations are shown in Table $\mathbf{5 . 6}$ with the printouts of the analysis shown in Appendix H. As was completed for the no-build analysis, the traffic signals were retimed/optimized as it can be expected that retiming will occur over the next 10 years. The intersection of SR 50/Emil Jahna Road was analyzed with two options, with Option 1 being an improved two-lane roadway (bringing the roadway up to modern design standards) and Option 2 being a 4-lane roadway.

Table 5.6 - Future Intersection Level of Service - Scenario 2

| Intersection | Stop Control | Intersection Conditions | Approach |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Overall | EB | WB | NB | SB |
| AM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | F | E | D | F | F |
|  |  | Delay (sec/veh) | 81.9 | 67.3 | 54.2 | 200.8 | 82.0 |
|  | Signal (Improved) | LOS | E | E | D | E | E |
|  |  | Delay (sec/veh) | 60.5 | 57.2 | 50.3 | 75.6 | 78.1 |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | LOS | C | D | B | E | D |
|  |  | Delay (sec/veh) | 32.4 | 38.7 | 13.6 | 74.9 | 51.1 |
|  | Signal (Option 2) | LOS | C | C | B | E | D |
|  |  | Delay (sec/veh) | 24.3 | 28.1 | 11.0 | 55.6 | 51.6 |
| SR 50 @ Hartle Rd | Signal | LOS | F | E | C | F | F |
|  |  | Delay (sec/veh) | 86.8 | 73.5 | 30.2 | 398.6 | 120.1 |
|  | Signal (Improved) | LOS | E | E | C | F | F |
|  |  | Delay (sec/veh) | 72.1 | 75.0 | 27.6 | 188.2 | 110.8 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | D | C | D | C |
|  |  | Delay (sec/veh) | 26.6 | 39.1 | 29.4 | 49.1 | 20.0 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | D | D | C | C |
|  |  | Delay (sec/veh) | 33.4 | 40.9 | 47.6 | 29.5 | 24.0 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | E | E | D | D |
|  |  | Delay (sec/veh) | 54.4 | 58.4 | 76.7 | 53.4 | 52.3 |
| Hartle Road @ North Access | TWSC | LOS | - | B |  | A |  |
|  |  | Delay (sec/veh) | - | 10.2 |  | 0.0 |  |
| Hartle Road @ South Access | AWSC | LOS | - | A | A |  | A |
|  |  | Delay (sec/veh) | - | 7.5 | 6.8 |  | 7.3 |
| Hancock Road @ South Access | TWSC | LOS | - |  | C |  | B |
|  |  | Delay (sec/veh) | - |  | 24.8 |  | 10.1 |

Table 5.6 cont. - Future Intersection Level of Service - Scenario 2

| Intersection | Stop Control | Intersection Conditions | Approach |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Overall | EB | WB | NB | SB |
| PM Peak Period |  |  |  |  |  |  |  |
| SR 50 @ Hancock Rd | Signal | LOS | F | F | F | F | F |
|  |  | Delay (sec/veh) | 195.9 | 129.2 | 227.8 | 200.1 | 207.5 |
|  | Signal (Improved) | LOS | F | F | F | F | F |
|  |  | Delay (sec/veh) | 174.2 | 109.7 | 207.2 | 114.0 | 216.6 |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | LOS | D | C | E | E | E |
|  |  | Delay (sec/veh) | 48.5 | 21.9 | 65.9 | 70.4 | 62.1 |
|  | Signal (Option 2) | LOS | D | B | D | E | E |
|  |  | Delay (sec/veh) | 37.6 | 18.1 | 49.7 | 67.5 | 63.9 |
| SR 50 @ Hartle Rd | Signal | LOS | F | D | F | F | F |
|  |  | Delay (sec/veh) | 143.4 | 47.7 | 148.6 | 104.4 | 468.3 |
|  | Signal (Improved) | LOS | E | E | C | E | F |
|  |  | Delay (sec/veh) | 66.3 | 78.2 | 29.3 | 77.4 | 109.1 |
| US 27 @ Johns Lake Rd | Signal | LOS | C | E | D | D | C |
|  |  | Delay (sec/veh) | 34.4 | 55.3 | 47.9 | 42.1 | 22.9 |
| Citrus Tower Blvd @ Johns Lake Rd | Signal | LOS | C | D | D | B | B |
|  |  | Delay (sec/veh) | 23.5 | 54.1 | 48.5 | 14.9 | 13.0 |
| Hancock Road @ Johns Lake Road | Signal | LOS | D | E | E | C | D |
|  |  | Delay (sec/veh) | 44.8 | 70.4 | 73.6 | 26.4 | 49.6 |
| Hartle Road @ North Access | TWSC | LOS | - | A |  | A |  |
|  |  | Delay (sec/veh) | - | 9.9 |  | 0.0 |  |
| Hartle Road @ South Access | TWSC | LOS | - | A | A |  | A |
|  |  | Delay (sec/veh) | - | 7.6 | 6.8 |  | 7.6 |
| Hancock Road @ South Access | TWSC | LOS | - |  | C |  | B |
|  |  | Delay (sec/veh) | - |  | 23.3 |  | 10.6 |

Source: Littlejohn Engineering Associates
While the intersection of SR 50/Hancock Road operated below the level of service standards in the no-build analysis, the addition of project trips causes a significant increase in delays on the northbound approach in the AM and PM peak periods. The addition of a northbound right-turn lane mitigates for the additional delays caused by project trips, although there are still numerous deficiencies at the intersection that can only be mitigated with by improved capacity on SR 50 .

At the intersection of SR 50/Emil Jahna Road, both options analyzed (2-lane or 4-lane roadway) result in deficient conditions for the minor street approaches due to the extended green times for the eastbound and westbound approaches. Option 2 (4-lane roadway) decreases average delays on the westbound approach in the PM peak period, allowing that approach to meet LOS standards.

As was indicated in Scenario 1, the addition of project trips significantly worsens the delays on the northbound approach to the SR 50/Hartle Road intersection, although this intersection did not
meet LOS standards in the no-build scenario. The addition of an "overlap" phase (giving the northbound right-turns a green arrow while the westbound left-turns have a green arrow) would significantly lessen the delays on this movement/approach in the AM peak period. The existing turn-lanes at the intersection are sufficient to serve the traffic for each movement, and there are no additions of turn lanes that would mitigate any of the remaining deficiencies which are caused by the large volume of traffic on SR 50.

All of the project access intersections operate within the level of service standards as two-lane roadways with no additional turn lanes proposed.

An analysis of the $95^{\text {th }}$ percentile queue length of each of the turn lanes into and out of the site is shown in Table 5.7.

Table 5.7 - Queue Analysis - Scenario 2

| Intersection | Stop Control | Lane | Existing Lane Length (ft) | 95 ${ }^{\text {th }} \%$ Queue Length (ft) | Required decel length ${ }^{1}$ (ft) | Total length required (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 50 @ Emil Jahna Rd | Signal (Option 1) | WB Left | 320 | 195 | 240 | 435 |
|  | Signal (Option 2) | WB Left | 320 | 201 | 240 | 441 |
| SR 50 @ Hartle Rd | Signal | EB Right | 480 | 30 | 240 | 270 |
|  |  | WB Left | 290 | 306 | 240 | 646 |
|  |  | NB Left | 120 | 121 | 0 | 121 |
|  | Signal (Improved) | EB Right | 480 | 30 | 240 | 270 |
|  |  | WB Left | 290 | 306 | 240 | 646 |
|  |  | NB Left | 120 | 121 | 0 | 121 |
| Hartle Road @ North Access | TWSC | SB Right | n/a | 0 | 95 | 95 |
|  |  | NB Left | n/a | 0 | 95 | 95 |
| Hancock Road @ South Access | TWSC | SB Left | n/a | 17 | 190 | 207 |
|  |  | NB Right | n/a | 0 | 190 | 190 |
|  |  | WB Left | n/a | 3 | 0 | 3 |

${ }^{1}$ Does not include required taper length
Source: Littlejohn Engineering Associates
When the required deceleration length is added to the projected 95th percentile queue for the roadway, the westbound left-turn lane at the intersection of SR 50/Emil Jahna Road, and the westbound left-turn lane at the intersection of SR 50/Hartle Road do not meet the required turn lane length. In lieu of extended the turn lanes at these intersections (as spacing to the upstream median openings prevents the extension of the lane to the proper length), a secondary left-turn lane may be added to store the vehicles.

### 5.5 Future Roadway Segment Analysis - Scenario 2

The project trips were added to the existing traffic volumes and committed trips shown in the Lake Sumter MPO TMS Report to determine the future roadway segment volumes. These volumes were identified and compared for each segment to the estimated capacity based on the FDOT Q/LOS Tables. The results of that analysis are shown in Table 5.8.

Based on the roadway segment analysis, there are eight (8) segments which are projected to operate below the level of service standard for the roadway. Of these segments, only one becomes deficient with the addition of project trips; with the rest operating below the level of service standards with the existing and/or existing + committed trips.

The segment where project trips result in the roadway volume becoming deficient is CR 455 from CR 455/CR 50 to SR 50. However, the addition of the Minneola Interchange may divert some of the existing and committed trips from this segment, which is only projected to be 10 vehicles over the level of service capacity with the addition of project trips.

The remaining segments are projected to be over-capacity prior to the addition of project trips, and thus can be considered backlogged. The required improvements (widening for additional lanes or equivalent capacity improvement) would also satisfy the demands of the project trips, and thus the project cannot be held responsible for the improvements to these segments, per Florida Statute 163.3180 (5) (h) 2. b.

Table 5.8 - Roadway Segment Analysis (2025) - Scenario 2

| Roadway | Segment | $\begin{aligned} & \text { LOS } \\ & \text { Std } \\ & \hline \end{aligned}$ | Los Capacity | AADT | $\begin{aligned} & \text { Pk } \\ & \text { Dir } \end{aligned}$ | Pk Hr/Pk Dir Existing | LOS | Committed Trips | Pk Hr/Pk Dir with Committed Trips | LOS | Project Trips | Background, Committed, and Project Trips | v/c | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SR 50 | CR 561 to East Ave | D | 2,000 | 34,421 | WB | 1,688 | C | 124 | 1,812 | C | 12 | 1,824 | 0.91 | C |
|  | East Ave to US 27 | D | 3,020 | 43,709 | WB | 2,144 | C | 156 | 2,300 | c | 18 | 2,318 | 0.77 | C |
|  | US 27 to Hancock Road | D | 3,020 | 44,255 | WB | 2,171 | c | 639 | 2,810 | c | 30 | 2,840 | 0.94 | C |
|  | Hancock Road to Emil Jahna Rd | D | 3,020 | 56,275 | WB | 2,760 | c | 854 | 3,614 | F | 207 | 3,821 | 1.27 | F |
|  | Emil Jahna Rd to CR 455 | D | 3,020 | 56,275 | WB | 2,760 | c | 854 | 3,614 | F | 107 | 3,721 | 1.23 | F |
|  | CR 455 to Orange County Line | D | 3,020 | 47,534 | WB | 2,332 | c | 907 | 3,239 | F | 241 | 3,480 | 1.15 | F |
| US 27 | Grand Hwy to SR 50 | C | 2,940 | 27,865 | NB | 1,367 | C | 173 | 1,540 | C | 6 | 1,546 | 0.53 | C |
|  | SR 50 to Johns Lake Rd | c | 2,940 | 37,153 | SB | 1,822 | C | 302 | 2,124 | c | 2 | 2,126 | 0.72 | C |
|  | Johns Lake Rd to Hartwood Marsh Rd | c | 2,940 | 33,328 | NB | 1,635 | C | 141 | 1,776 | c | 2 | 1,778 | 0.60 | C |
|  | Hartwood Marsh Rd to Lake Louisa Rd | c | 2,940 | 22,947 | NB | 1,126 | C | 141 | 1,267 | c | 12 | 1,279 | 0.44 | C |
|  | Lake Louisa Rd to Boggy Marsh Rd | C | 2,940 | 24,586 | SB | 1,206 | c | 50 | 1,256 | c | 7 | 1,263 | 0.43 | C |
| Old Hwy 50 | US 27 to Turkey Farm Rd | D | 792 | 7,238 | WB | 378 | c | 172 | 550 | C | 6 | 556 | 0.70 | C |
|  | Turkey Farm Rd to CR 455 | D | 792 | 5,592 | EB | 448 | c | 305 | 753 | D | 23 | 776 | 0.98 | D |
|  | CR 455 to Orange County Line | D | 792 | 5,950 | WB | 513 | C | 100 | 613 | C | 25 | 638 | 0.81 | C |
| CR 455 | Ridgewood Ave to CR 455/CR 50 | D | 1,200 | 6,879 | SB | 331 | B | 257 | 588 | C | 17 | 605 | 0.50 | C |
|  | CR 455/CR 50 to SR 50 | D | 675 | 7,844 | NB | 398 | D | 249 | 647 | D | 38 | 685 | 1.01 | E |
| Citrus Tower Boulevard | US 27 to Oakley Seaver Dr | D | 792 | 12,177 | SB | 601 | C | 6 | 607 | C | 15 | 622 | 0.79 | C |
|  | Oakley Seaver Dr to SR 50 | D | 1,800 | 16,110 | NB | 692 | c | 60 | 752 | c | 6 | 758 | 0.42 | C |
|  | SR 50 to Hooks St | D | 1,800 | 17,355 | SB | 834 | c | 102 | 936 | c | 16 | 952 | 0.53 | C |
|  | Hooks St to Johns Lake Rd | D | 1,800 | 18,431 | SB | 922 | C | 108 | 1,030 | c | 8 | 1,038 | 0.58 | C |
|  | Johns Lake Rd to US 27 | D | 1,800 | 14,579 | SB | 713 | C | 50 | 763 | C | 3 | 766 | 0.43 | C |
| Hancock Road | CR 50 to Ridge Blvd | D | 1,800 | 11,023 | SB | 472 | C | 394 | 866 | c | 32 | 898 | 0.50 | C |
|  | Ridge Blvd to SR 50 | D | 1,800 | 14,533 | NB | 643 | c | 611 | 1,254 | c | 22 | 1,276 | 0.71 | C |
|  | SR 50 to Hooks St | D | 1,800 | 18,478 | SB | 932 | c | 170 | 1,102 | c | 93 | 1,195 | 0.66 | C |
|  | Hooks St to Johns Lake Rd | D | 792 | 18,478 | SB | 932 | F | 161 | 1,093 | F | 77 | 1,170 | 1.48 | F |
|  | Johns Lake Rd to Hartwood Marsh Rd | D | 792 | 8,483 | SB | 405 | C | 139 | 544 | C | 18 | 562 | 0.71 | C |
| Hartwood Marsh Road | US 27 to Hancock Road | D | 675 | 14,102 | WB | 771 | F | 11 | 782 | F | 7 | 789 | 1.17 | F |
|  | Hancock Road to 90 Degree Bend | D | 675 | 10,247 | EB | 720 | F | 6 | 726 | F | 5 | 731 | 1.08 | F |
|  | 90 Degree Bend to Orange County Line | D | 675 | 10,247 | EB | 720 | F | 6 | 726 | F | 4 | 730 | 1.08 | F |
| Lake Louisa Road | Lakeshore Dr to Vista Del Lago Blvd | D | 675 | 3,456 | EB | 163 | C | 0 | 163 | C | 0 | 163 | 0.24 | C |
|  | Vista Del Lago Blvd to US 27 | D | 675 | 4,044 | WB | 301 | c | 0 | 301 | C | 0 | 301 | 0.45 | C |
| Grand Highway | Citrus Tower Blvd to SR 50 | D | 675 | 6,436 | NB | 309 | C | 5 | 314 | C | 0 | 314 | 0.47 | C |
|  | SR 50 to Hooks St | D | 1,800 | 6,292 | SB | 303 | C | 35 | 338 | C | 3 | 341 | 0.19 | C |

Table 5.8 cont. - Roadway Segment Analysis (2025) - Scenario 2

| Roadway | Segment | $\begin{aligned} & \text { LOS } \\ & \text { Std } \end{aligned}$ | $\begin{aligned} & \text { LOS } \\ & \text { Capacity } \end{aligned}$ | AADT | $\begin{array}{\|l} \hline \mathrm{Pk} \\ \text { Dir } \\ \hline \end{array}$ | Pk Hr/Pk Dir Existing | LOS | Committed Trips | Pk Hr/Pk Dir with Committed Trips | LOS | Project Trips | Background, Committed, and Project Trips | v/c | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hooks Street | Lakeshore Dr to US 27 | D | 675 | 7,007 | EB | 347 | D | 4 | 351 | D | 0 | 351 | 0.52 | D |
|  | US 27 to Oakley Seaver Dr | D | 1,800 | 9,512 | WB | 396 | C | 22 | 418 | C | 4 | 422 | 0.23 | C |
|  | Oakley Seaver Dr to Citrus Tower Blvd | D | 1,800 | 9,367 | WB | 398 | c | 22 | 420 | c | 8 | 428 | 0.24 | c |
|  | Citrus Tower Blvd to Hancock Rd | D | 1,800 | 11,451 | WB | 603 | C | 11 | 614 | C | 5 | 619 | 0.34 | C |
| Anderson Hill Road | Lakeshore Dr to US 27 | D | 675 | 1,584 | EB | 105 | c | 0 | 105 | c | 2 | 107 | 0.16 | c |
| East Avenue | CR 561 to SR 50 | D | 675 | 5,103 | SB | 286 | c | 0 | 286 | c | 3 | 289 | 0.43 | C |
| Hammock Ridge Road | Lakeshore Dr to US 27 | D | 1,800 | 15,472 | WB | 921 | C | 60 | 981 | C | 1 | 982 | 0.55 | C |
| Lakeshore Drive | Hammock Ridge Road to Anderson Hill Rd | D | 675 | 7,500 | NB | 416 | D | 13 | 429 | D | 3 | 432 | 0.64 | D |
| Turkey Farm Road | E Grassy Lake Road to CR 50 | D | 675 | 344 | NB | 22 | C | 0 | 22 | C | 9 | 31 | 0.05 | C |
| Johns Lake Road | US 27 to Hancock Road | D | 675 | 8,489 | EB | 390 | D | 26 | 416 | D | 6 | 422 | 0.62 | D |
| Blackstill Lake Road | Fosgate Rd to CR 50 | D | 612 | 3,135 | SB | 156 | C | 68 | 224 | C | 1 | 225 | 0.37 | c |

Source: Lake Sumter MPO TMS Report for Lake County, April 5, 2015; Florida Traffic Online; Littlejohn

### 6.0 Findings and Recommendations

### 6.1 Intersection Findings

The intersection analysis indicated that the majority of intersections in the study area do not fully meet the level of service standards for the roadway network. For the intersections on SR 50, this is primarily due to the large through volume on the eastbound and westbound approaches which require the majority of the green time at the intersection, and limit the ability to provide an acceptable level of service on the side streets. These intersections have appropriate turn lanes for the volume of traffic, and no additional turn lane improvements would significantly improve the delays for the minor street approaches and turning movements on the major roadway. Thus, the only solution to improve the operation of these intersections would be to increase capacity on SR 50 (through widening or other capacity improvements) or to reduce the demand on SR 50, which should happen with the construction of the Minneola interchange on the turnpike.

The intersections of SR 50/Hancock Road and SR 50/Hartle Road do not meet the LOS standards in the existing conditions. With the addition of project trips in both scenarios, there is a significant increase in the northbound delays at the SR 50/Hartle Road intersection, which could be lessened by the addition of a right-turn overlap phase (allowing the northbound right-turns to have a green arrow during the westbound left-turn phase). Likewise, in Scenario 2, there is a significant increase in delays on the northbound approach to the SR 50/Hancock Road intersection over the existing condition. Adding a dedicated right-turn lane at this intersection would lessen the delays on this approach. As both of these intersections have existing deficiencies prior to the addition of project volumes, improvements at these intersections should be accomplished through a proportionate fair-share agreement and credited to the impact fees of the project.

All of the direct project access points (onto Hancock Road and Hartle Road) operate at an acceptable level of service. The intersection of Hancock Road/south access point was assumed to have a southbound left-turn lane, a northbound right-turn lane, and a westbound left-turn lane. The intersection of Hartle Road/north access point was assumed to have a southbound right-turn lane and a northbound left-turn lane. No additional turn lanes were assumed for the Hartle Road/south access point intersection.

The intersection of SR 50/Emil Jahna Road was analyzed with two scenarios, a two-lane Emil Jahna Road (Option 1) and a four-lane Emil Jahna Road (Option 2). Option 2 reduces the delays on the minor street approach, but not significantly enough to impact the level of service of the approach.

The queue analysis of the access intersections indicated that the existing westbound left-turn lanes on SR 50 at the intersection of SR 50/Emil Jahna Road and SR 50/Hartle Road are too short to provide ample space for both the $95^{\text {th }}$ percentile queue and the required deceleration distance per FDOT standards. At both of these intersections, there may not be sufficient length between the turn lane and upstream median openings to provide the required length, thus creating a double left-turn may be appropriate to satisfy the queuing requirements.

### 6.2 Roadway Network Findings

Based on the roadway segment analysis, there are seven (7) segments in Scenario 1 (cross-access allowed between Phases $5 \& 6$ ) and eight (8) segments in Scenario 2 (emergency access only between Phases $5 \& 6$ ) which are projected to operate below the level of service standard for the roadway. Of these segments, only one becomes deficient with the addition of project trips (in Scenario 2 only), with the rest operating below the level of service standards with the existing and/or existing + committed trips. The segment where project trips result in the roadway volumes becoming deficient in Scenario 2 is CR 455 from CR $455 / C R 50$ to SR 50 . However, the addition of the Minneola Interchange may divert some of the existing and committed trips from this segment, which is only projected to be four vehicles over the level of service capacity with the addition of project trips in either Scenario.

The remaining seven segments are projected to be over-capacity prior to the addition of project trips, and thus can be considered backlogged. The required improvements (widening for additional lanes or equivalent capacity improvement) would also satisfy the demands of the project trips, and thus the project cannot be held responsible for the improvements to these segments, per Florida Statute 163.3180 (5) (h) 2. b.

### 6.3 Recommendations

Based on the above analysis, the following improvements are proposed:

1. Add northbound right-turn lane at the intersection of SR 50/Hancock Road (Scenario 2 only)
2. Add a northbound right-turn arrow to the signal at the intersection of SR 50/Hartle Road
3. Lengthen the westbound left-turn lane at the intersection of SR 50/Emil Jahna Road or add a second westbound left-turn lane (if Option 2 is selected for Emil Jahna Road)
4. Lengthen the westbound left-turn lane at the intersection of SR 50/Hartle Road or add a second westbound left-turn lane

Improvements $1 \& 2$ are both located on approaches that are currently backlogged (and thus the project has no responsibility for the improvement), but are recommended in order to improve delays experienced by project traffic. Improvements $3 \& 4$ are recommended in order to provide sufficient queuing and deceleration distance per FDOT standards. All improvements should be completed using a proportionate fair-share agreement, with any costs of the off-site improvements being credited against the impact fees for the development. The construction of a portion of Hartle Road, from the existing terminus to the southern border of the property, may also be considered part of the projects mitigation requirements in lieu of the recommended improvements, as it is a portion of a larger planned roadway between SR 50 and Hartwood Marsh Road. Any other improvements to the roadway network and/or intersections are the responsibility of the City, County, and/or FDOT per Florida Statute, as a backlogged facility.

